

# HOW TO ESTIMATE THE RESOLUTION OF AN LES OF RECIRCULATING FLOW [1]

Lars Davidson, [www.tfd.chalmers.se/~lada](http://www.tfd.chalmers.se/~lada)

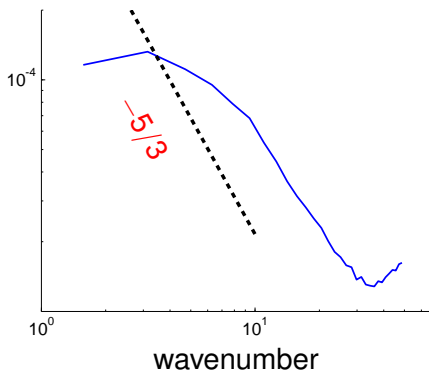
QLES 2009, Pisa, 9-11 Sept

# HOW TO ESTIMATE RESOLUTION OF AN LES?

- In boundary layers there are guidelines *à priori*. The cells size in the streamwise and spanwise direction should be approximately **100** and **30** respectively. First wall-adjacent node at  $y^+ \simeq 1$ .
- **No** guidelines in free-flow region (shear layers, re-circulation region ...)
- **Worse:** even after having carried out an LES, it is difficult to know if the resolution is good!
- I have recently made a similar study for channel flow [2]

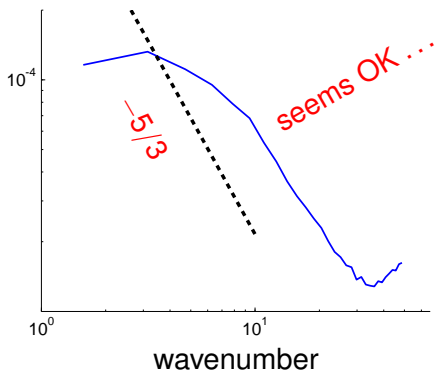
# ENERGY SPECTRUM

Energy spectrum



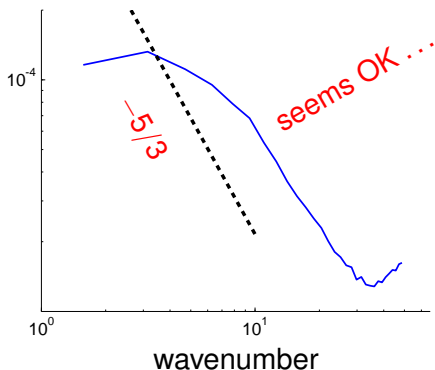
# ENERGY SPECTRUM AND TWO-POINT CORRELATION

Energy spectrum

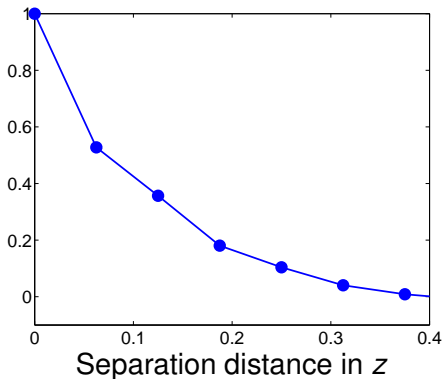


# ENERGY SPECTRUM AND TWO-POINT CORRELATION

## Energy spectrum

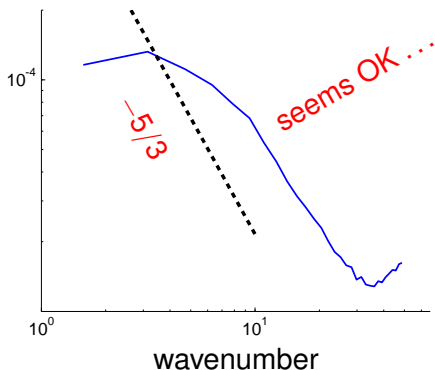


## Two-point correlation

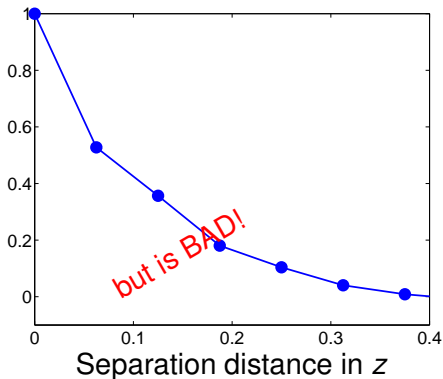


# ENERGY SPECTRUM AND TWO-POINT CORRELATION

## Energy spectrum

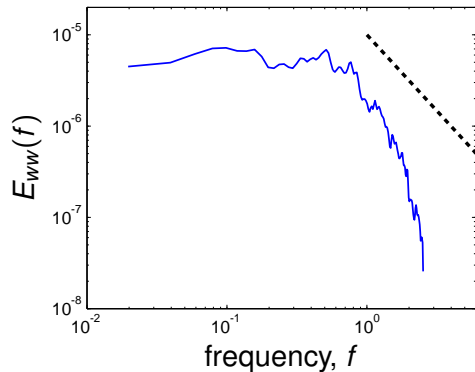


## Two-point correlation

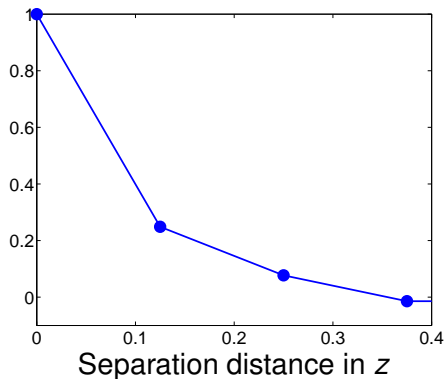


# ENERGY SPECTRUM VS TIME AND TWO-POINT CORRELATION

## Energy spectrum



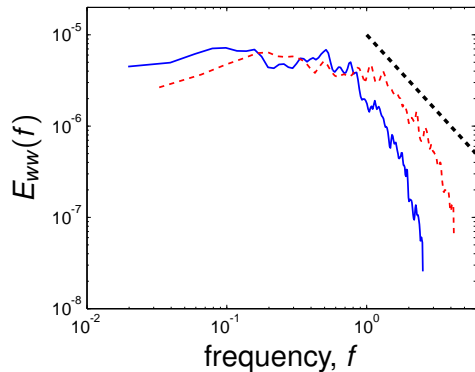
## Two-point correlation



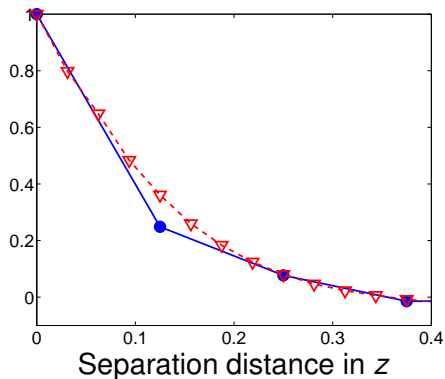
$N_x = 256, N_z = 32$

# ENERGY SPECTRUM VS TIME AND TWO-POINT CORRELATION

## Energy spectrum



## Two-point correlation

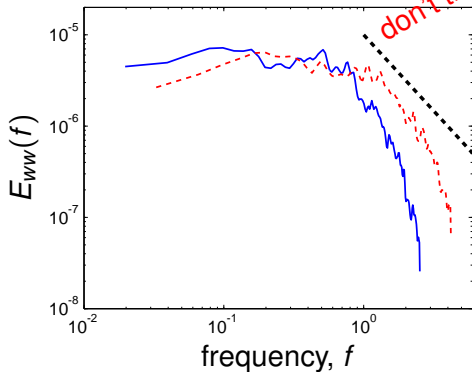


—  $N_x = 256, N_z = 32$ ; - - -  $N_x = 512, N_z = 128$

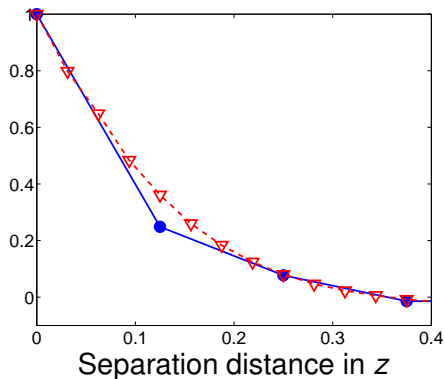


# ENERGY SPECTRUM VS TIME AND TWO-POINT CORRELATION

## Energy spectrum



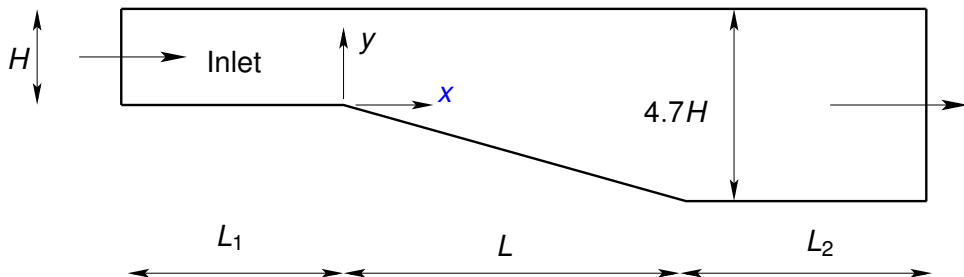
## Two-point correlation



don't trust energy spectra

—  $N_x = 256, N_z = 32$ ; - - -  $N_x = 512, N_z = 128$

# PLANE ASYMMETRIC DIFFUSER (NOT TO SCALE)



$L_1 = 7.9H$ ,  $L = 21H$ ,  $L_2 = 28H$ . The spanwise width is  $z_{max} = 4H$ .

- Mesh ( $x \times y \times z$ )

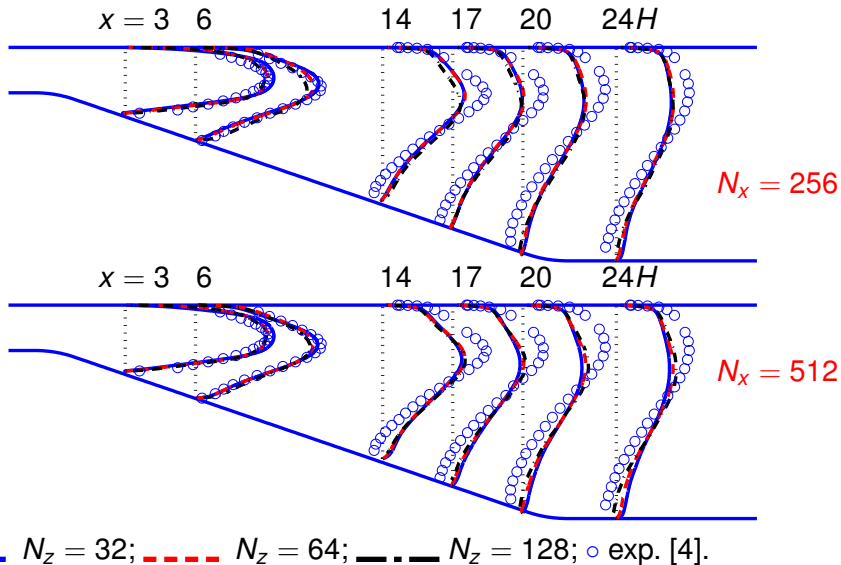
- $258 \times 64 \times 32$ ,  $258 \times 64 \times 64$ ,  $258 \times 64 \times 128$

- $512 \times 64 \times 32$ ,  $512 \times 64 \times 64$ ,  $512 \times 64 \times 128$

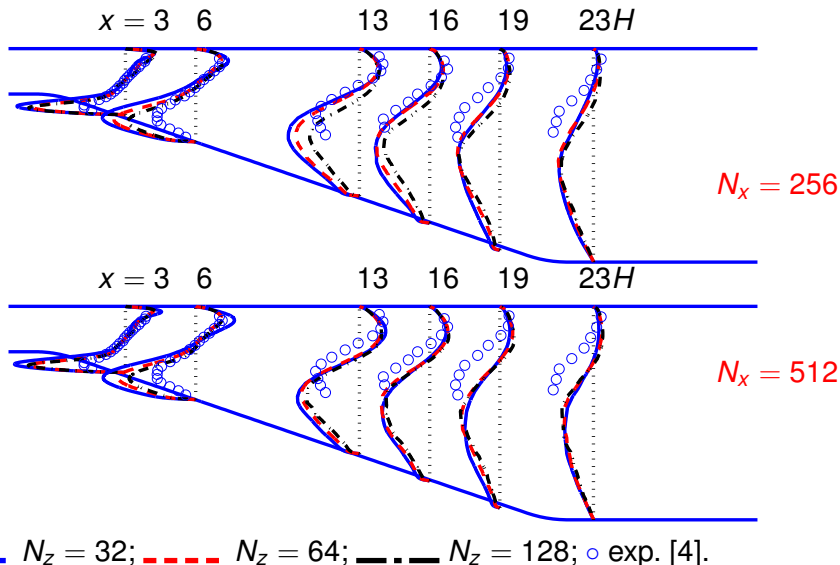
# COMPUTATIONAL METHOD

- Finite volume with central differencing in space and time (Crank-Nicolson)
- Fractional step
- Dynamic Smagorinsky model
- Inlet fluctuating boundary conditions: synthetic isotropic turbulence [3]
- All simulations run on a single CPU. Averaging during one week (the finest mesh: two weeks)

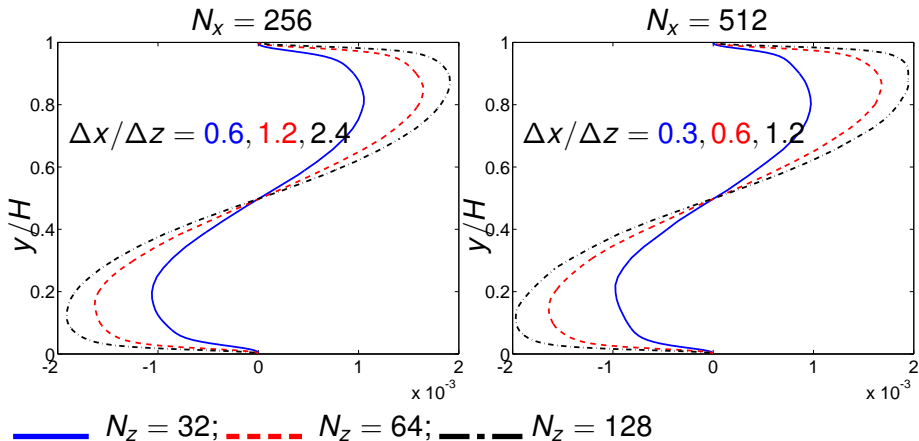
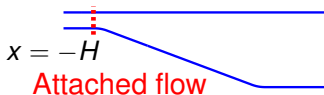
# $\langle \bar{u} \rangle / U_{b,in}$ PROFILES



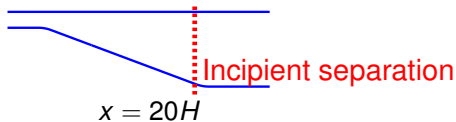
# $\langle u'v' \rangle / U_{b,in}^2$ PROFILES



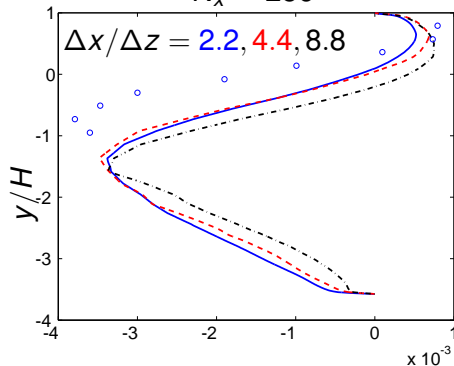
# $\langle u'v' \rangle / U_{b,in}^2$ PROFILES AT $x = -H$



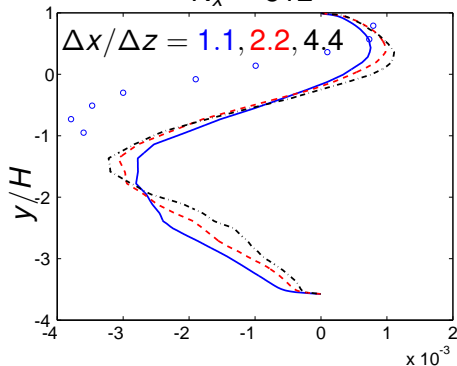
# $\langle u'v' \rangle / U_{b,in}^2$ PROFILES AT $x = 20H$



$N_x = 256$



$N_x = 512$



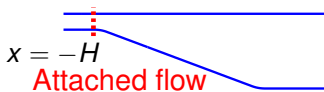
—  $N_z = 32$ ; - - -  $N_z = 64$ ; - . -  $N_z = 128$ ;  $\circ$  exp. [4].

# DIFFERENT WAYS TO ESTIMATE RESOLUTION

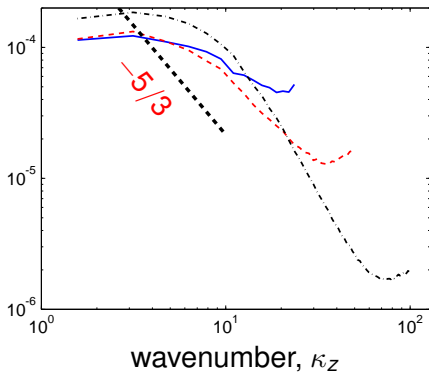
- **Energy** spectra (both in spanwise direction and time)
  - **Two-point** correlations
  - Ratio of SGS shear stress  $\langle \tau_{sgs,12} \rangle$  to resolved  $\langle u'v' \rangle$
  - Ratio of SGS viscosity,  $\langle \nu_{sgs} \rangle$  to molecular,  $\nu$
  - Energy spectra of **SGS dissipation**
  - Comparison of SGS dissipation due to  $\partial u'_i / \partial x_j$  and  $\partial \langle \bar{u}_i \rangle / \partial x_j$
- 
- Below we will only analyze results from the  $N_x = 256$  meshes



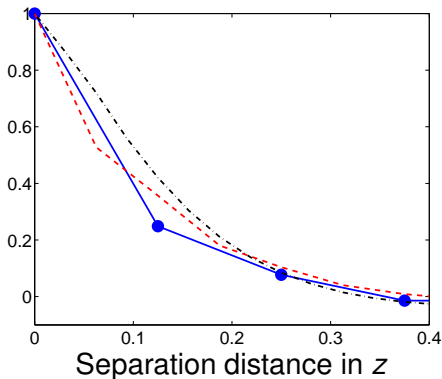
# ENERGY SPECTRA, TWO-POINT CORR. AT $x = -H$



Energy spectrum



Two-point correlation



—  $N_z = 32$ ; - - -  $N_z = 64$ ; - . -  $N_z = 128$ .

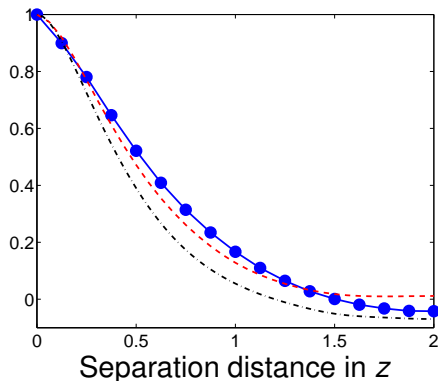
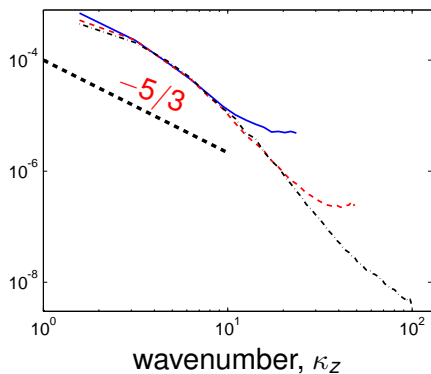
# ENERGY SPECTRA, TWO-POINT CORR. AT $x = 20H$



Energy spectrum

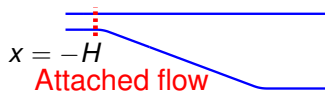
$x = 20H$

Two-point correlation

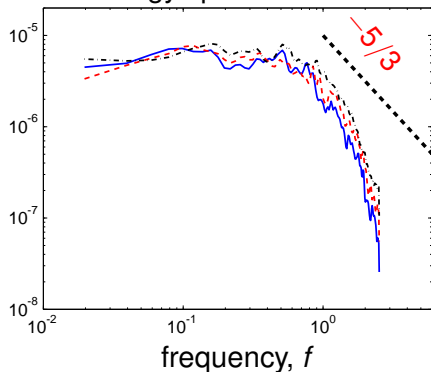


—  $N_z = 32$ ; 
 - - -  $N_z = 64$ ; 
 - . - .  $N_z = 128$ .

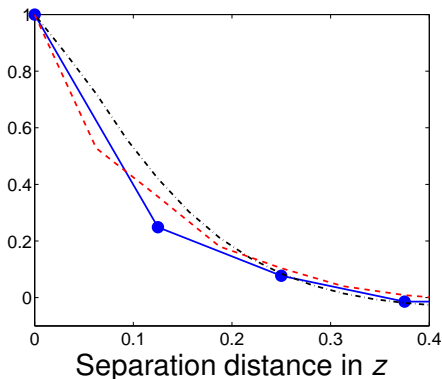
# ENERGY SPECTRA IN TIME. $x = -1$ .



## Energy spectra in time



## Two-point correlation



—  $N_z = 32$ ; - - -  $N_z = 64$ ; - . -  $N_z = 128$ .

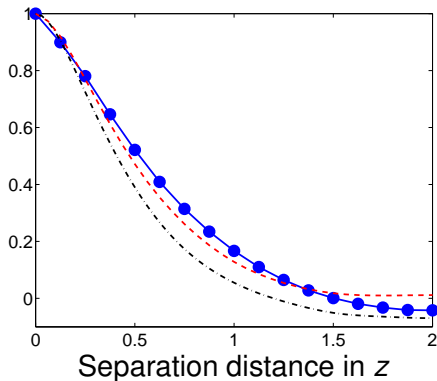
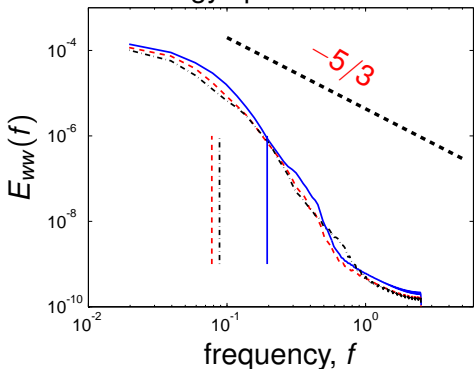
# ENERGY SPECTRA IN TIME. $x = 20$ .



Energy spectra in time

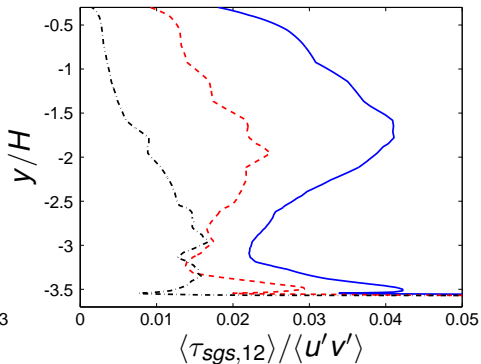
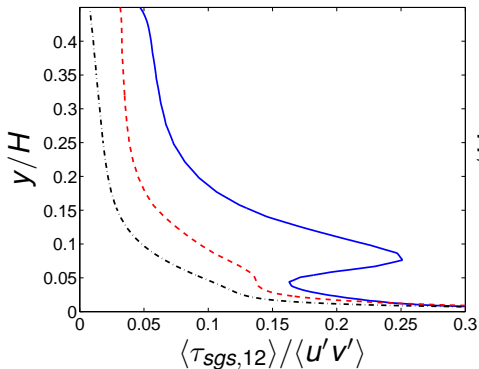
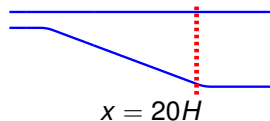
Two-point correlation

$x = 20H$



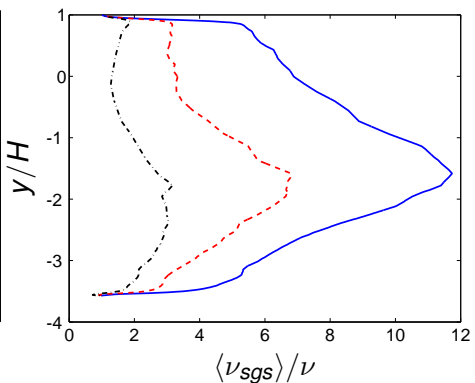
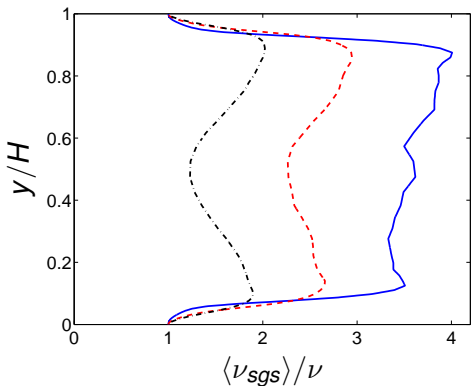
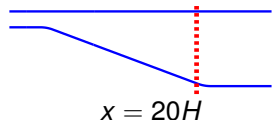
—  $N_z = 32$ ; 
 - - -  $N_z = 64$ ; 
 - - -  $N_z = 128$ .

# SGS VS. RESOLVED SHEAR STRESSES



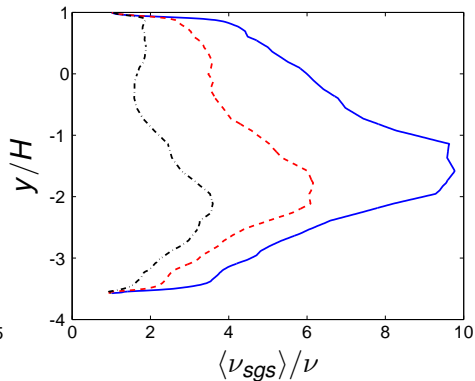
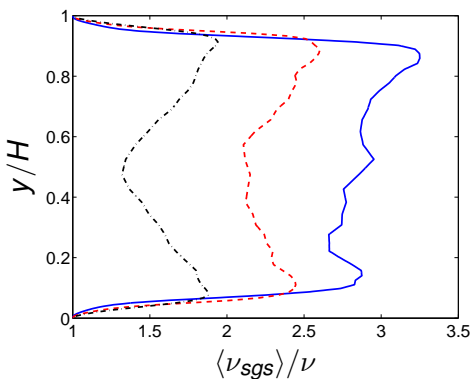
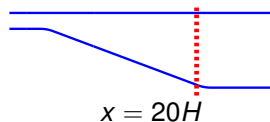
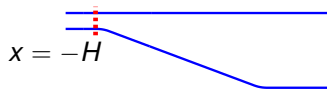
—  $N_z = 32$ ; 
 - - -  $N_z = 64$ ; 
 - . - .  $N_z = 128$ .

# SGS vs. MOLECULAR VISCOSITY



—  $N_z = 32$ ; 
 - - -  $N_z = 64$ ; 
 - · - ·  $N_z = 128$ .

# SGS vs. MOLECULAR VISCOSITY, $N_x = 512$

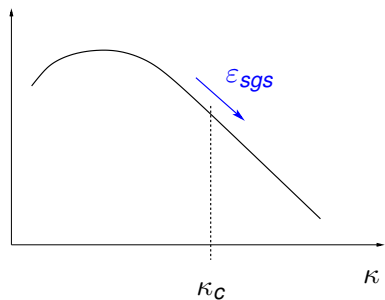


—  $N_z = 32$ ; - - -  $N_z = 64$ ; - . -  $N_z = 128$ .

# DISSIPATION ENERGY SPECTRA: THEORY VS. REALITY

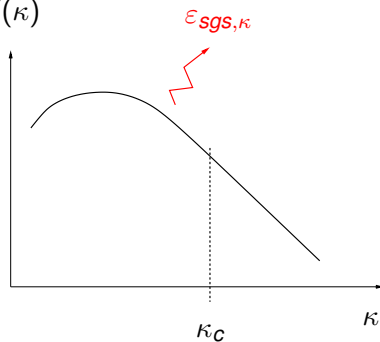
Theory

$E(\kappa)$



Reality

$E(\kappa)$



$$\epsilon_{sgs} = \int_0^{\kappa_c} \epsilon_{sgs,\kappa}(\kappa) d\kappa$$



# APPROXIMATED DISSIPATION ENERGY SPECTRA

- At which **wavenumber** is the SGS dissipation largest?
- In the **homogeneous** direction,  $z$ , the SGS dissipation can be analyzed in the **wavenumber space**
- $\varepsilon_{wz}$ , can — in theory — be obtained from the two-point correlation [5] as

$$\varepsilon_{wz} = 2\nu \left\langle \left( \frac{\partial w'}{\partial z} \right)^2 \right\rangle = 2\nu \frac{\partial^2 B_{ww}(\hat{z})}{\partial \hat{z}^2} \Big|_{\hat{z}=0} = 2\nu \sum_{k_z=1}^{N_z} \kappa_z^2 E_{ww}(k_z)$$

- When the equations are discretized, the left side  $\neq$  the right side
- The right side gives  $\varepsilon_{wz} \propto \kappa_z^2 E_{ww} = \kappa_z^2 \kappa^{-5/3} = \kappa^{1/3}$

# EXACT DISSIPATION ENERGY SPECTRA

A discrete Fourier transform of  $\partial w' / \partial z$  is formed as

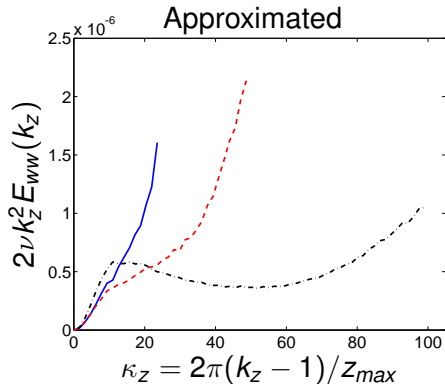
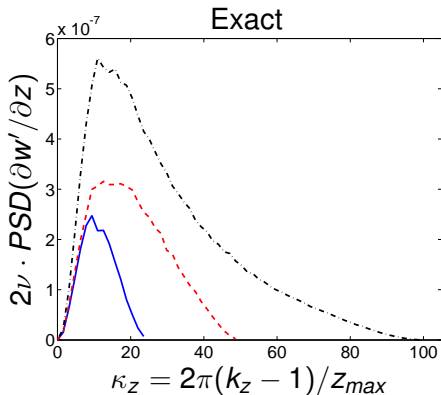
$$\hat{D}_z(k_z) = \frac{1}{N_z} \sum_{n=1}^{N_z} \frac{\partial w'(n)}{\partial z} \left[ \cos \left( \frac{2\pi(n-1)(k_z-1)}{N_z} \right) - i \sin \left( \frac{2\pi(n-1)(k_z-1)}{N_z} \right) \right] \quad (1)$$

where  $n$  is node number in  $z$  direction. Power Spectral Density (PSD)

$$\left\langle \left( \frac{\partial w'}{\partial z} \right)^2 \right\rangle = \sum_{k_z=1}^{N_z} \langle \hat{D}_z * \hat{D}_z^* \rangle = \sum_{k_z=1}^{N_z} PSD \left( \frac{\partial w'}{\partial z} \right)$$

# PREDICTED DISSIPATION ENERGY SPECTRA

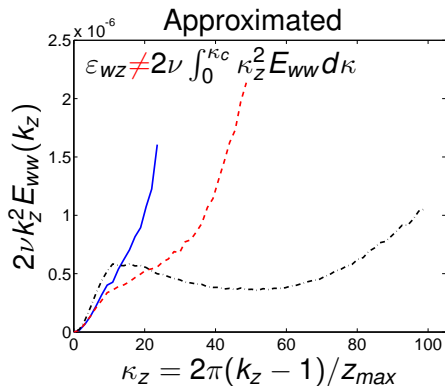
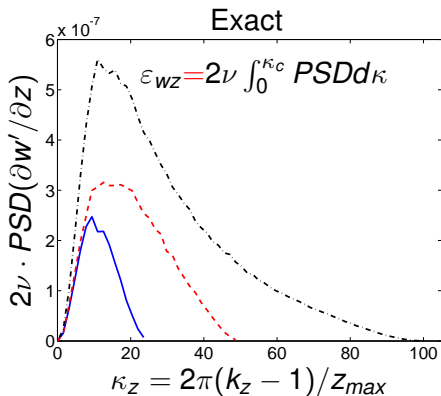
$x = -H, y = 0.15H$



—  $N_z = 32$ ; - - -  $N_z = 64$ ; - . -  $N_z = 128$ .

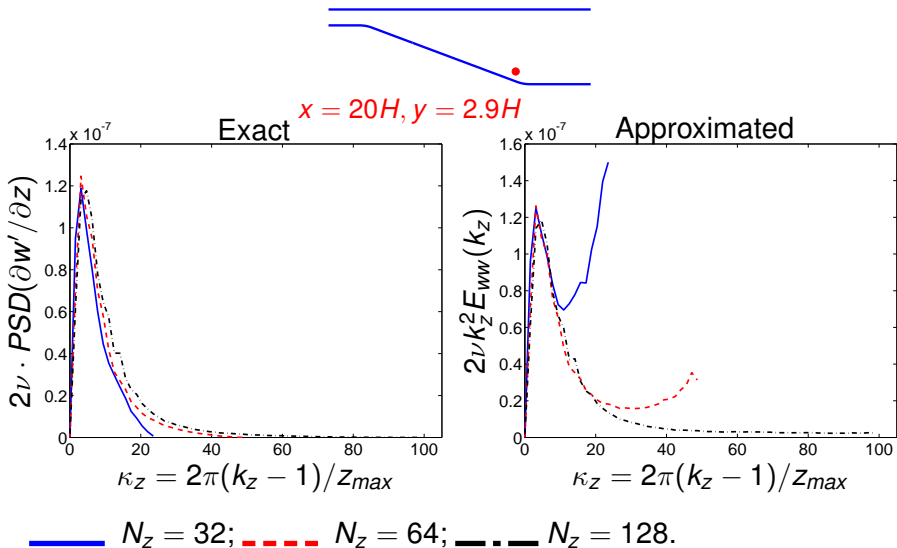
# PREDICTED DISSIPATION ENERGY SPECTRA

$x = -H, y = 0.15H$



—  $N_z = 32$ ; - - -  $N_z = 64$ ; - . -  $N_z = 128$ .

# PREDICTED DISSIPATION ENERGY SPECTRA



# SGS DISSIPATION ENERGY SPECTRA

- Above, energy spectra for  $\partial w' / \partial z$  have been presented which is part of the **viscous** dissipation
- What about energy spectra for the **SGS** dissipation

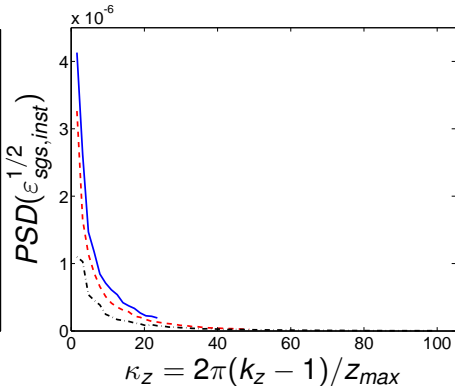
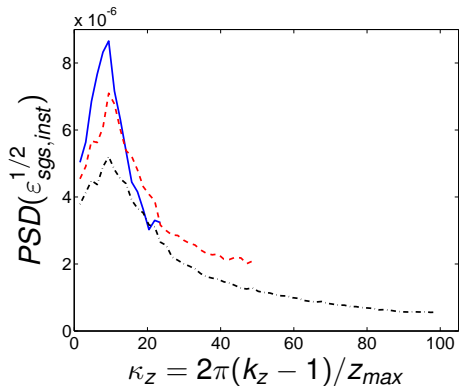
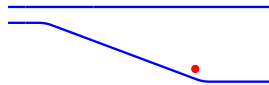
$$\varepsilon_{sgs} = \left\langle \nu_{sgs} \frac{\partial \bar{u}_i}{\partial x_j} \frac{\partial \bar{u}_j}{\partial x_i} \right\rangle \quad ?$$

- Form a discrete Fourier transform of  $\varepsilon_{sgs}^{1/2}$ . Replace  $\partial w' / \partial z$  in Eq. 1 on Slide 26 by  $\varepsilon_{sgs}^{1/2}$ .
- Strange unphysical Fourier coefficients! but the energy spectra

$$\varepsilon_{sgs} = \sum_{k_z=1}^{N_z} \langle \hat{D}_z * \hat{D}_z^* \rangle = \sum_{k_z=1}^{N_z} PSD \left( \varepsilon_{sgs}^{1/2} \right)$$

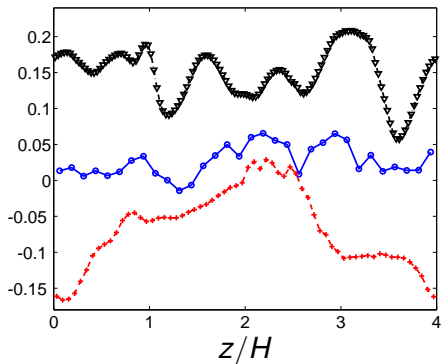
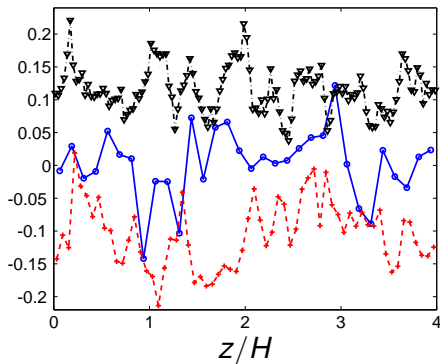
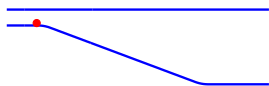
are OK

# SGS DISSIPATION ENERGY SPECTRA



—  $N_z = 32$ ; - - -  $N_z = 64$ ; - . -  $N_z = 128$ .

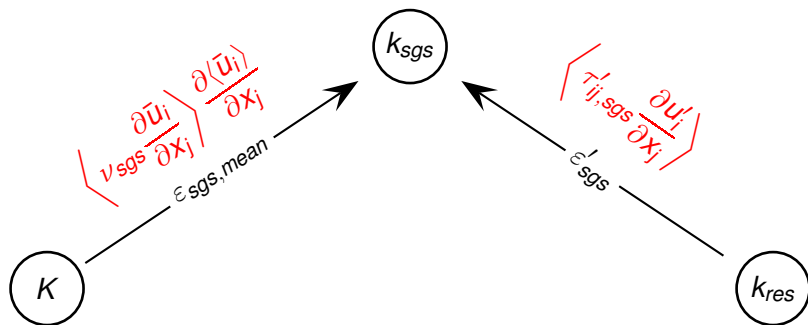
# SNAPSHOTS OF $w'$ VS. $z$



———  $N_z = 32$ ; 
 - - - -  $N_z = 64, w' - 0.1$ ; 
 - · - · -  $N_z = 128, w' + 0.14$ .

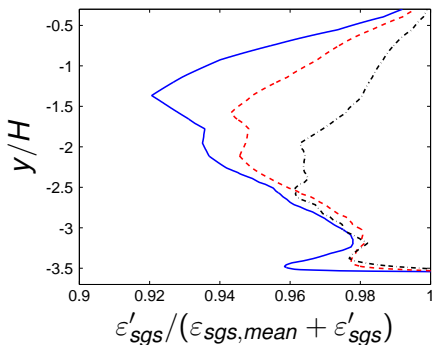
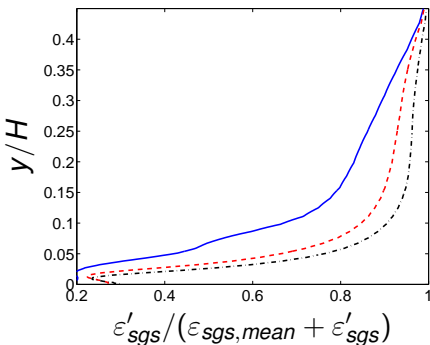


# TRANSFER OF KINETIC TURBULENT ENERGY



- time-averaged  $K = \frac{1}{2} \langle \bar{u}_i \rangle \langle \bar{u}_i \rangle$  (**RANS**)
- resolved  $k_{res} = \frac{1}{2} \langle u'_i u'_i \rangle$  (**RANS** and **LES**)
- SGS kinetic energy,  $k_{sgs}$ .

# RATIO OF SGS DISSIPATION



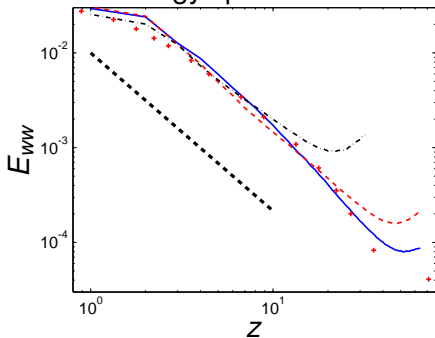
—  $N_z = 32$ ; - - -  $N_z = 64$ ; - . -  $N_z = 128$ .

# DECAYING GRID TURBULENCE

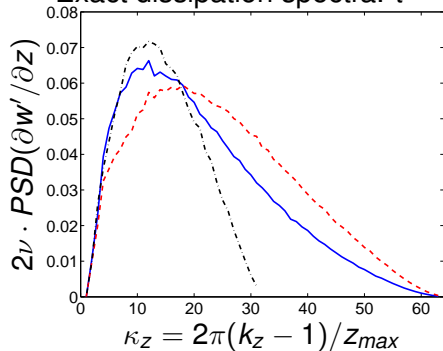
- Diffuser flow: peaks in  $\partial w'/\partial z$  at **surprisingly** low wavenumbers.
- The “**decaying grid turbulence**” is presented below in order to find at which wavenumbers the dissipation attain its peak
- The domain is a **cubic box** of side  $2\pi$ . Three computations have been carried out.
  1. **Fine LES** using a Smagorinsky model ( $C_S = 0.1$ ) on a  $128^3$  grid.
  2. **DNS** on a  $128^3$  grid.
  3. **Coarse LES** using a Smagorinsky model ( $C_S = 0.1$ ) on a  $64^3$  grid.

# DECAYING GRID TURBULENCE: RESULTS

Energy spectra.  $t = 2$



Exact dissipation spectra.  $t = 2$



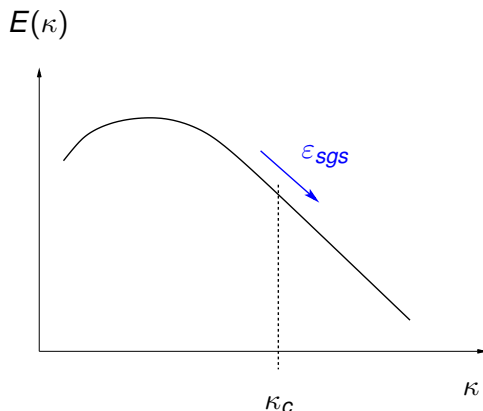
— Fine LES; - - - DNS; . . . coarse LES; + exp. [6].

# CONCLUSIONS

- **Two-point** correlation **best**. They show by how many cells the largest scales are resolved.
- The **energy spectra** do **not** give any reliable information on the resolution.
- The  $\langle \nu_t / \nu \rangle$  is not a good measure. It compares LES with DNS.
- $\langle \tau_{sgs,12} \rangle / \langle u'v' \rangle$  is a good measure. However, it is difficult to give any **quantitative** guidelines.
- Ratio of  $\varepsilon'_{sgs} / \varepsilon_{sgs,mean}$  useful but difficult to give any **quantitative** guidelines.

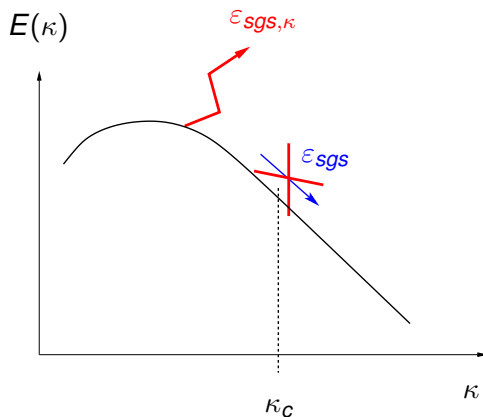
## CONCLUSIONS CONT'D

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