



FLOW AROUND A THREE-DIMENSIONAL BLUFF BODY

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ABSTRACT

Large Eddy Simulation (LES) is used to compute the flow around a sharp-edged surface-mounted cube. Different visualization techniques were used, and the results of these are presented. Since Large Eddy Simulation is a time-dependent three-dimensional numerical technique, it allows visualization that is unattainable in RANS (Reynolds Averaged Navier Stokes) methods or experiments.

1 INTRODUCTION

Large Eddy Simulation is a numerical method that results in a three-dimensional time-dependent solution. With the increases in computer power in the last ten years, this technique has grown rapidly and is used in high Reynolds number flows and more complex geometries. While the technique is intended for accurate predictions of statistics, a qualitative picture of instantaneous flow can also be obtained.

One area of application for LES is the wake behind a three-dimensional bluff body. The physics of such a wake is not possible to predict with RANS methods because of the unsteady nature of wakes. These unsteadiness can easily be captured using the LES technique as is shown in this work. A movie can be made using the instantaneous data obtained from LES, making it possible to study the flow in detail.

2 COMPUTATIONAL DETAILS

The Reynolds number was $Re = U_b H / \nu = 40000$ based on the incoming mean bulk velocity, U_b , and the obstacle height, H . The cube is located between $x = 0$ and $x = 1$, and the channel height is $h = 2H$ (see Fig. 1). A computational domain with an upstream length of $x_1/H = 3$ and a downstream length of $x_2/H = 6$ was used, while the span-wise width was set to $b/H = 7$. Even though the geometry of the flow configuration is rather simple, the flow is physically quite complex, with multiple separation regions and vortices. A mesh of $82 \times 50 \times 66$ nodes was used. Near the walls of the cube, $y_{min}^+ = 3.7$, while, on the top of the cube, $y_{min}^+ = 5.2$. The time step was set to 0.02, which gave a maximum CFL number of approximately 2.

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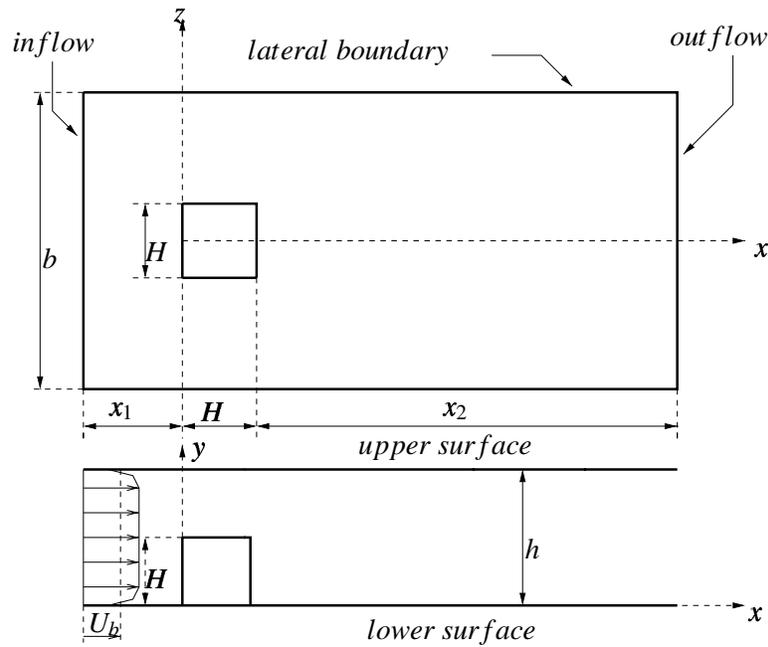


Fig. 1 Geometry of the computational domain.

2.1 Boundary Conditions

The experimental profile (constant in time) was used at the inlet. The lateral boundaries were treated as slip surfaces. At the downstream boundary, convective boundary condition $\frac{\partial u_i}{\partial t} + c \frac{\partial u_i}{\partial x} = 0$ was used. Here, c is the mean bulk velocity, U_b . No-slip conditions were used at the upper and lower surfaces.

3 VISUALIZATION TOOLS

EnSight 6.2.2 post-processing program was used for the visualizations. The interface between the solver used for the LES calculation and EnSight 6.2.2 was written by the authors. This program enabled the authors to visualize many features of the flow using different techniques discussed below. A number of movies were made showing the unsteadiness in the flow.

4 RESULTS OF THE VISUALIZATIONS

Various visualization techniques were used in this work. Among them are:

1. streamlines
2. velocity vector planes
3. isosurfaces of pressure and surface pressure
4. isosurfaces of second invariant of the velocity gradient Q defined as

$$Q = -\frac{1}{2} \frac{\partial \bar{u}_i}{\partial x_j} \frac{\partial \bar{u}_j}{\partial x_i} = -\frac{1}{2} (\bar{S}_{ij} \bar{S}_{ij} - \bar{\Omega}_{ij} \bar{\Omega}_{ij}) \quad (1)$$

where $\bar{\Omega}_{ij}$ is the anti-symmetric part of the resolved velocity gradient tensor.

5. particle traces

4.1 Streamlines

Streamlines are used to visualize separations and re-attachments in the mean in front of, on the top of, at the lateral sides and behind the cube (see Fig. 2). In Fig. 2a, there is a horseshoe vortex in front of the cube and recirculation regions on the top and behind the cube. The node point in the shear layer of the recirculation region behind the cube is also visible. The technique of streamlines was also used in comparisons with oil-film visualization by Martinuzzi and Tropea, which can be found in Ref. [4]. Streamlines of the mean flow are projected onto the channel floor in Fig. 2b.

All flow features from oil-film visualization in Ref. [4] are also visible here (see Fig. 2b). There are two recirculation regions with their foci on the lateral sides of the cube. A pair of vortices behind the cube is clearly visible. The saddle point in front of the cube is followed by the horseshoe vortex. A node point and two foci can be seen behind the cube. Streamlines in Fig. 3a show vortices generated within the shear layer on the top and the lateral sides of the cube. The position of the lateral vortex at the junction of the channel floor and the cube is visualized using streamlines in Fig. 3b. The multiple vortex system on the top of the cube is visualized using streamlines projected from the line at $x = 0.4$ and $y = 1.1$ in Fig. 4a. In the mean, these vortices form two cone-like structures with their base close to position $z = 0$, $y = 1.1$ and their nibs attached on the top of the cube near the lateral sides (see Fig. 4a). Both vortices behind the cube are visualized using streamlines coloured with velocity magnitude in Fig. 4b. Studying Fig. 4b, it was found that the axes of the back vortices are tilted with respect to the vertical axes.

Hunt et al. [1] observed the exchange of the fluid between the separation regions. From this, they concluded that the separation region in the flow around a three-dimensional bluff body cannot be closed. To arrive at this conclusion, they used a surface oil-film visualization. Their results are confirmed in Fig. 5a. In this figure, streamlines are produced from line-tool at $x = 0.5$, $z = -0.55$. Two velocity vector planes at $x = 0.5$ and $x = 1.5$ were also plotted in this figure. It can be seen how the streamlines stretch from the lateral to the back vortices, showing the exchange of the fluid between vortices.

4.2 Velocity vector planes

Velocity vector planes are used in identifying the coherent structures. The position of the horseshoe vortex on the lateral side of the cube is shown in Fig. 5b. This was compared with the results of Hussein and Martinuzzi in Ref. [2]. The position of the horseshoe leg along the plane $x/H = 1.75$ equal $z/H \approx 1.7$ was registered from the results of Large Eddy Simulation, while the position of the horseshoe leg $z/H \approx 1.25$ was measured in the experiment. This difference is addressed in Ref. [3].

The cone-like vortices are visualized using mean velocity vectors in plane $y = 1.02$ in Fig. 6a. These vectors are coloured with velocity magnitude. The secondary corner vortex behind the cube is visualized using the same technique in Fig. 6b. Additional information on the shape of this vortex is obtained here using isolines of the vorticity.

Lateral vortices are also studied using velocity vector planes. One of these lateral vortices is shown in Fig. 7a as a time-averaged velocity vectors in plane $z = -0.55$. There is a focus at approximately 80% the cube height. This focus is correlated with attachment of the streamlines in Fig. 3b on the lateral side of the cube.

Velocity vectors coloured with velocity magnitude in planes $z = 0$ and $y = 0.02$ are shown in Fig. 3a. Both separation regions on the top and behind the obstacle with their foci are clearly visible in vector plane $z = 0$. Velocity vectors in plane $y = 0.05$ are plotted in Fig. 7b. Two vortices with their foci are visible in this figure. A stagnation point at the rear face of the cube is also visible. Three time-averaged velocity planes are plotted in Fig. 8. The change in position of the foci again indicates tilting of two back vortices.

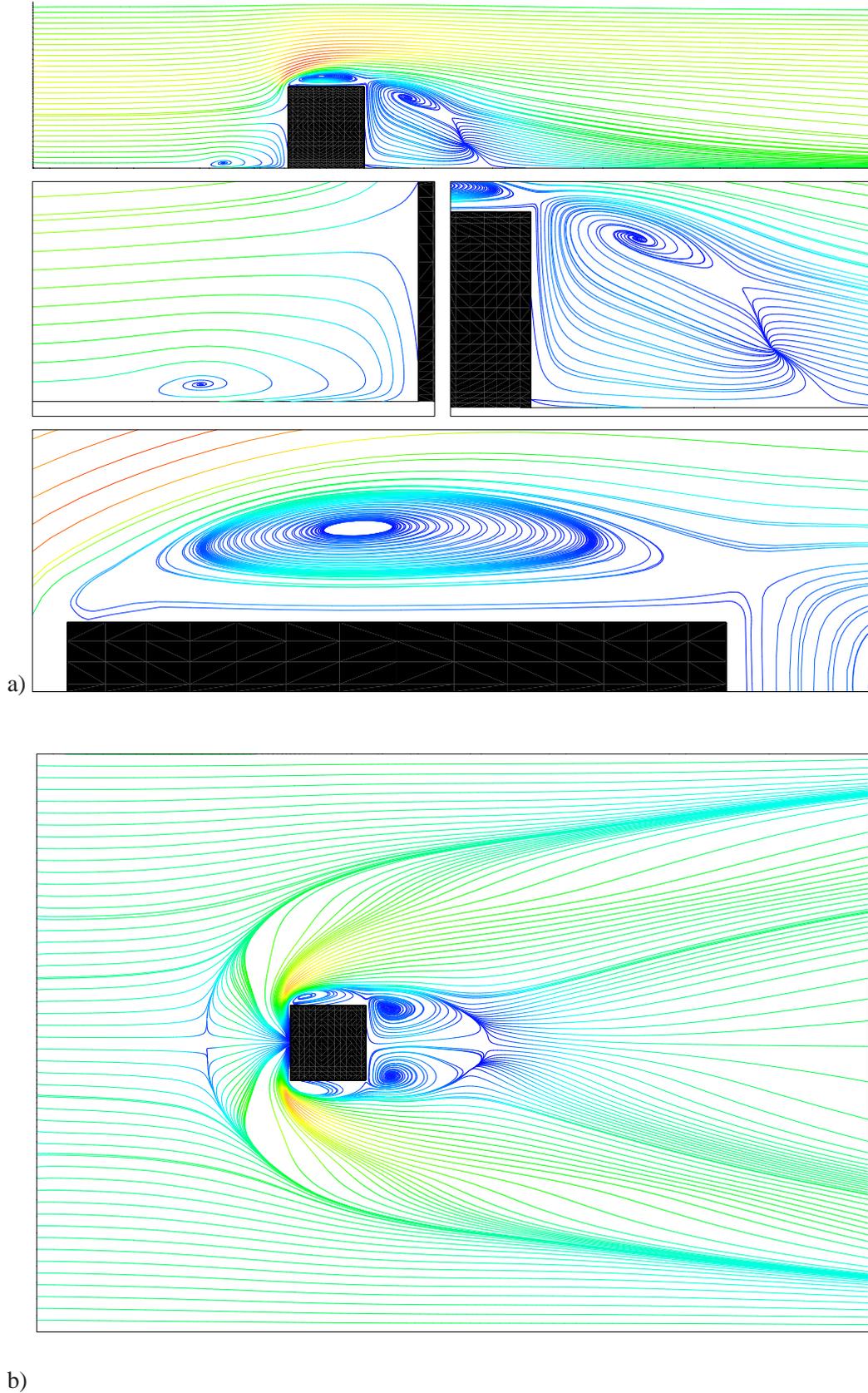


Fig. 2 Streamlines of the mean flow projected onto: a) the center-plane of the cube; b) the channel floor.

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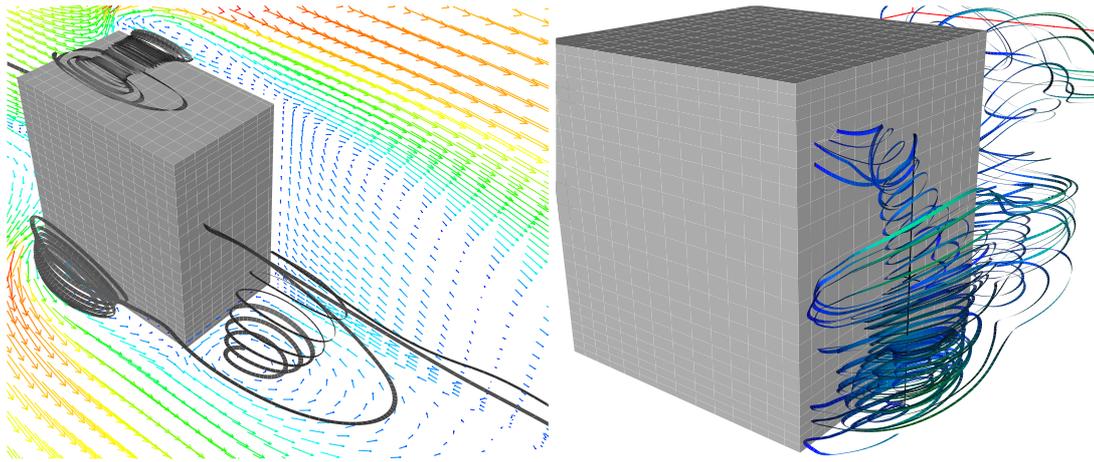


Fig. 3 a) Vortices generated within the shear layer. b) Time averaged streamlines showing the lateral vortex.

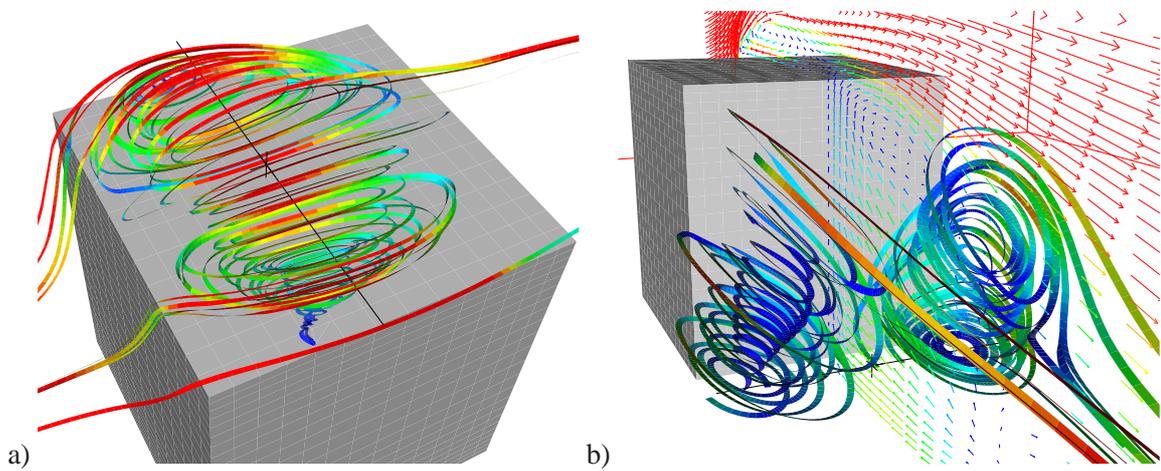


Fig. 4 a) Time-averaged streamlines on the top of the cube. b) Time-averaged streamlines behind the cube. Time-averaged velocity plane $z = 0$

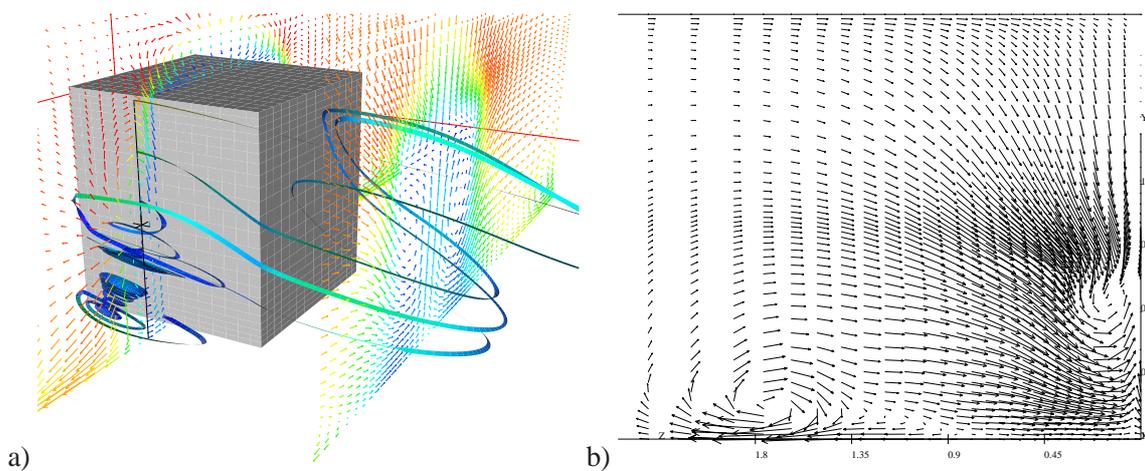


Fig. 5 a) Exchange of the fluid between lateral and back vortices; b) Time-averaged velocity field along the plane $x/H = 1.75$.

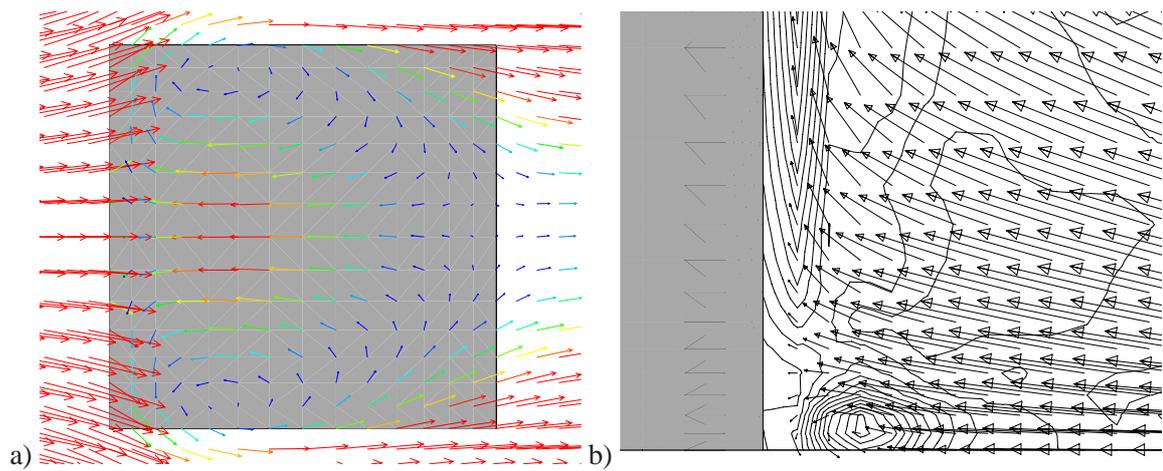


Fig. 6 a) Mean velocity vectors in plane $y = 1.02$; b) Time-averaged velocity vectors and vorticity isolines in plane $z = 0$, showing the secondary vortex behind the cube.

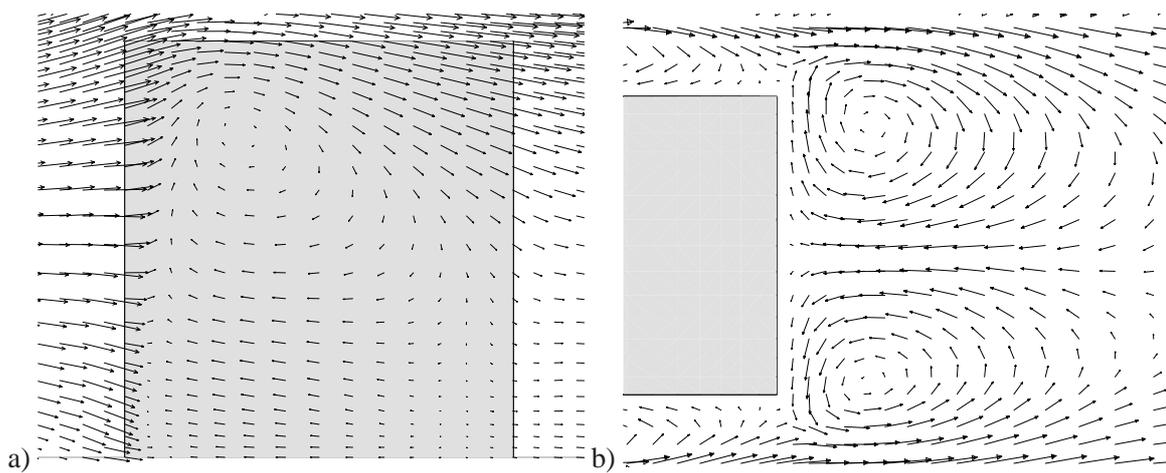


Fig. 7 a) Time-averaged velocity vectors in plane $z = -0.55$; b) Time-averaged velocity field in plane $y = 0.05$.

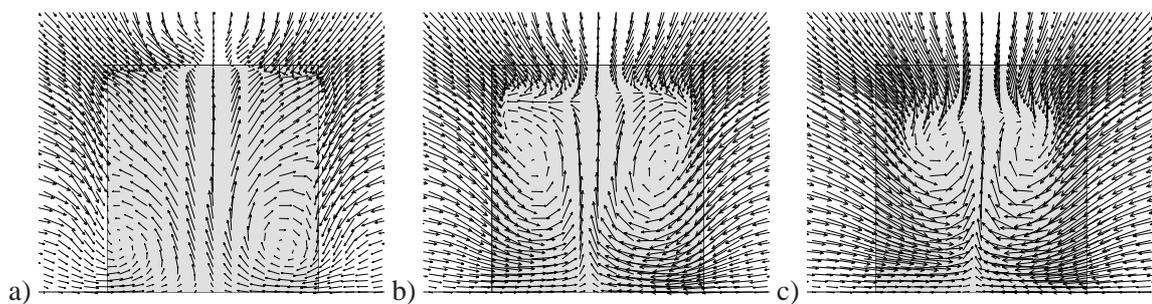


Fig. 8 Time-averaged velocity field in plane: a) $x = 1.3$, b) $x = 1.5$ and c) $x = 1.7$.

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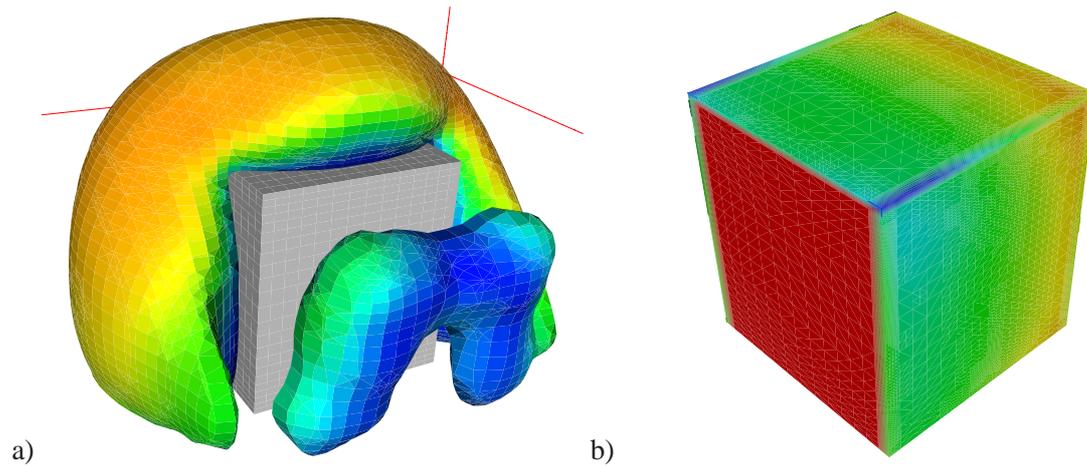


Fig. 9 a) Pressure isosurface $p = -0.22$. View of downstream face of the cube; b) Mean surface pressure.

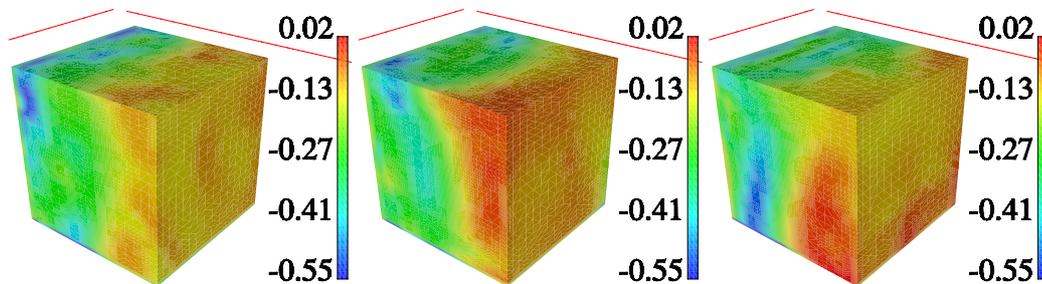


Fig. 10 Surface pressure with three different times.

4.3 Isosurfaces of pressure and surface pressure

It has been found that isosurfaces of pressure are useful in visualizing large-scale coherent structures. The isosurface of time-averaged pressure $p = -0.22$ is shown in Fig. 9a. Two vortices behind the cube join at the symmetry plane in this figure. The same was found in the experiments by Martinuzzi and Tropea [4]. Surface pressure was studied both in the mean in Fig. 9b and instantaneously in Fig. 10. It was found that the surface pressure both in the wake and on the top and lateral sides of the body is highly oscillating in Fig. 10.

4.4 Isosurfaces of second invariant of the velocity gradient, Q

It was found that technique of isosurfaces of Q defined in Eq. 1 is superior for identifying coherent structures to the technique of isosurfaces of vorticity. This method was used both for the mean flow in Fig. 11a and for instantaneous flow in Figs. 11b and 12. The isosurfaces of Q are coloured with velocity magnitude in these figures. In Fig. 11a, both a horseshoe vortex and a secondary corner vortex in front of the cube are visible. It was possible to follow the lifespan of lateral vortices from formation close to the front vertical corner of the obstacle in Fig. 12a to the breakdown close to the rear vertical corner of the obstacle in Fig. 12b.

The multiple vortex system on the top of the cube was also observed using this technique in Fig. 12. The vortices forming this system were followed in a similar way as in lateral vortices. Using the same technique, very long vortex structures were observed in the wake region in Fig. 11b.

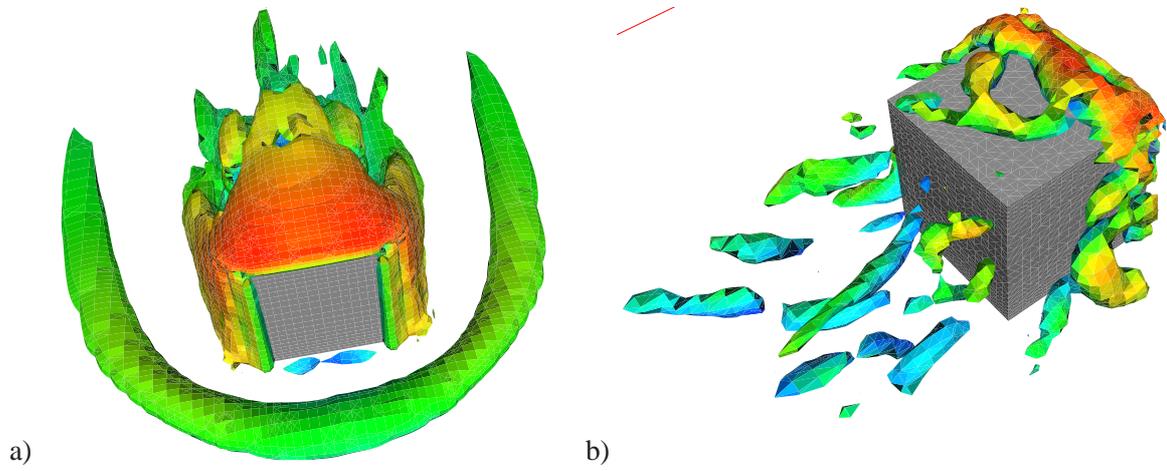


Fig. 11 a) Time-averaged second invariant of the velocity gradient $Q = 0.18$; b) Instantaneous $Q = 5$. View of downstream face of the cube.

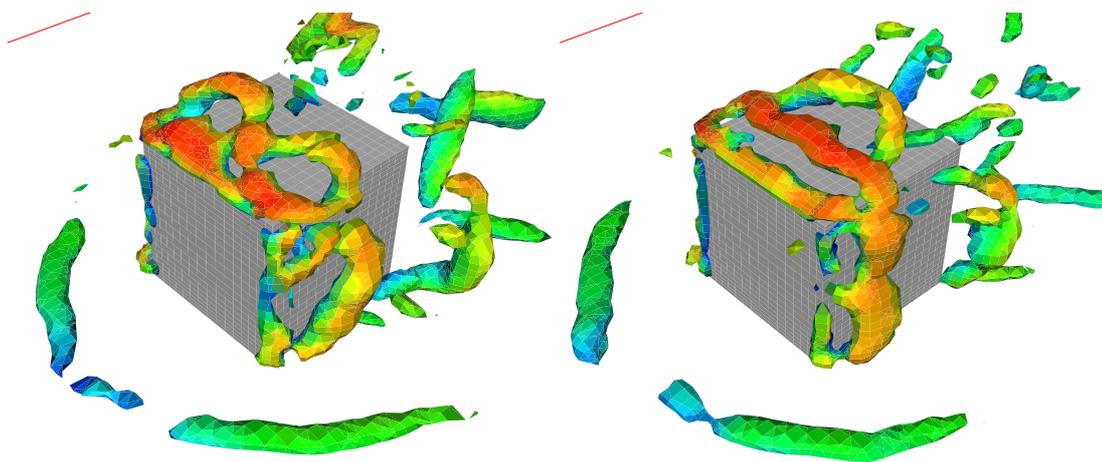


Fig. 12 Instantaneous second velocity invariant $Q = 5$ coloured with velocity magnitude for two time steps.

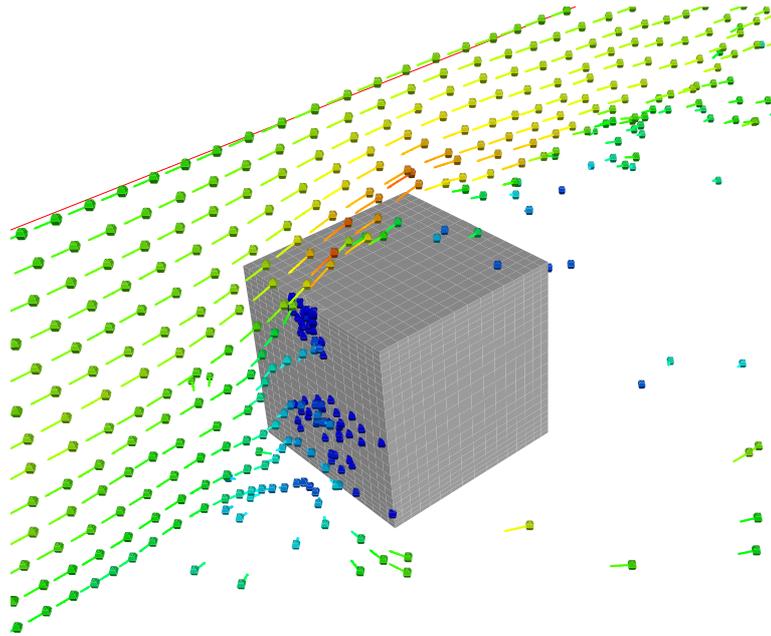


Fig. 13 Simulated hydrogen bubbles. Numerical bubbles are produced from line tool at $x = -2.8$, $z = 0$.

4.5 Particle traces

In Large Eddy Simulation, results are obtained in the entire computational domain and for each time step. This can be compared with experiments in which researchers are often limited in making measurements at only one point, along a line or a plane.

This enormous amount of data obtained from LES can be used to simulate some of the experiments. One experiment simulated in this work was an experiment with hydrogen bubbles (see Fig. 13). In a traditional experiment, researchers put a wire in the flow at only a few positions in order to produce hydrogen bubbles. These bubbles are then convected downstream, visualizing the flow. Here, the authors were able to put a line-tool ('wire') in the flow at any interesting position and then produce particle traces like those shown in Fig. 13. Numerical 'hydrogen bubbles' have an infinite life compared with those in a real-life experiment. They also have the same density as a surrounding fluid, giving a more realistic picture of the flow than the real-life experiment with hydrogen bubbles. Using this technique it was possible to see how some of the 'numerical bubbles' lose their kinetic energy and attach onto the front face (see Fig. 13) and on the rear face of the obstacle.

5 CONCLUSIONS

Results from Large Eddy Simulation are used for visualization of the flow around a three-dimensional bluff body. Different techniques for visualization were used, giving very good results. Many aspects of this flow were studied here, and all flow features obtained in the experiments in Ref. [4] were observed in this work. It was shown that real-life experiments can be simulated from data obtained in Large Eddy Simulation. With increases in storage resources and computational power, this technique will be used more frequently and for computationally more demanding flows in the future.

6 ACKNOWLEDGMENT

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