

Since  $f_k = 0.4$ , it means that the turbulent diffusion in the  $k$  and  $\varepsilon$  equations are  $1/0.4^2 \simeq 6$  times larger in [168] than in [203]. The consequence is that peaks in  $k$  and  $\varepsilon$  (and also  $\nu_t$ ) are reduced in the former case compared to the latter (this is the physical role played by diffusion: it transports  $k$  from regions of high  $k$  to regions of low  $k$ ). This explains why the peaks of  $k$  are much larger in [203] compared to in [168].

Hence, in the original PANS model (Eq U.3), the RANS turbulent viscosity appears in the turbulent diffusion of  $k$  (and  $\varepsilon$ ), because the turbulent diffusion term reads (recall that  $f_k = k/k_{total} = k/k_{RANS}$  where  $k_{RANS}$  denotes the turbulent kinetic energy in a RANS simulation)

$$\begin{aligned} \frac{\partial}{\partial x_j} \left( \frac{\nu_t f_k^2}{1.4} \frac{\partial k}{\partial x_j} \right) &= \frac{\partial}{\partial x_j} \left( \frac{c_\mu k^2}{\varepsilon f_k^2 1.4} \frac{\partial k}{\partial x_j} \right) \\ &= \frac{\partial}{\partial x_j} \left( \frac{c_\mu k_{RANS}^2}{\varepsilon 1.4} \frac{\partial k}{\partial x_j} \right) = \frac{\partial}{\partial x_j} \left( \frac{\nu_{t,RANS}}{1.4} \frac{\partial k}{\partial x_j} \right) \end{aligned} \quad (\text{U.5})$$

cf. Eqs. 18 and 19 in [144]. Thus the *total* (i.e. RANS) viscosity is responsible for the transport of the *modeled* turbulent kinetic energy.

#### U.4 Location of interface in DES and DDES

The results analyzed above were from LES simulations [168,203] (i.e. the PANS model was used in LES mode). Now we will analyze results from Zonal PANS [164] where the interface is prescribed along a fixed grid line (No  $j = 32$ ). Let's compare that with DES and DDES. Load the file `vectz_zonal_pans.dat` in `pl_vect_hump.m`. Recall that  $\Delta z = 0.2/32$  (note that in [168,203]  $\Delta z = 0.2/64$ )

In SA-DES, the interface is defined as the location where the wall distance is equal to  $C_{DES}\Delta$  where  $\Delta = \max\{\Delta_x, \Delta_y, \Delta_z\}$ , see Eq. 20.3. How does this compare with gridline number  $j = 32$ ? Compare the DES lengthscale,  $C_{DES}\Delta$ , with the lengthscale of PANS, i.e.

$$\ell_{PANS} = C_\mu^{3/4} \frac{k_{total}^{3/2}}{\varepsilon} \quad (\text{U.6})$$

see Eq. 12 in [168]

In SST-DES, the location of the interface is computed using  $k$  and  $\omega$ . Compute  $\omega$  from  $\varepsilon/(\beta^*k)$  and compute the location using Eq. 20.8. How does the location compare with gridline  $j = 32$  and SA-DES?

In DDES, the boundary layer is shielded with a damping function. In SST-DES, the shielding function (see Eq. 20.9) may be one of the blending functions,  $F_1$  or  $F_2$  (see Eq. 20.5). Let's use  $F_2$  as the shielding function as in [78]. Does DDES work, i.e. does it make the model to be in RANS mode in the entire boundary layer? What about the separation region?

#### U.5 Compute $f_k$

The function  $f_k$  is used in the PANS model. see Section 23. In [168,203],  $f_k = 0.4$  in the entire domain. In the Zonal PANS simulations [164],  $f_k = 0.4$  in the LES region or it is computed from Eq. U.7; in the RANS region near the lower wall  $f_k = 1$  (interface at grid line No  $j = 32$ ). The expression for computing  $f_k$  reads [209]

$$f_k = c_\mu^{-2/3} \frac{\Delta}{L_t}, \quad L_t = \frac{k_{total}^{3/2}}{\langle \varepsilon \rangle} \quad (\text{U.7})$$