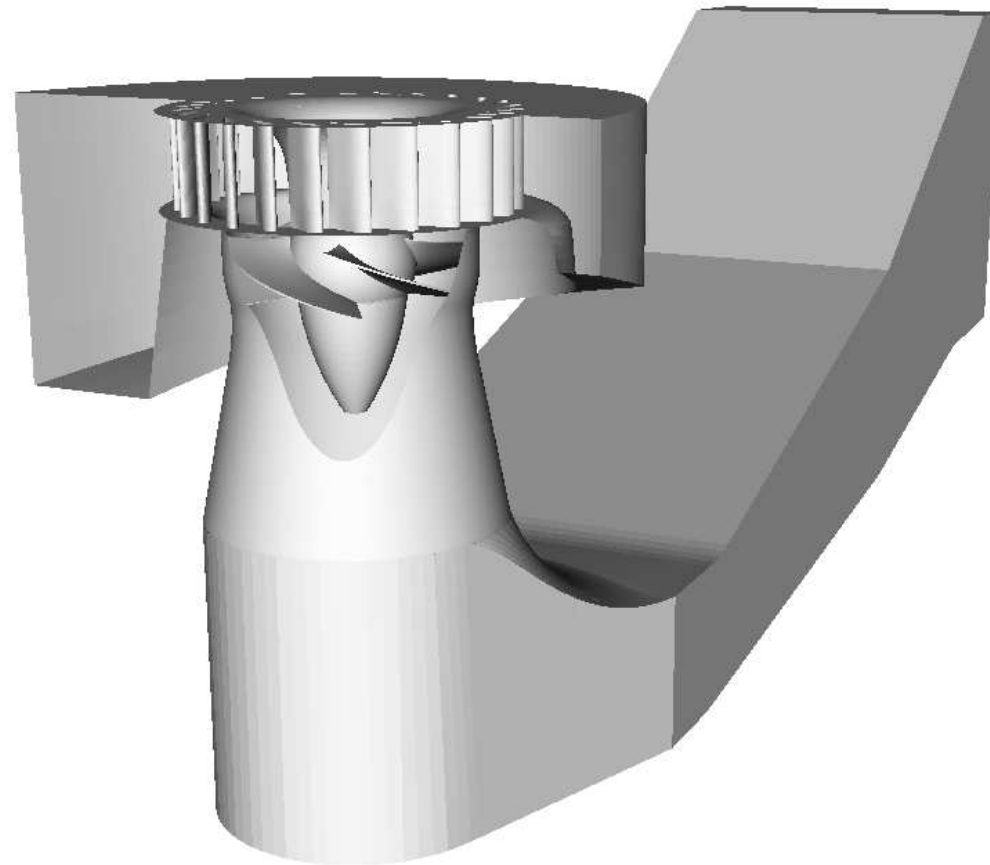


OpenFOAM SIMULATION OF THE FLOW IN THE HÖLLEFORSSEN DRAFT TUBE MODEL

Nilsson H. and Page M.
Chalmers / Hydro Quebec



The OpenSource OpenFOAM CFD solver

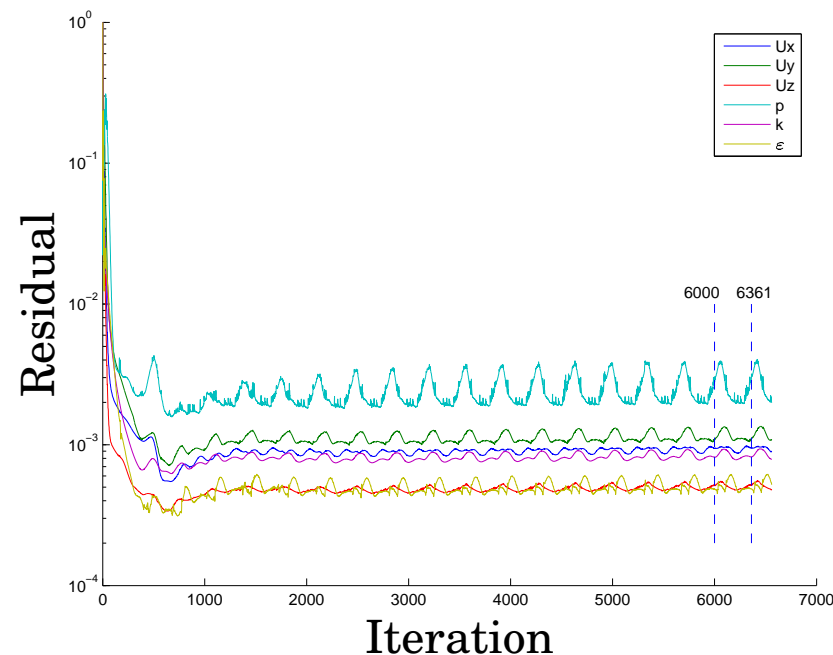
- OpenFOAM = Open Field Operation and Manipulation, www.openfoam.org
An OpenSource object oriented C++ tool for solving PDE's
- Preprocessing (grid generator, converters, manipulators, case setup)
- Postprocessing (using OpenSource Paraview)
- Many specialized CFD solvers implemented, e.g.
 - simpleFoam: A finite volume steady-state solver for incompressible, turbulent flow of non-Newtonian fluids, using the SIMPLE algorithm
 - turbFoam: A finite volume solver for unsteady incompressible, turbulent flow of non-Newtonian fluids, using the PISO algorithm
 - icoTopoFoam: Sliding grid
- OpenSource = possibility to have insight into the code
 - * Makes development and tailor-made solvers possible
 - simpleUnsteadyFoam: Unsteady SIMPLE solver
 - cavInterFoam: Cavitation using VOF and the Kunz' cavitation model
 - * Makes research implementations available and results reproducible.
- Access to an international community of OpenFOAM users
- Runs in parallel using automatic/manual domain decomposition.

Studied case

- Case 1: Steady calculation
- Prescribed wall-function grid, 1,002,360 grid points.
- Standard $k - \varepsilon$ turbulence model with wall-functions
- Axi-symmetric inlet boundary conditions using linear interpolation of the measurements (velocities multiplied by a factor of 1.07 to get the correct volume flow), $k = 1/2(\overline{u^2} + \overline{v^2} + \overline{w^2})$, $\varepsilon = C_\mu^{3/4} k^{3/2} / l_{turb}$, $C_\mu = 0.09$, $l_{turb} = 0.1 * (R_{wall} - R_{cone})$
- Homogeneous Neumann b.c. at the outlet for velocity, k and ε . Back-flow values of $k = 0.4$ and $\varepsilon = 3.55$ whenever needed (derived from the inlet average).
- The pressure had a homogeneous Neumann boundary condition everywhere except at the outlet, where it was set to zero.
- No surface roughness used.
- Gamma discretization scheme. A smooth and bounded blend between the second-order central scheme and the first-order upwind scheme.

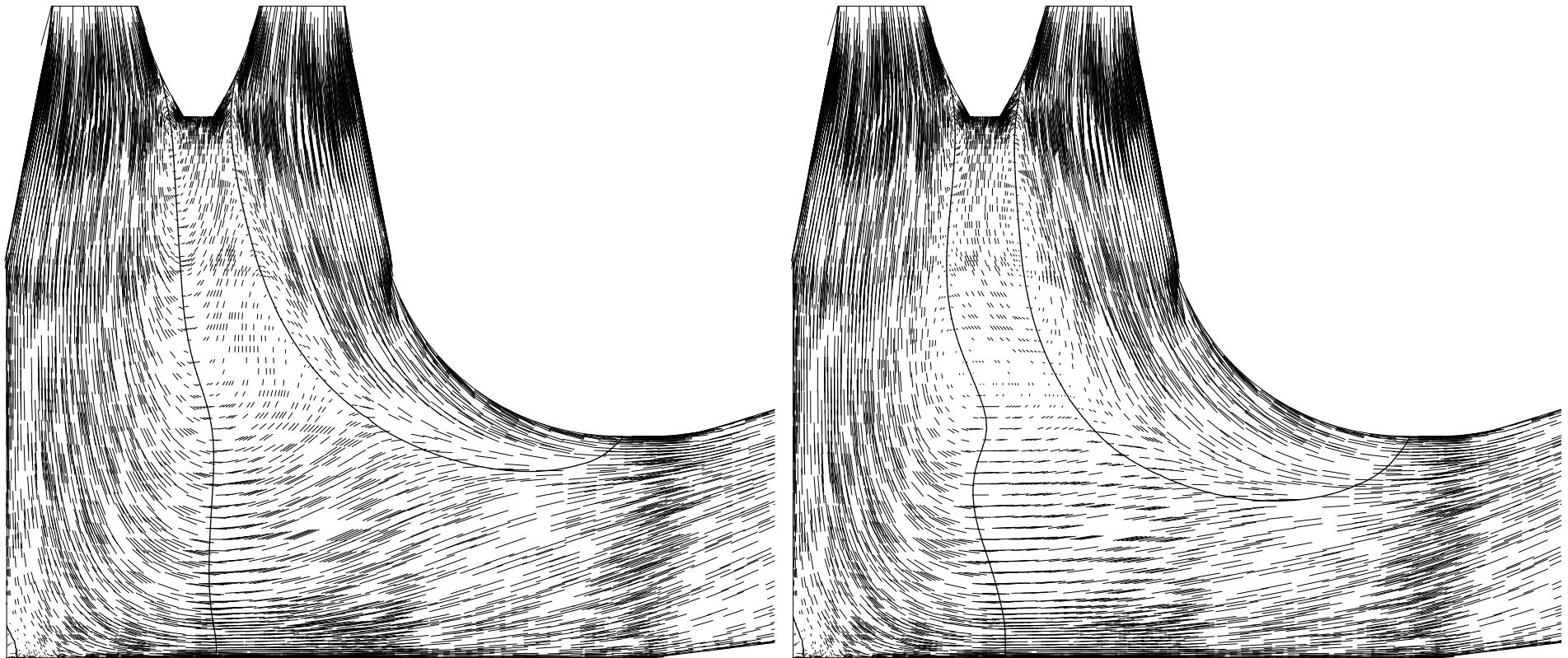
Convergence

- The residuals drop rapidly in the initial phase of the computation, but are then oscillating in a periodic fashion about a mean level.
- Inherent unsteadiness in the flow makes a steady solution impossible with the present level of diffusion (turbulence and numerical).
- One period in the fluctuating residuals correspond to one period in the vortex rope.
- Chosen averaging interval shown with dashed lines, yielding the 'quasi-steady' solution that is presented in the present work.



Unsteadiness

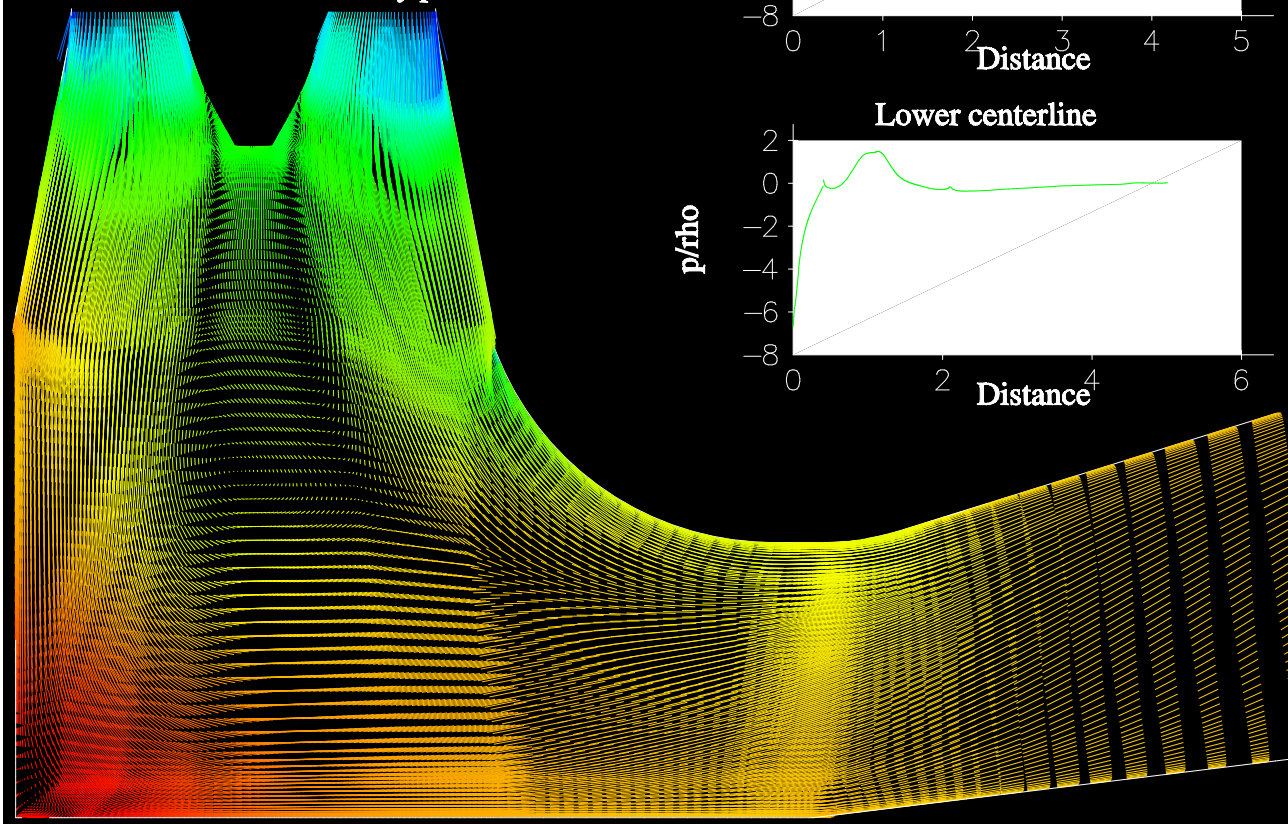
- Two snapshots of the flow to show the magnitude of the flow oscillations. The solid lines are where the vertical velocity is zero.



Unsteadiness, the movie

The Turbine-99 draft tube
OpenFOAM results
'quasi-steady' $k-\epsilon$
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Vectors colored by $p/\rho h_0$

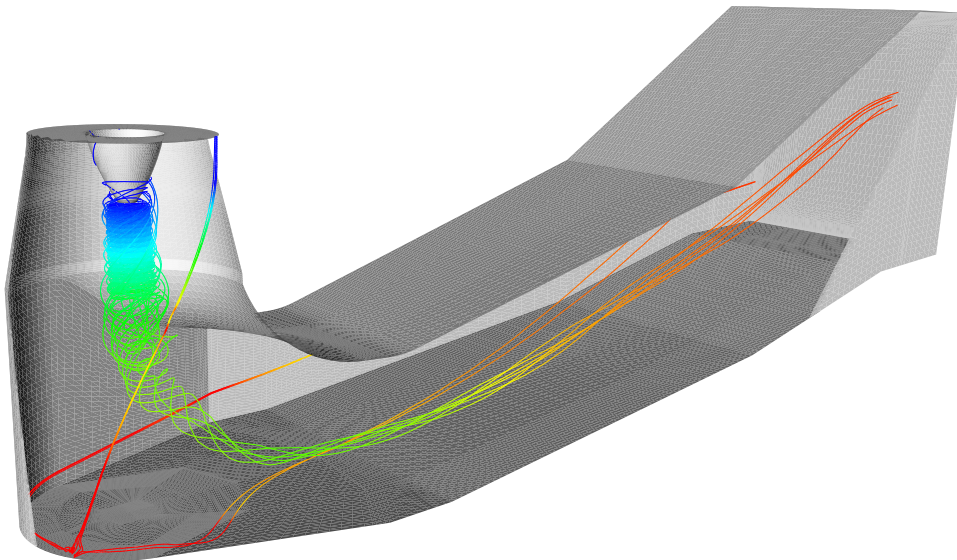


Computational time and parallel performance

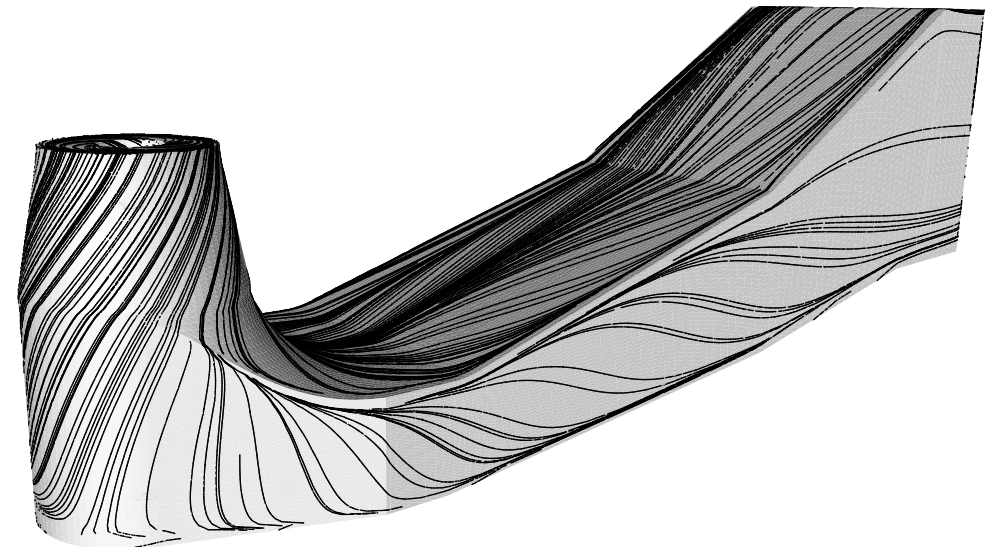
- 15s wall time (including some output) and 7s CPU time per iteration
- 10 CPU's on a dual node AMD Opteron cluster with 2.2GHz CPU's, 500MB RAM/CPU, 1MB cache/CPU and a 100Mbps Ethernet network.
- Default settings used in OpenFOAM \implies The parallel efficiency could be improved.

Computational results

- The results are very similar to CFX-5 results by Page et al.
- y^+ range $2 \leq y^+ \leq 150$ ($\overline{y^+} \approx 30$)
- $C_{pr} = 1.0171$ (pressure recovery factor)
- $C_{prm} = 0.9027$ (mean pressure recovery factor)
- $\zeta = 0.173$ (energy loss coefficient)



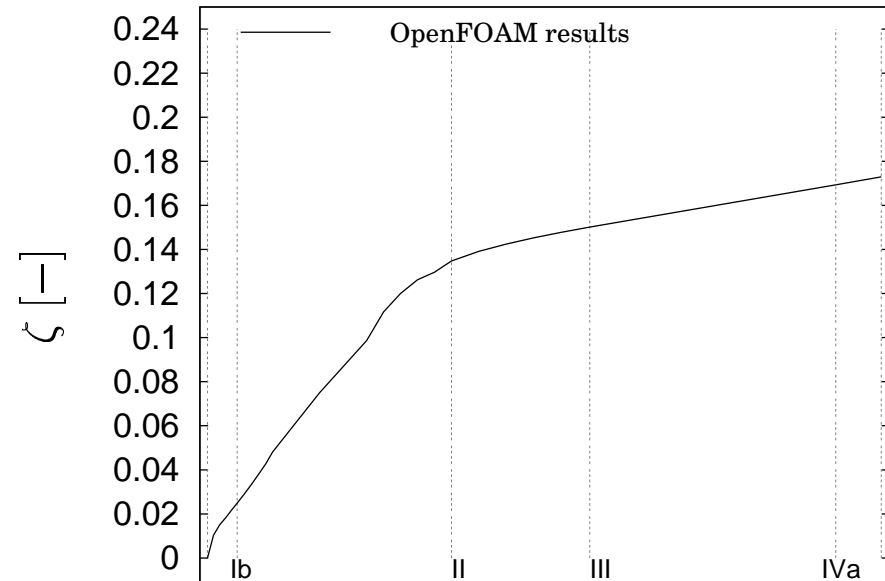
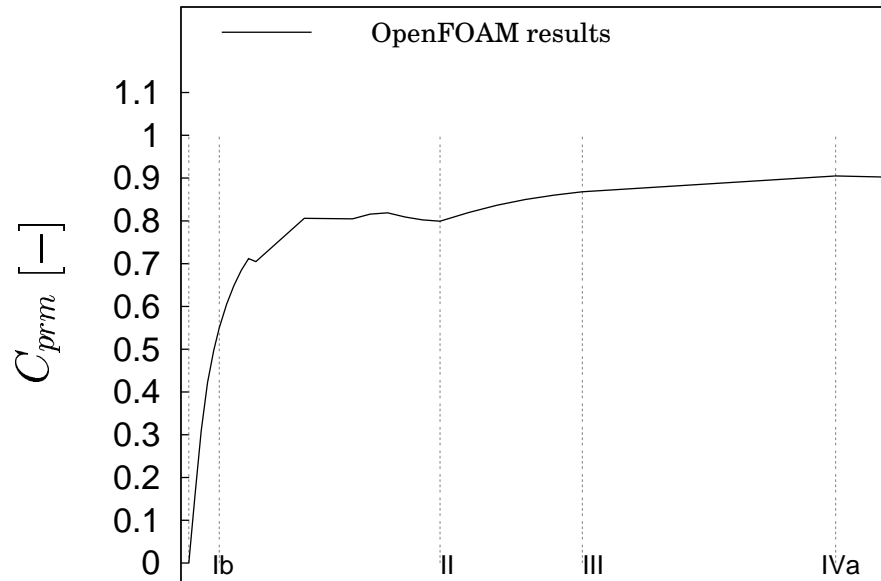
Streamlines colored by static pressure



Surface smearlines

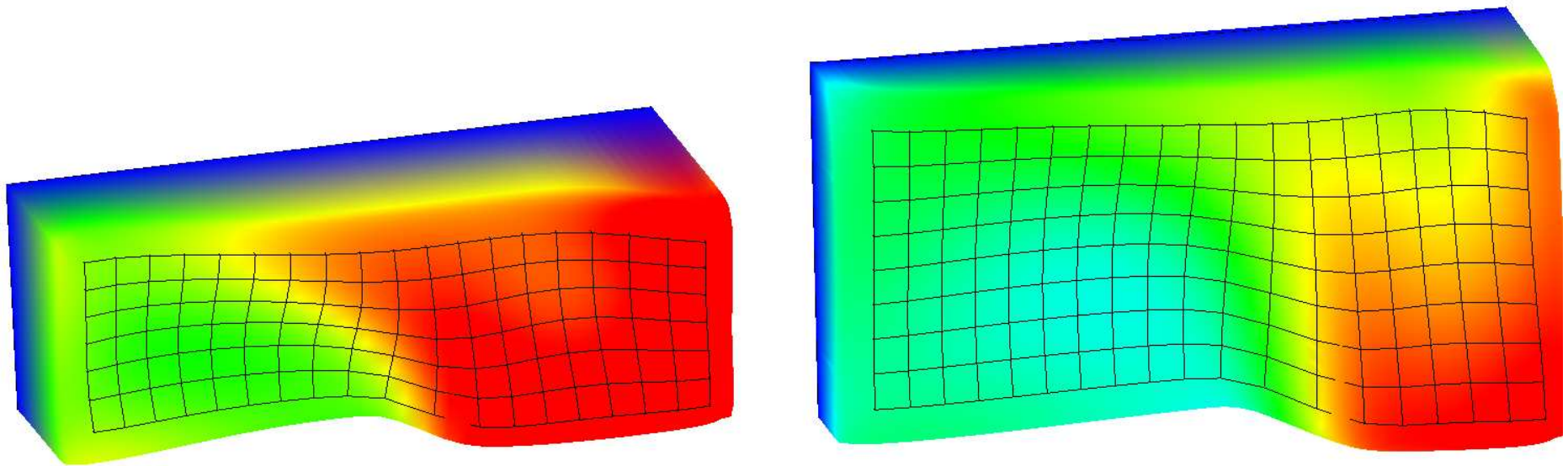
Through-flow analysis

- Through-flow analysis of the mean pressure recovery factor (C_{prm}) and the energy loss coefficient (ζ)



Velocity distributions

To be compared in detail with measurements and other computational results at the workshop.



Through-flow velocity distributions at Cross-Sections II and III

Unsteadiness

- The 'quasi-steady' solution was unsteady
- The time terms are not included in the equations
- A 'false time step' is given by the iterations and the under-relaxations
- The 'false time step' is different for different control volumes
- A true unsteady solution is needed to resolve the unsteadiness
- An unsteady $k - \varepsilon$ computation of the same case has been made

Preliminary unsteady computations

Time step: $3 \cdot 10^{-4} s$, Periodicity in time: $\sim 0.48 s$

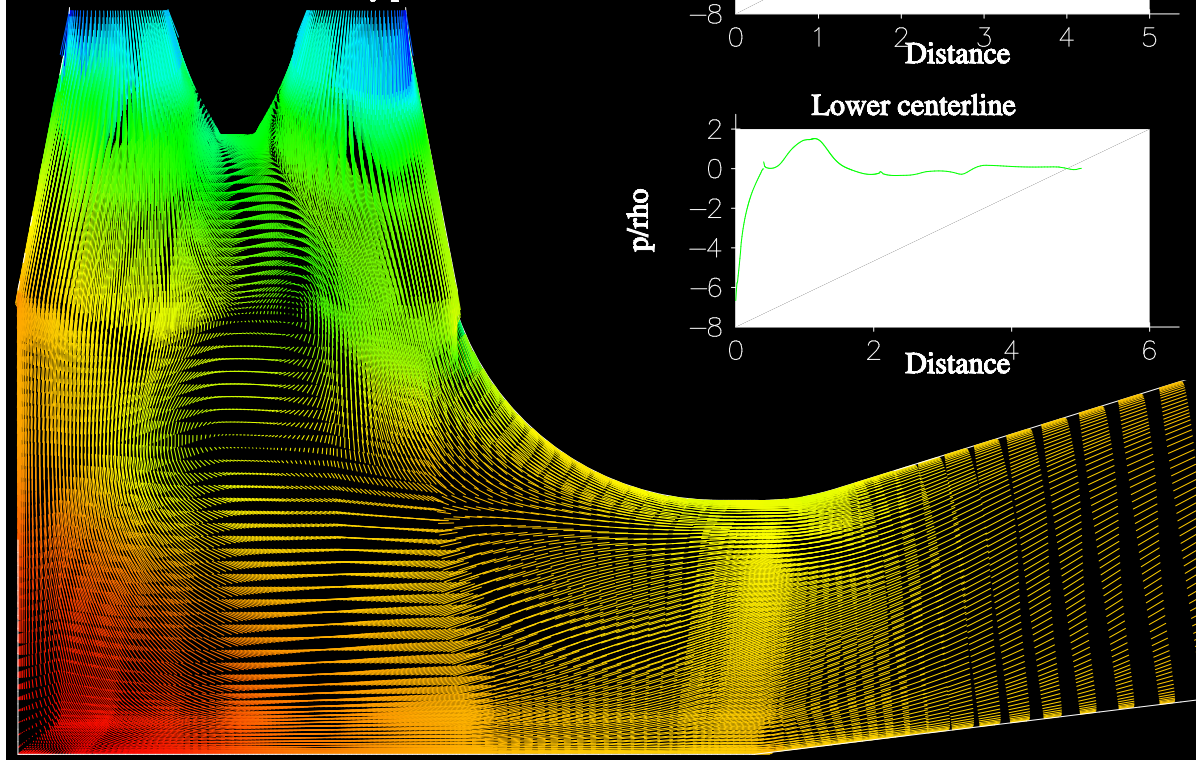
The Turbine-99 draft tube

OpenFOAM results

Unsteady k- ϵ

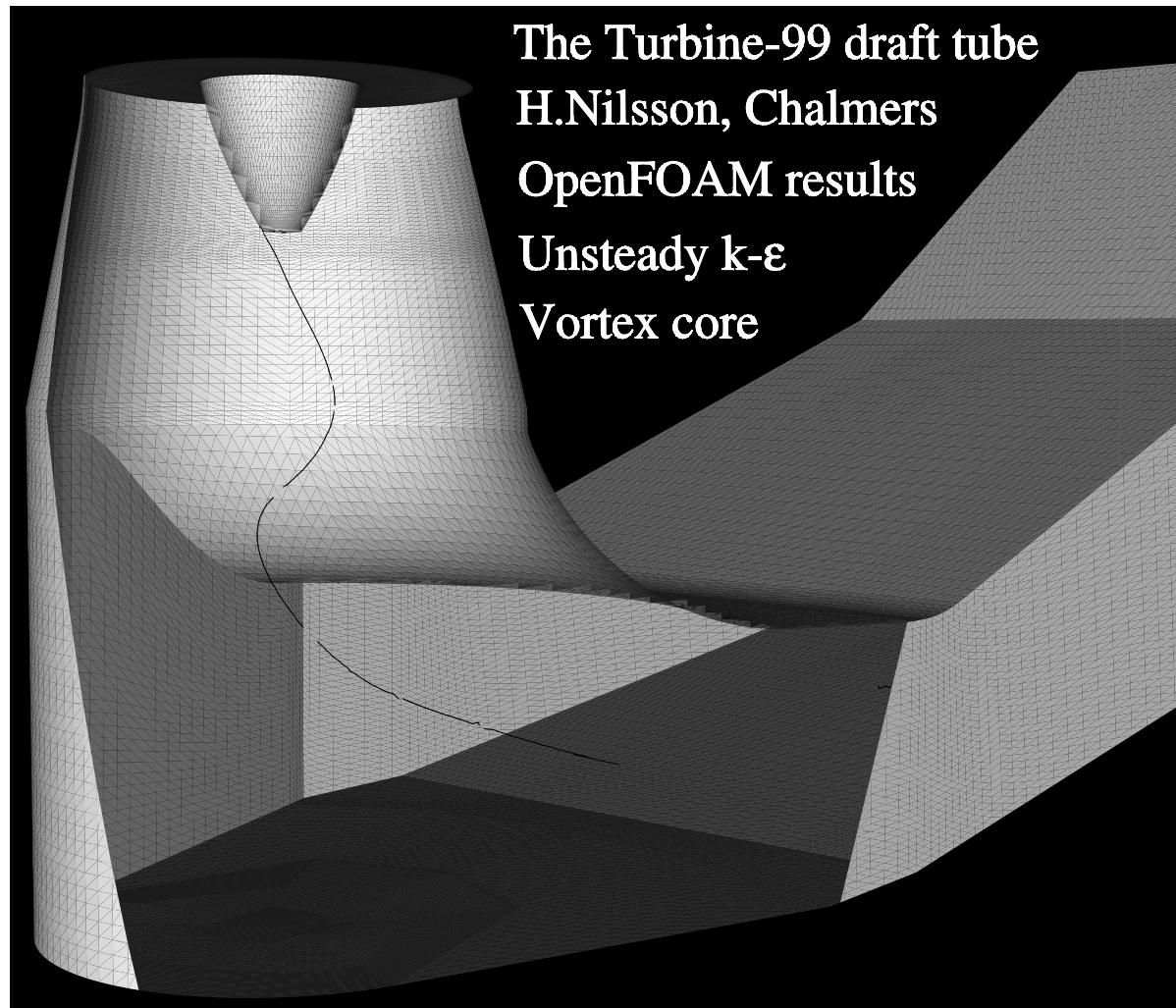
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Vectors colored by p/rho



Preliminary unsteady computations

Time step: $3 \cdot 10^{-4} s$, Periodicity in time: $\sim 0.48 s$



Conclusions

- The steady computation was unable to dampen the physical unsteadiness in the flow, i.e. neither the $k - \varepsilon$ turbulence model nor the numerical schemes were diffusive enough to yield a fully steady solution.
- A preliminary unsteady computation yields a highly unsteady flow
- The averaged 'quasi-steady' solution yields results very similar to those of CFX-5 (Page et al.)
- OpenFOAM is able to generate good computational results in an efficient way.
- The OpenFOAM common platform facilitates international collaboration like the one in the present work.

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WAPLANS

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