

Electric welding arc modeling with the 3D solver OpenFOAM

- A comparison of different electromagnetic models -

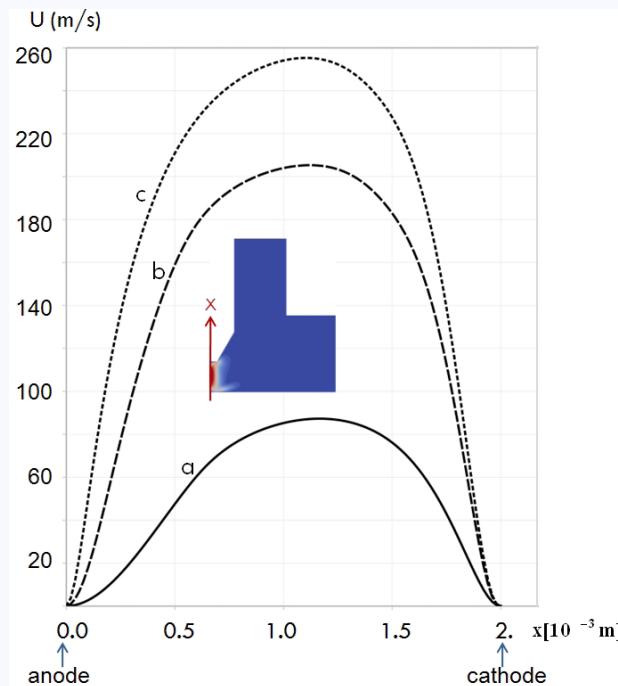
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¹University West, Dep. of Engineering Science, Trollhättan, Sweden

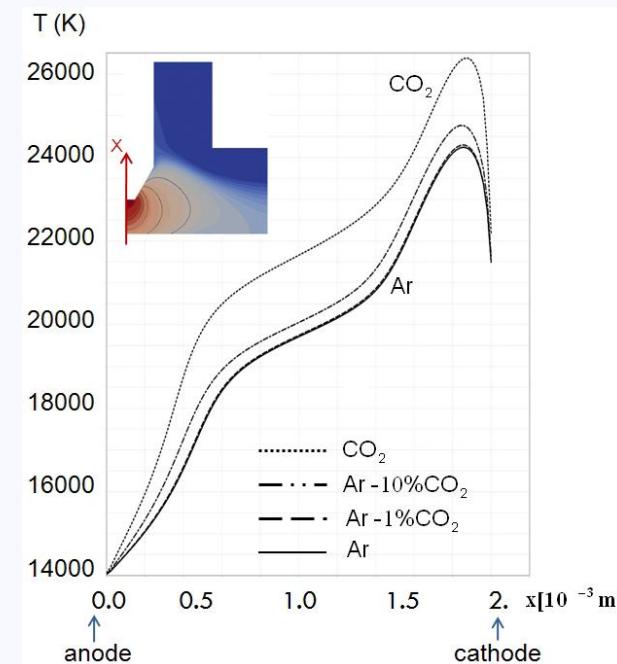
²Chalmers University of Technology, Dep. of Applied Mechanics,
Gothenburg, Sweden

- **Context / Motivation:**
better understand the heat source
- **Software OpenFOAM-1.6.x**
 - open source CFD software
 - C++ library of object-oriented classes
for implementing solvers for continuum mechanics

”Numerical simulation of Ar-x%CO₂ shielding gas and its effect on an electric welding arc”



Influence of BC on anode an cathode composition



Influence of gas

Here focus on a comparison of different electromagnetic models

Model: thermal fluid part

Main assumptions (plasma core):

- one-fluid model
- local thermal equilibrium
- mechanically incompressible and thermally expansible
- *steady flow*
- *laminar flow (assuming laminar shielding gas inlet)*

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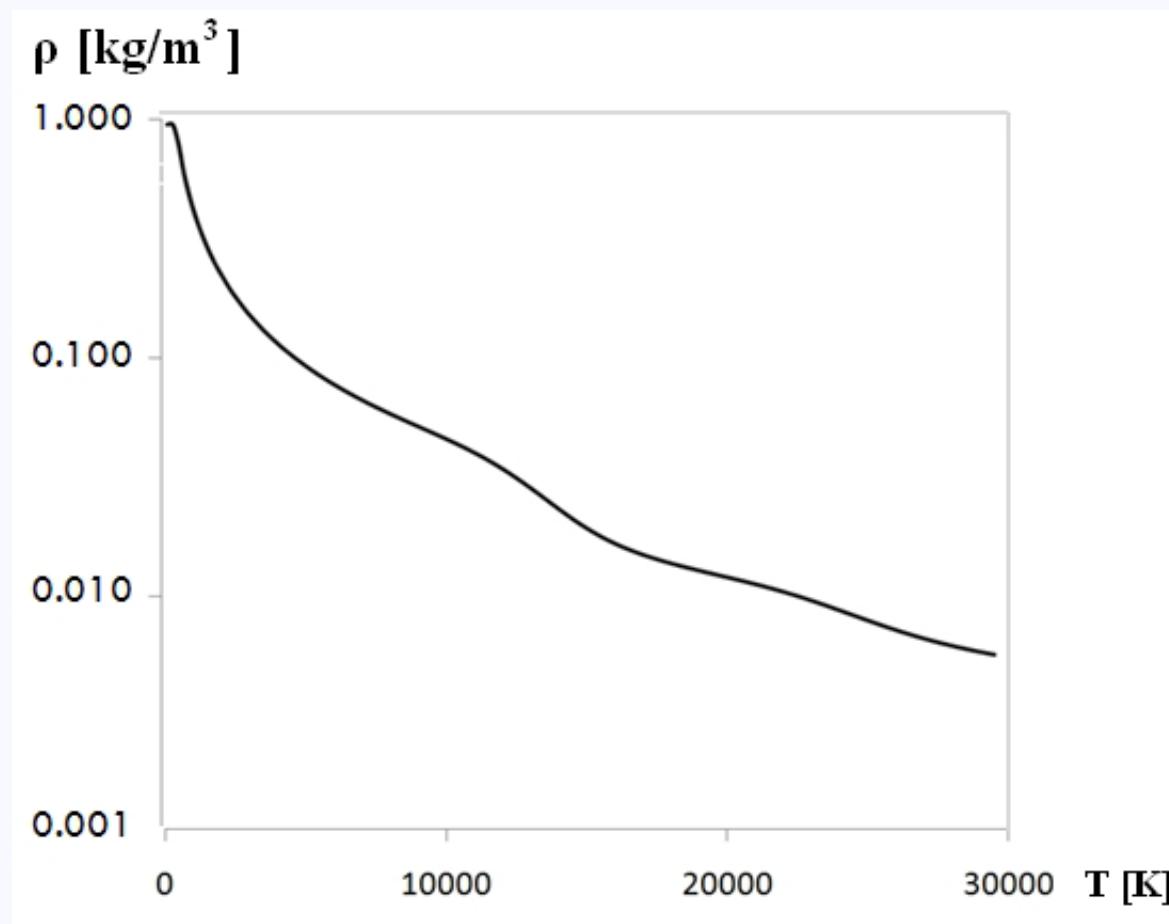
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Argon plasma density as function of temperature.

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Main assumptions:

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- plasma optically thin
- *steady*
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- *laminar flow (assuming laminar shielding gas)* IIW Doc.212-1189 -11

Model: electromagnetic part

- 3D model with
- 2D axi-symmetric models:
 - ✓ Electric potential formulation
 - ✓ Magnetic field formulation

Model: electromagnetic part

- 3D model with $V, \vec{A} \rightarrow \vec{E}, \vec{J}, \vec{B}$

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- 3D model with $V, \vec{A} \rightarrow \vec{E}, \vec{J}, \vec{B}$
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 - ✓ Electric potential formulation $V \rightarrow \vec{E}, \vec{J} \rightarrow B_\theta$
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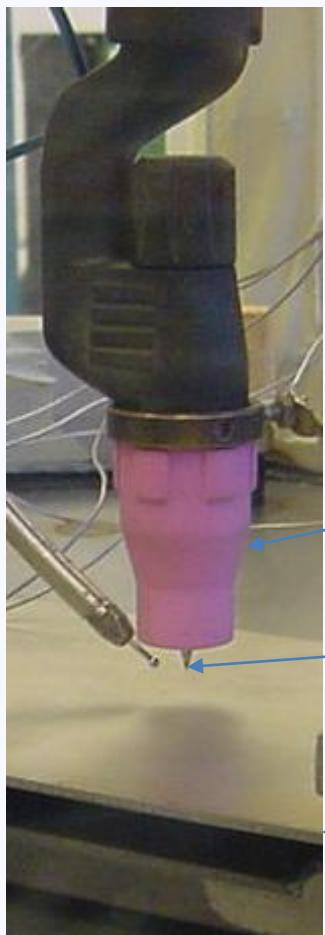
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M.A. Ramírez , G. Trapaga and J. McKelliget (2003). A comparison between two different numerical formulations of welding arc simulation. *Modelling Simul. Mater. Sci. Eng.*, **11**, pp. 675-695.

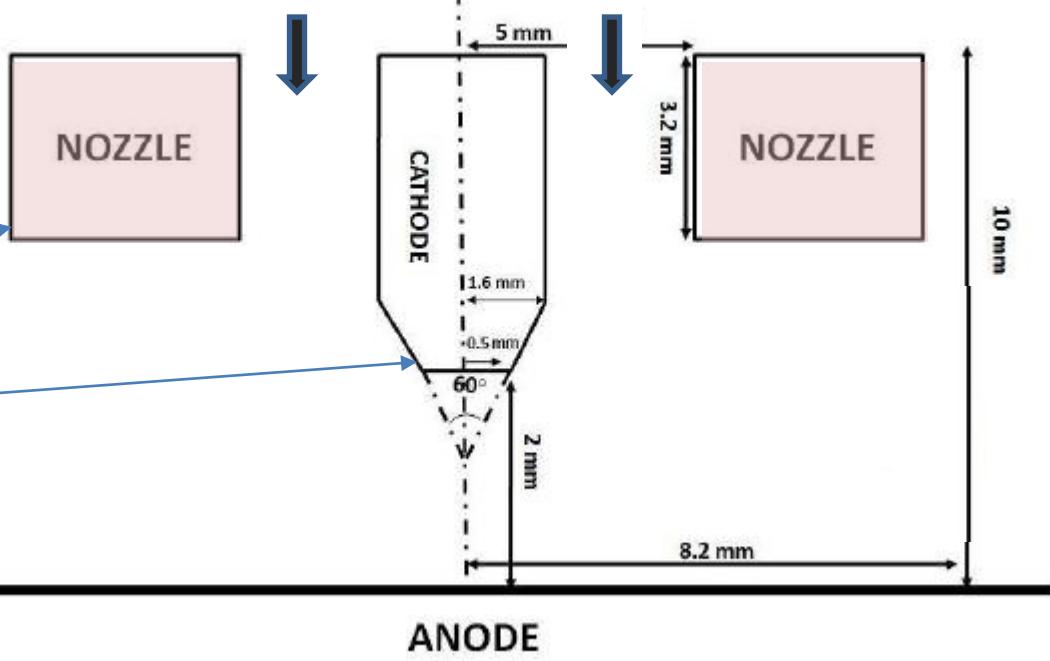
Test case: Tungsten Inert Gas welding



Applied current: $I=200\text{A}$

Ar shielding
gas inlet

Shielding gas
inlet $\bar{u} = 2.36\text{m/s}$

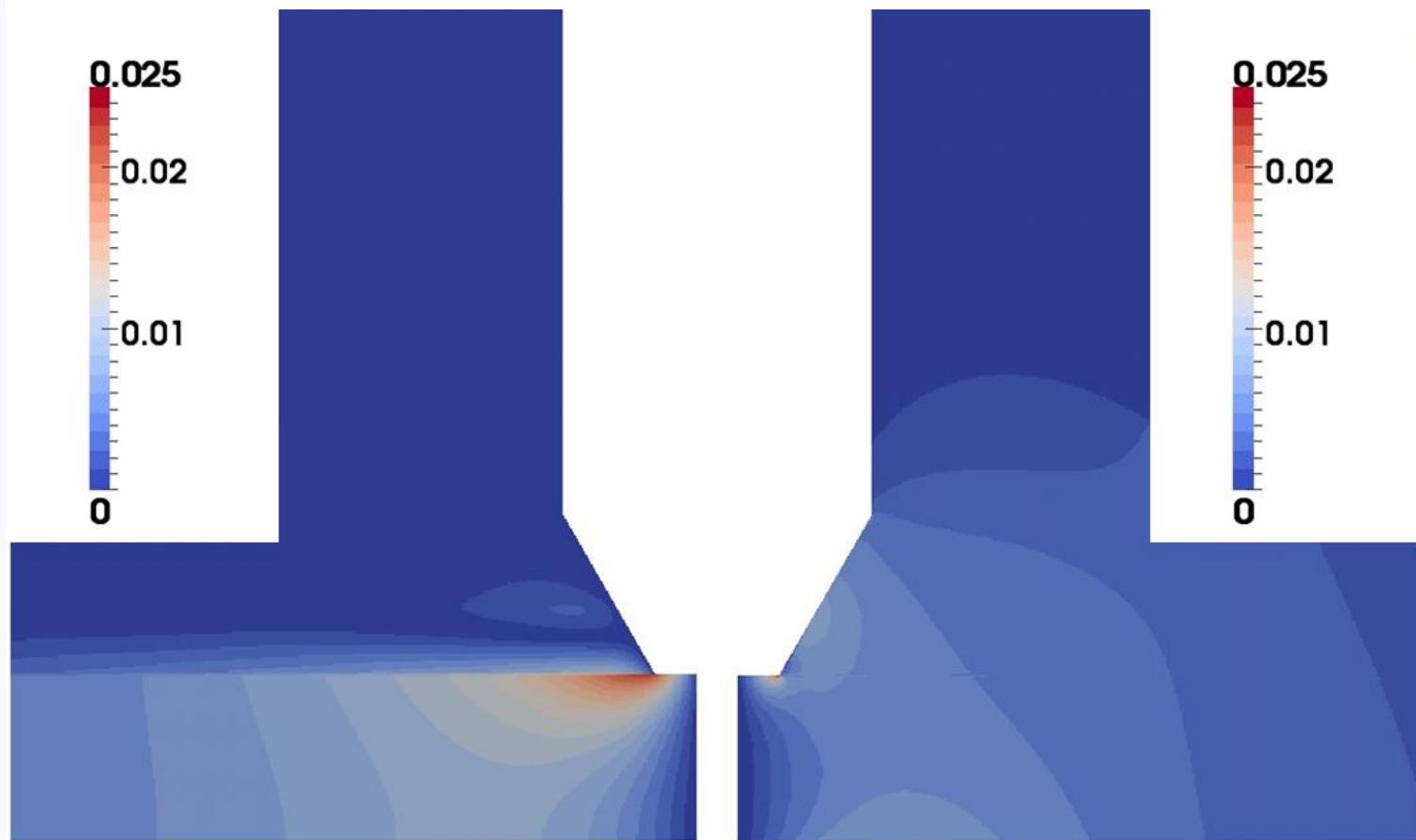


Picture of a TIG torch

Sketch of the cross section of a TIG torch

$$B_\theta = \frac{\mu_0}{r} \int_0^r J_{axial}(l) l \, dl$$

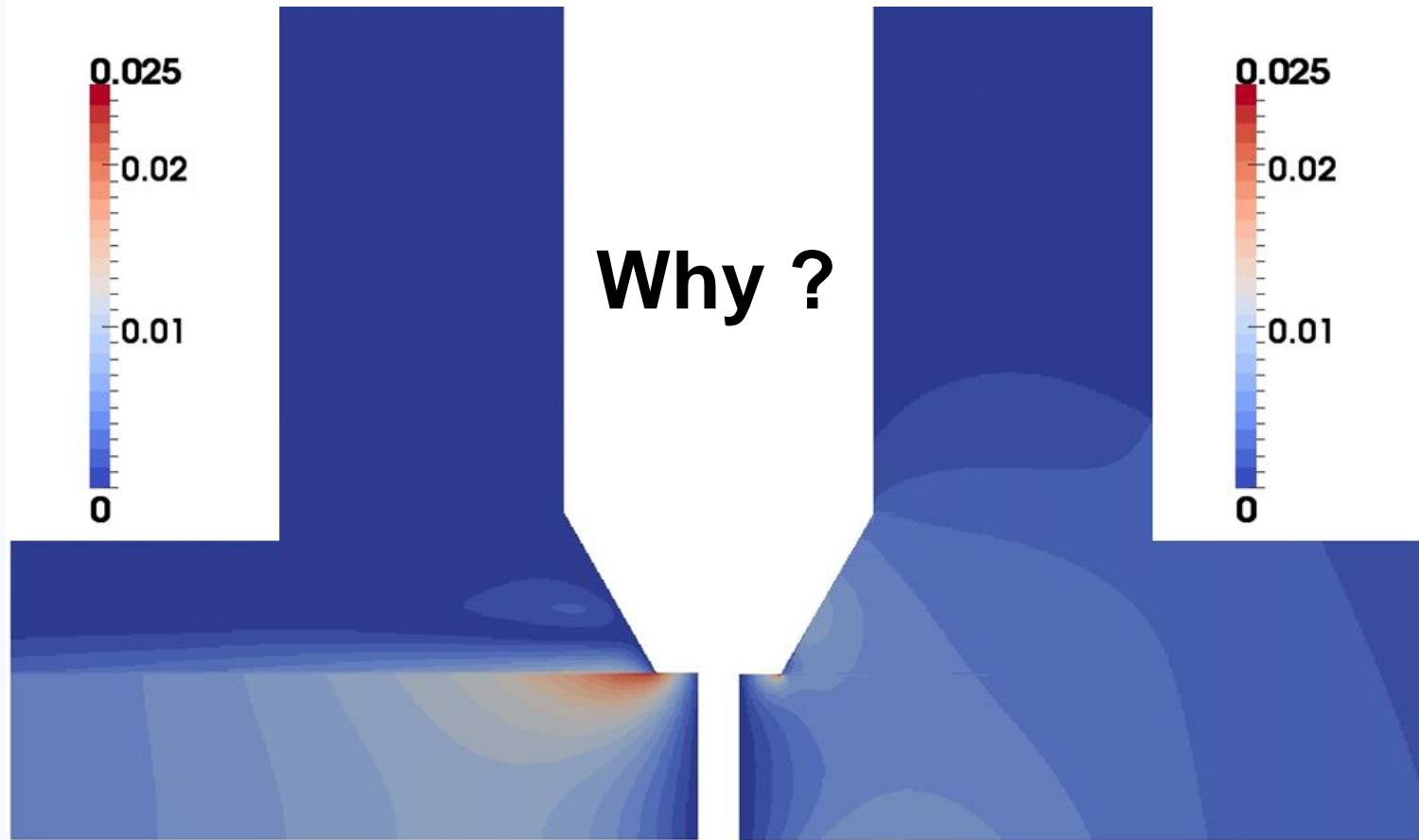
$$B_\theta = (\nabla \times \vec{A})_\theta$$



Magnetic field magnitude calculated with the electric potential formulation (left) and the 3D

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Magnetic field magnitude calculated with the electric potential formulation (left) and the 3D
1 (right)

Maxwell's equations

- Gauss' law for magnetism: $\nabla \cdot \vec{B} = 0$
- Ampère's law: $\epsilon_0 \mu_0 \partial_t \vec{E} = \nabla \times \vec{B} - \mu_0 \vec{J}$
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- + generalized Ohm's law $\vec{J} = \vec{J}_{drift} + \vec{J}_{ind} + \vec{J}_{Hall} + \vec{J}_{diff} + \vec{J}_{ther}$

Assumptions (plasma core)

- $\lambda_{Debye} \approx 10^{-8} m \ll L_c \rightarrow$ local electro-neutrality
- quasi-steady electromagnetic phenomena
-
-

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- $Re_m \ll 1 \rightarrow \vec{J}_{ind} = \sigma \vec{u} \times \vec{B} \ll \vec{J}_{drift}$

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Electromagnetic model for arc plasma core

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Electromagnetic model for arc plasma core

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$$\Delta \vec{A} = \mu_0 \sigma \nabla V$$

with

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$$\vec{B} = \nabla \times \vec{A}$$

Electromagnetic model for arc plasma core

(1)

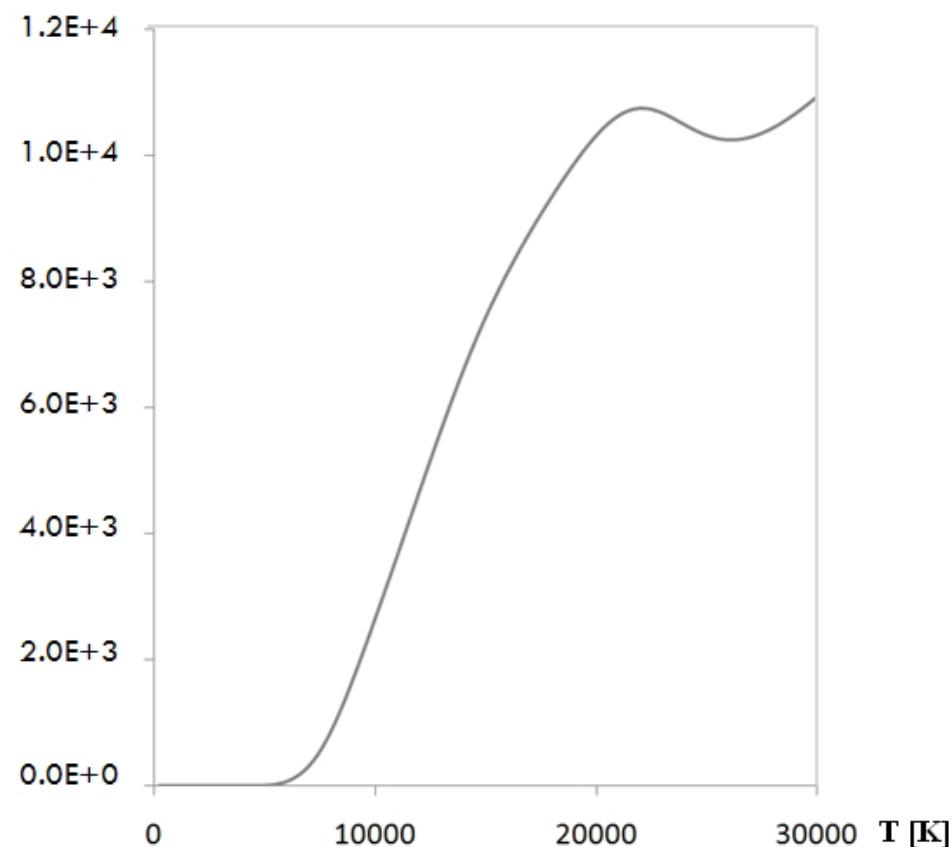
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Argon plasma electric conductivity
as function of temperature

(1) with Lorentz gauge : $\nabla \cdot \vec{A} = 0$

2D axi-symmetric case

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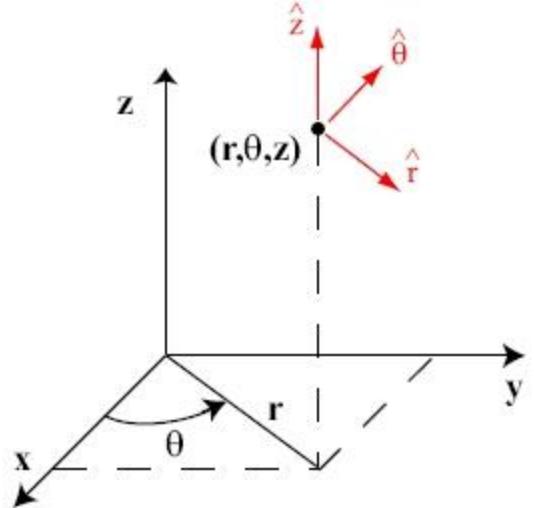
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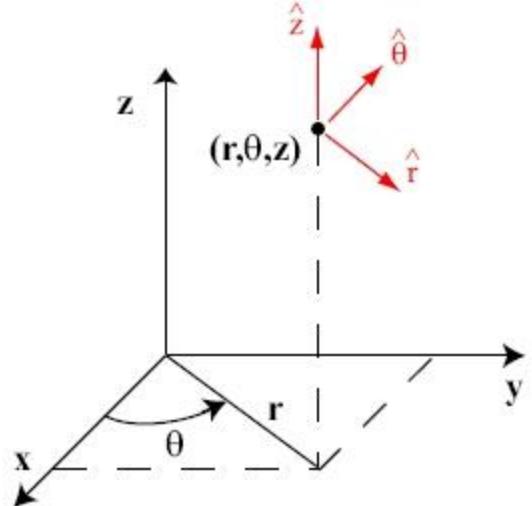
2D axi-symmetric case⁽¹⁾



2D axi-symmetric case⁽¹⁾

Then

$$\partial_\theta \rightarrow 0$$



with

with

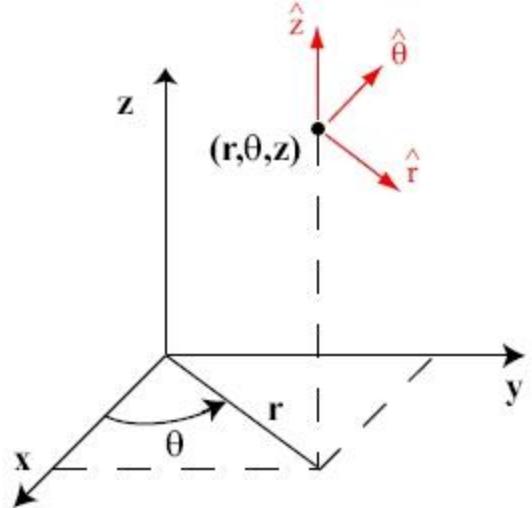
with

2D axi-symmetric case⁽¹⁾

Then

$$\partial_{\theta} = \hat{r} \sin \theta \frac{\partial}{\partial r} + \hat{z} \frac{\partial}{\partial z}$$

$$V(r, z)$$

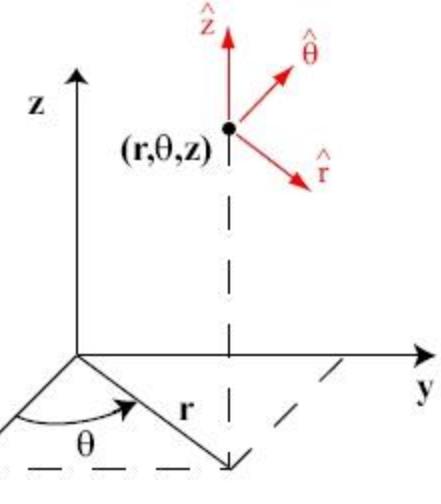


with

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Then

$$\partial_{\theta}$$

$$V(r,z)$$

$$\vec{A} = (A_r, 0, A_z) \quad \text{with} \quad A_r(r,z), A_z(r,z)$$

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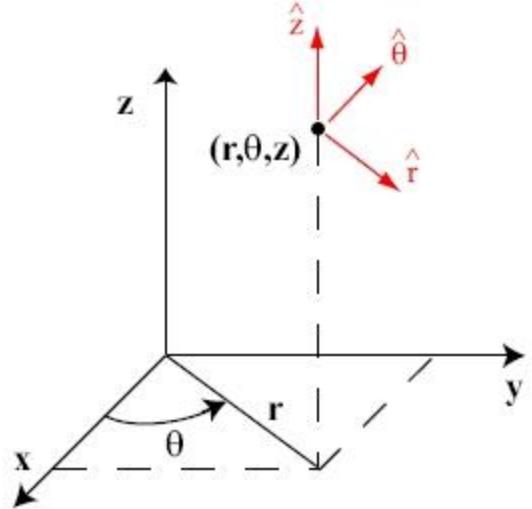
Then

$$\partial_\theta \rightarrow 0$$

$$V(r,z)$$

$$\vec{A} = (A_r, 0, A_z) \quad \text{with} \quad A_r(r,z), A_z(r,z)$$

$$\vec{J} = (J_r, 0, J_z) \quad \text{with} \quad J_r(r,z), J_z(r,z)$$



with

2D axi-symmetric case⁽¹⁾

Then

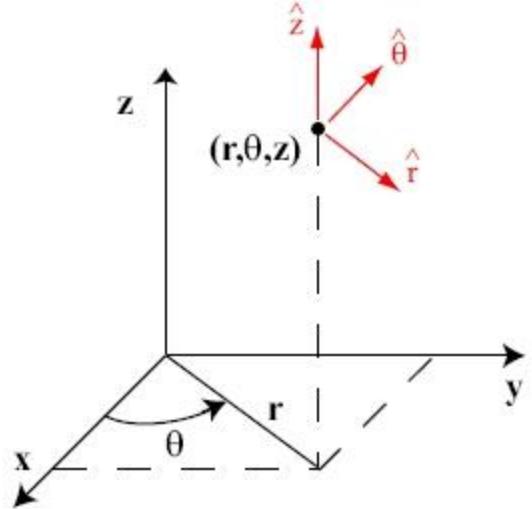
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$$\vec{B} = (0, B_{\theta}, 0) \quad \text{with} \quad B_{\theta}(r,z)$$



2D axi-symmetric case⁽¹⁾

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \sigma \frac{\partial V}{\partial r} \right) + \frac{\partial}{\partial z} \left(\sigma \frac{\partial V}{\partial z} \right) = 0$$

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial A_r}{\partial r} \right) + \frac{\partial^2 A_r}{\partial z^2} - \frac{A_r}{r^2} = \mu_0 \sigma \frac{\partial V}{\partial r}$$

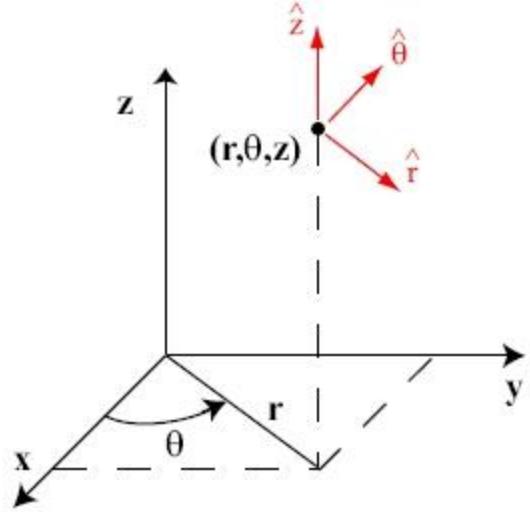
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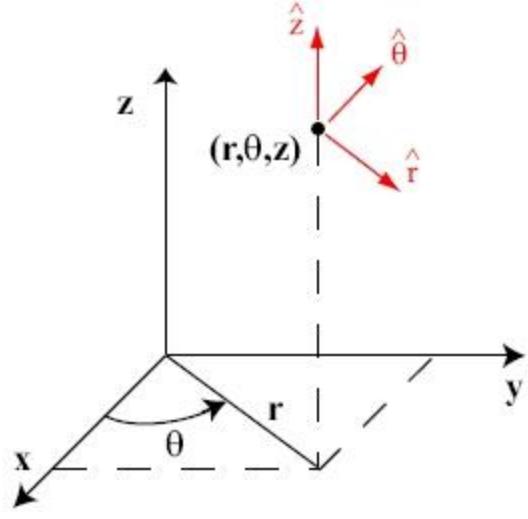
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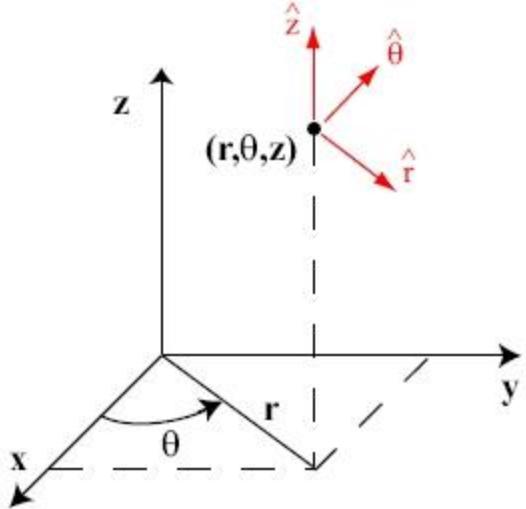
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(2)

Induction diffusion equation

$$\frac{\partial}{\partial r} \left(\frac{1}{\sigma r} \frac{\partial (r B_\theta)}{\partial r} \right) + \frac{\partial}{\partial z} \left(\frac{1}{\sigma} \frac{\partial B_\theta}{\partial z} \right) = 0$$

(1) with Lorentz gauge : $\nabla \cdot \vec{A} = 0$

(2) as $\partial_{r,z}^2 V = \partial_{z,r}^2 V$

2D axi-symmetric case - equivalent formulations

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial A_r}{\partial r} \right) + \frac{\partial^2 A_r}{\partial z^2} - \frac{A_r}{r^2} = \mu_0 \sigma \frac{\partial V}{\partial r}$$

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial A_z}{\partial r} \right) + \frac{\partial^2 A_z}{\partial z^2} = \mu_0 \sigma \frac{\partial V}{\partial z}$$

(1)

$$\frac{\partial B_\theta}{\partial z} = \mu_0 \sigma \frac{\partial V}{\partial r} = -\mu_0 J_r$$

$$\frac{1}{r} \frac{\partial (r B_\theta)}{\partial r} = -\mu_0 \sigma \frac{\partial V}{\partial z} = \mu_0 J_z$$

Induction diffusion equation

$$\frac{\partial}{\partial r} \left(\frac{1}{\sigma r} \frac{\partial (r B_\theta)}{\partial r} \right) + \frac{\partial}{\partial z} \left(\frac{1}{\sigma} \frac{\partial B_\theta}{\partial z} \right) = 0$$

(2)

(2)

$$B_\theta(r, z) = \int_{l=z_0}^{l=z} J_z(r, l) \, dl + B_\theta(r, z_0)$$

(1) with Lorentz gauge : $\nabla \cdot \vec{A} = 0$

(2) as $\partial_{r,z}^2 V = \partial_{z,r}^2 V$

2D axi-symmetric case - equivalent formulations

F1

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial A_r}{\partial r} \right) + \frac{\partial^2 A_r}{\partial z^2} - \frac{A_r}{r^2} = \mu_0 \sigma \frac{\partial V}{\partial r}$$

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial A_z}{\partial r} \right) + \frac{\partial^2 A_z}{\partial z^2} = \mu_0 \sigma \frac{\partial V}{\partial z}$$

(1)

$$\frac{\partial B_\theta}{\partial z} = \mu_0 \sigma \frac{\partial V}{\partial r} = -\mu_0 J_r$$

$$\frac{1}{r} \frac{\partial (r B_\theta)}{\partial r} = -\mu_0 \sigma \frac{\partial V}{\partial z} = \mu_0 J_z$$

Induction diffusion equation

$$F2 \quad \frac{\partial}{\partial r} \left(\frac{1}{\sigma r} \frac{\partial (r B_\theta)}{\partial r} \right) + \frac{\partial}{\partial z} \left(\frac{1}{\sigma} \frac{\partial B_\theta}{\partial z} \right) = 0$$

(2)

(2)

$$F3 \quad B_\theta(r, z) = \int_{l=z_0}^{l=z} J_z(r, l) \, dl + B_\theta(r, z_0)$$

(1) with Lorentz gauge : $\nabla \cdot \vec{A} = 0$

(2) as $\partial_{r,z}^2 V = \partial_{z,r}^2 V$

2D axi-symmetric case - equivalent formulations

F1

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial A_r}{\partial r} \right) + \frac{\partial^2 A_r}{\partial z^2} - \frac{A_r}{r^2} = \mu_0 \sigma \frac{\partial V}{\partial r}$$

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial A_z}{\partial r} \right) + \frac{\partial^2 A_z}{\partial z^2} = \mu_0 \sigma \frac{\partial V}{\partial z}$$

(1)

$$\frac{\partial B_\theta}{\partial z} = \mu_0 \sigma \frac{\partial V}{\partial r} = -\mu_0 J_r$$

$$\frac{1}{r} \frac{\partial (r B_\theta)}{\partial r} = -\mu_0 \sigma \frac{\partial V}{\partial z} = \mu_0 J_z$$

F2

Induction diffusion equation

$$\frac{\partial}{\partial r} \left(\frac{1}{\sigma r} \frac{\partial (r B_\theta)}{\partial r} \right) + \frac{\partial}{\partial z} \left(\frac{1}{\sigma} \frac{\partial B_\theta}{\partial z} \right) = 0$$

(2)

(2)

F3 $B_\theta(r, z) = \int_{l=z_0}^{l=z} J_z(r, l) dl + B_\theta(r, z_0)$

(1) with Lorentz gauge : $\nabla \cdot \vec{A} = 0$

(2) as $\partial_{r,z}^2 V = \partial_{z,r}^2 V$

2D axi-symmetric case - equivalent formulations

F1

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial A_r}{\partial r} \right) + \frac{\partial^2 A_r}{\partial z^2} - \frac{A_r}{r^2} = \mu_0 \sigma \frac{\partial V}{\partial r}$$

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial A_z}{\partial r} \right) + \frac{\partial^2 A_z}{\partial z^2} = \mu_0 \sigma \frac{\partial V}{\partial z}$$

(1)

$$\frac{\partial B_\theta}{\partial z} = \mu_0 \sigma \frac{\partial V}{\partial r} = -\mu_0 J_r$$

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F2

Induction diffusion equation

$$\frac{\partial}{\partial r} \left(\frac{1}{\sigma r} \frac{\partial (r B_\theta)}{\partial r} \right) + \frac{\partial}{\partial z} \left(\frac{1}{\sigma} \frac{\partial B_\theta}{\partial z} \right) = 0$$

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F3

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2D axi-symmetric case - equivalent formulations

F1

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial A_r}{\partial r} \right) + \frac{\partial^2 A_r}{\partial z^2} - \frac{A_r}{r^2} = \mu_0 \sigma \frac{\partial V}{\partial r}$$

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial A_z}{\partial r} \right) + \frac{\partial^2 A_z}{\partial z^2} = \mu_0 \sigma \frac{\partial V}{\partial z}$$

(1)

$$\frac{\partial B_\theta}{\partial z} = \mu_0 \sigma \frac{\partial V}{\partial r} = -\mu_0 J_r$$

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F2

Induction diffusion equation

$$\frac{\partial}{\partial r} \left(\frac{1}{\sigma r} \frac{\partial (r B_\theta)}{\partial r} \right) + \frac{\partial}{\partial z} \left(\frac{1}{\sigma} \frac{\partial B_\theta}{\partial z} \right) = 0$$

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(2)

F3

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(1) with Lorentz gauge : $\nabla \cdot \vec{A} = 0$

(2) as $\partial_{r,z}^2 V = \partial_{z,r}^2 V$

Magnetic field formulation

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial A_r}{\partial r} \right) + \frac{\partial^2 A_r}{\partial z^2} - \frac{A_r}{r^2} = \mu_0 \sigma \frac{\partial V}{\partial r}$$

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial A_z}{\partial r} \right) + \frac{\partial^2 A_z}{\partial z^2} = \mu_0 \sigma \frac{\partial V}{\partial z}$$

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Induction diffusion equation

$$\frac{\partial}{\partial r} \left(\frac{1}{\sigma r} \frac{\partial (r B_\theta)}{\partial r} \right) + \frac{\partial}{\partial z} \left(\frac{1}{\sigma} \frac{\partial B_\theta}{\partial z} \right) = 0$$

$$B_\theta(r, z) = \int_{l=z_0}^{l=z} J_z(r, l) \, dl + B_\theta(r, z_0)$$

(1) with Lorentz gauge : $\nabla \cdot \vec{A} = 0$

(2) as $\partial_{r,z}^2 V = \partial_{z,r}^2 V$

2D axi-symmetric case⁽¹⁾

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \sigma \frac{\partial V}{\partial r} \right) + \frac{\partial}{\partial z} \left(\sigma \frac{\partial V}{\partial z} \right) = 0$$

F1

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial A_r}{\partial r} \right) + \frac{\partial^2 A_r}{\partial z^2} - \frac{A_r}{r^2} = \mu_0 \sigma \frac{\partial V}{\partial r}$$

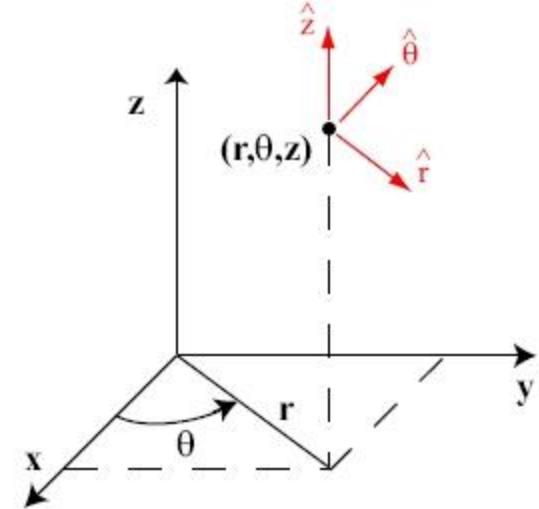
$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial A_z}{\partial r} \right) + \frac{\partial^2 A_z}{\partial z^2} = \mu_0 \sigma \frac{\partial V}{\partial z}$$

with

$$\vec{J} : \quad J_r = \sigma E_r = -\sigma \frac{\partial V}{\partial r} \quad \text{and} \quad J_z = \sigma E_z = -\sigma \frac{\partial V}{\partial z}$$

$$\vec{B} : \quad B_\theta = \frac{\partial A_r}{\partial z} - \frac{\partial A_z}{\partial r}$$

(1) with Lorentz gauge : $\nabla \cdot \vec{A} = 0$



2D axi-symmetric case⁽¹⁾

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \sigma \frac{\partial V}{\partial r} \right) + \frac{\partial}{\partial z} \left(\sigma \frac{\partial V}{\partial z} \right) = 0$$

Induction diffusion equation

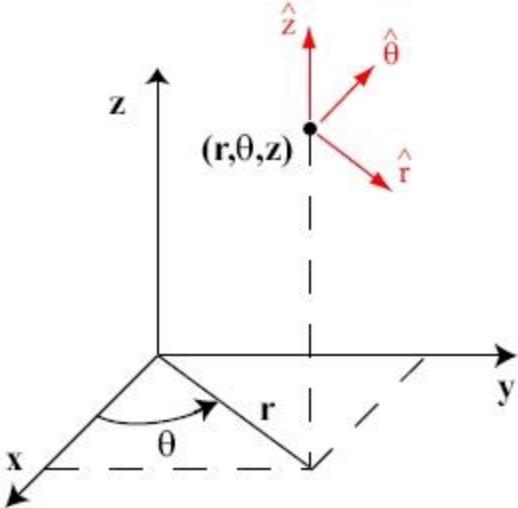
F2

$$\frac{\partial}{\partial r} \left(\frac{1}{\sigma r} \frac{\partial (r B_\theta)}{\partial r} \right) + \frac{\partial}{\partial z} \left(\frac{1}{\sigma} \frac{\partial B_\theta}{\partial z} \right) = 0$$

with

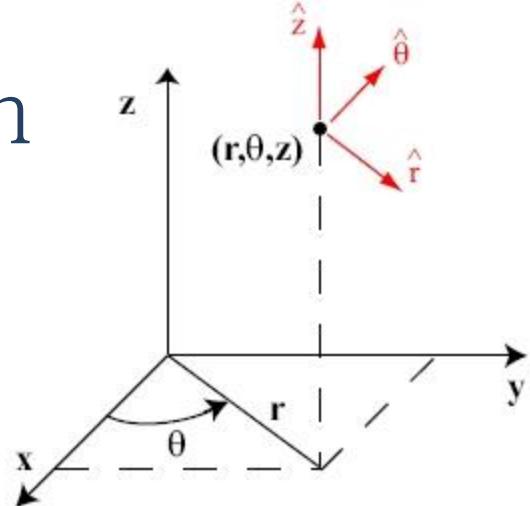
$$\vec{J} : \quad J_r = \sigma E_r = -\sigma \frac{\partial V}{\partial r} \quad \text{and} \quad J_z = \sigma E_z = -\sigma \frac{\partial V}{\partial z}$$

(1) with Lorentz gauge : $\nabla \cdot \vec{A} = 0$



Electric potential formulation

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \sigma \frac{\partial V}{\partial r} \right) + \frac{\partial}{\partial z} \left(\sigma \frac{\partial V}{\partial z} \right) = 0$$



Induction diffusion equation

F2

$$\frac{\partial}{\partial r} \left(\frac{1}{\sigma r} \frac{\partial (r B_\theta)}{\partial r} \right) + \frac{\partial}{\partial z} \left(\frac{1}{\sigma} \frac{\partial B_\theta}{\partial z} \right) = 0$$

0

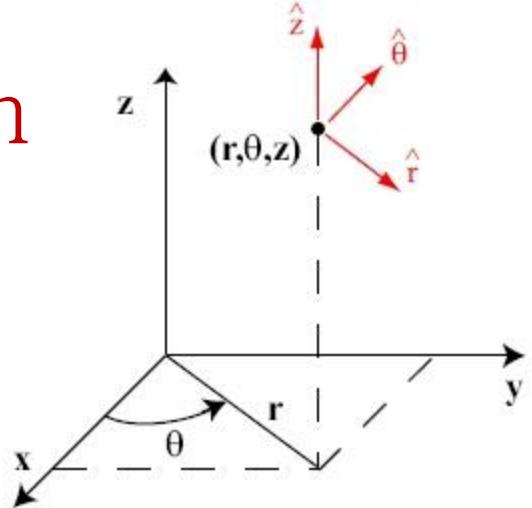
with

$$\vec{J} : \quad J_r = \sigma E_r = -\sigma \frac{\partial V}{\partial r} \quad \text{and} \quad J_z = \sigma E_z = -\sigma \frac{\partial V}{\partial z}$$

(1) with Lorentz gauge : $\nabla \cdot \vec{A} = 0$

Electric potential formulation

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \sigma \frac{\partial V}{\partial r} \right) + \frac{\partial}{\partial z} \left(\sigma \frac{\partial V}{\partial z} \right) = 0$$



$$B_\theta(r) = \frac{\mu_0}{r} \int_{l=r_0}^{l=r} l J_z(l) dl + B_\theta(r_0)$$

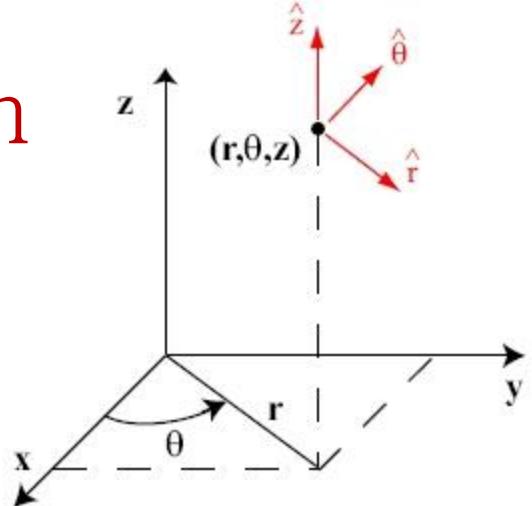
with

$$\vec{J} : \quad J_r = \sigma E_r = -\sigma \frac{\partial V}{\partial r} \quad \text{and} \quad J_z = \sigma E_z = -\sigma \frac{\partial V}{\partial z}$$

(1) with Lorentz gauge : $\nabla \cdot \vec{A} = 0$

Electric potential formulation

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \sigma \frac{\partial V}{\partial r} \right) + \frac{\partial}{\partial z} \left(\sigma \frac{\partial V}{\partial z} \right) = 0$$



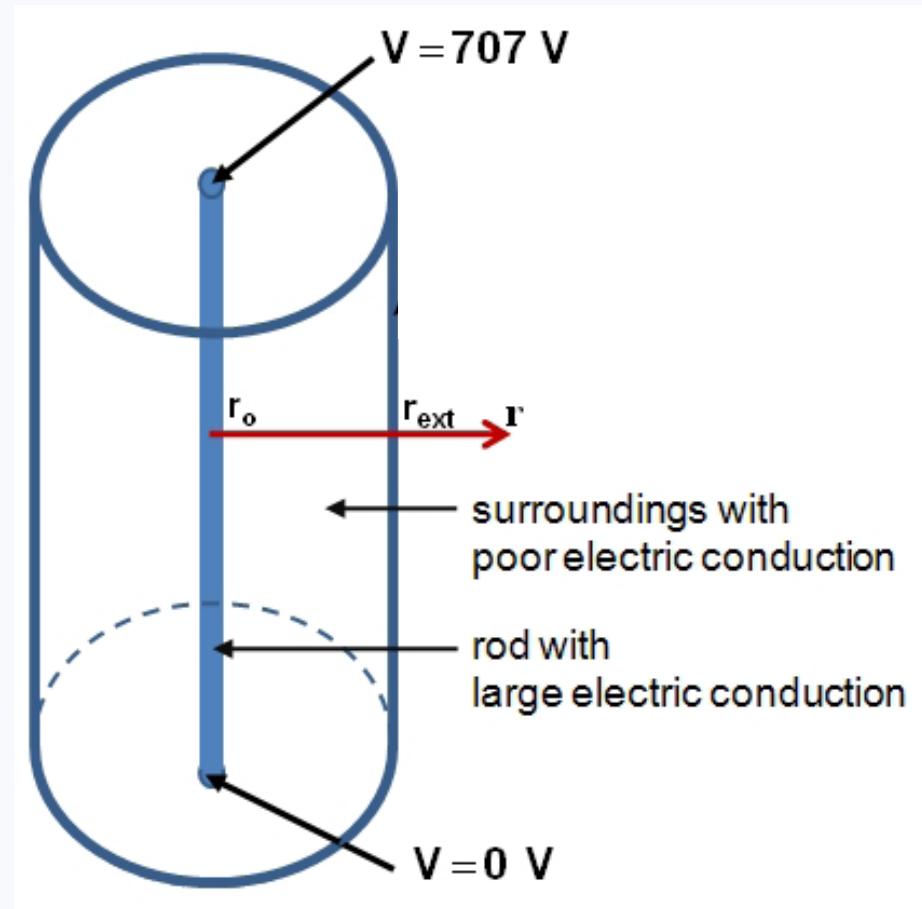
$$B_\theta(r) = \frac{\mu_0}{r} \int_{l=r_0}^{l=r} l J_z(l) dl + B_\theta(r_0)$$

with

$$\vec{J} : \quad J_r = \sigma E_r = -\sigma \frac{\partial V}{\partial r} \quad \textcolor{red}{<<} \quad J_z = \sigma E_z = -\sigma \frac{\partial V}{\partial z}$$

(1) with Lorentz gauge : $\nabla \cdot \vec{A} = 0$

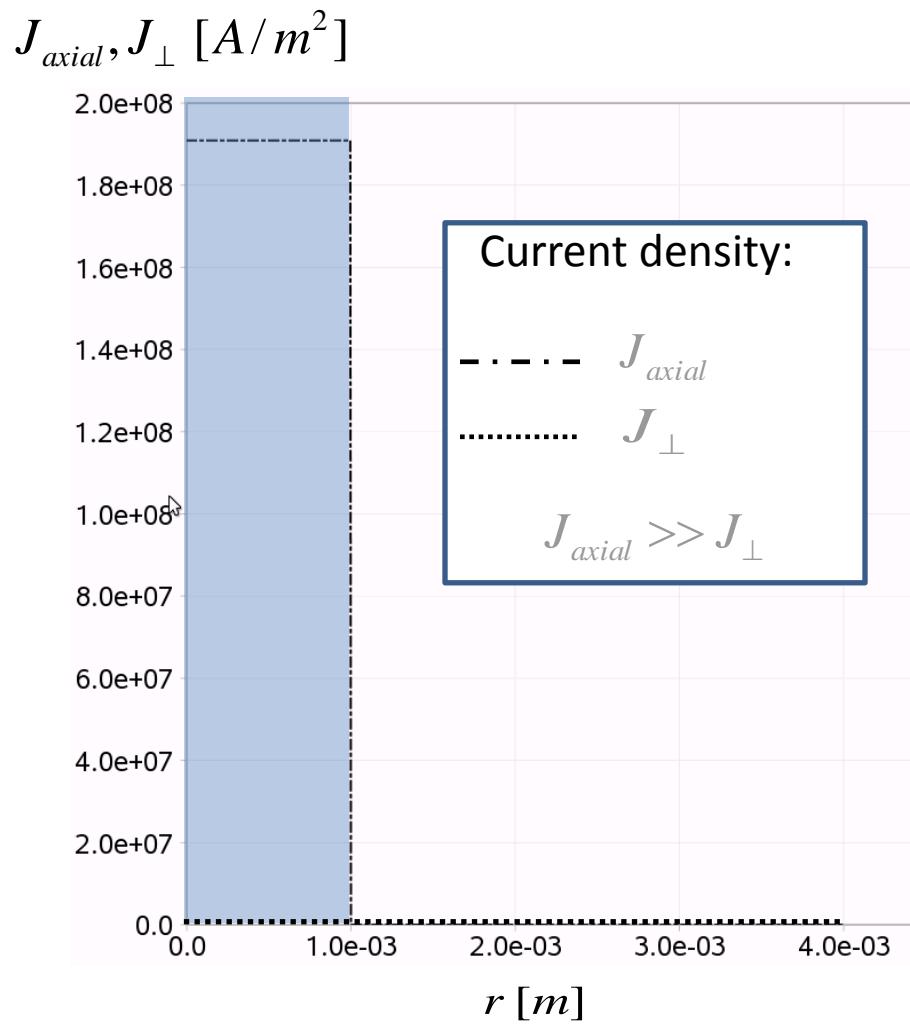
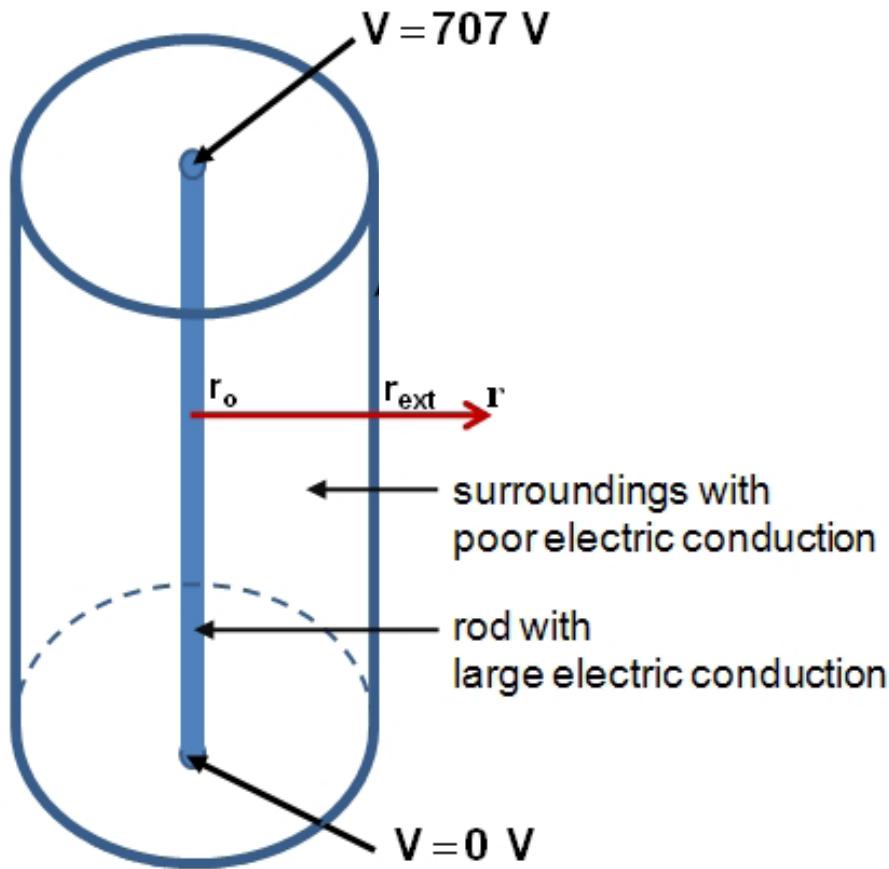
Test case: infinite conducting rod



$$\sigma = 2700 \text{ A}/(\text{V} \cdot \text{m})$$

$$\sigma = 10^{-5} \text{ A}/(\text{V} \cdot \text{m})$$

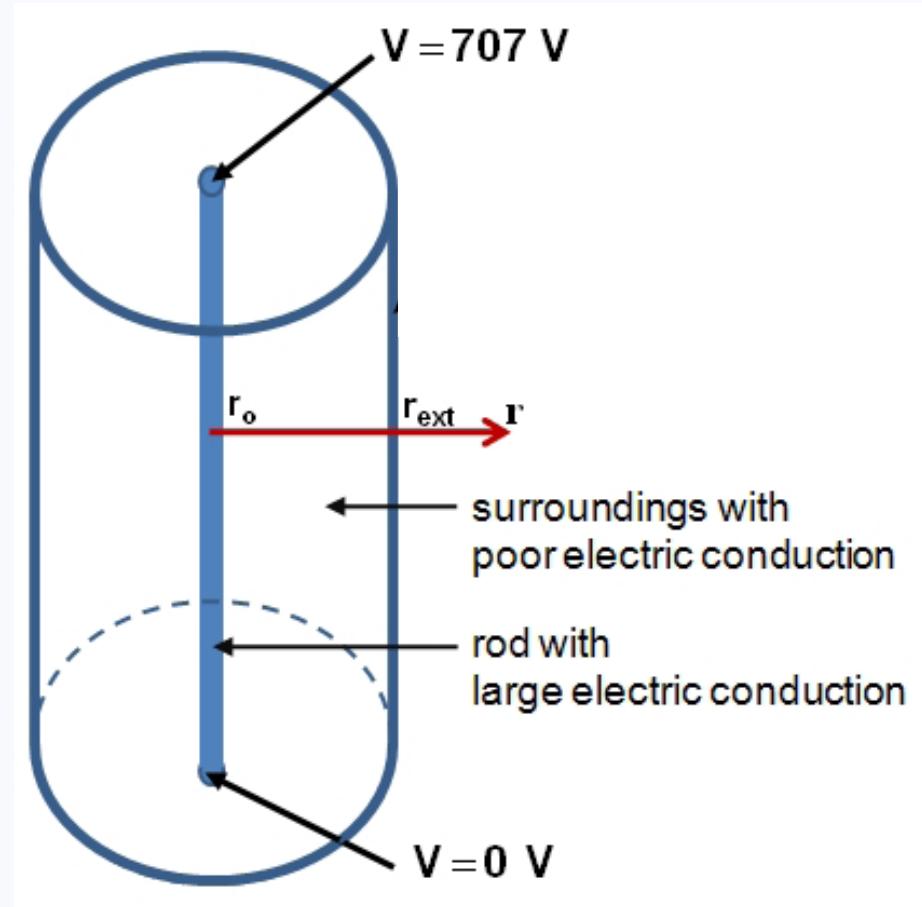
Test case: infinite conducting rod



$$\sigma = 2700 \text{ A}/(\text{V} \cdot \text{m})$$

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Test case: infinite conducting rod



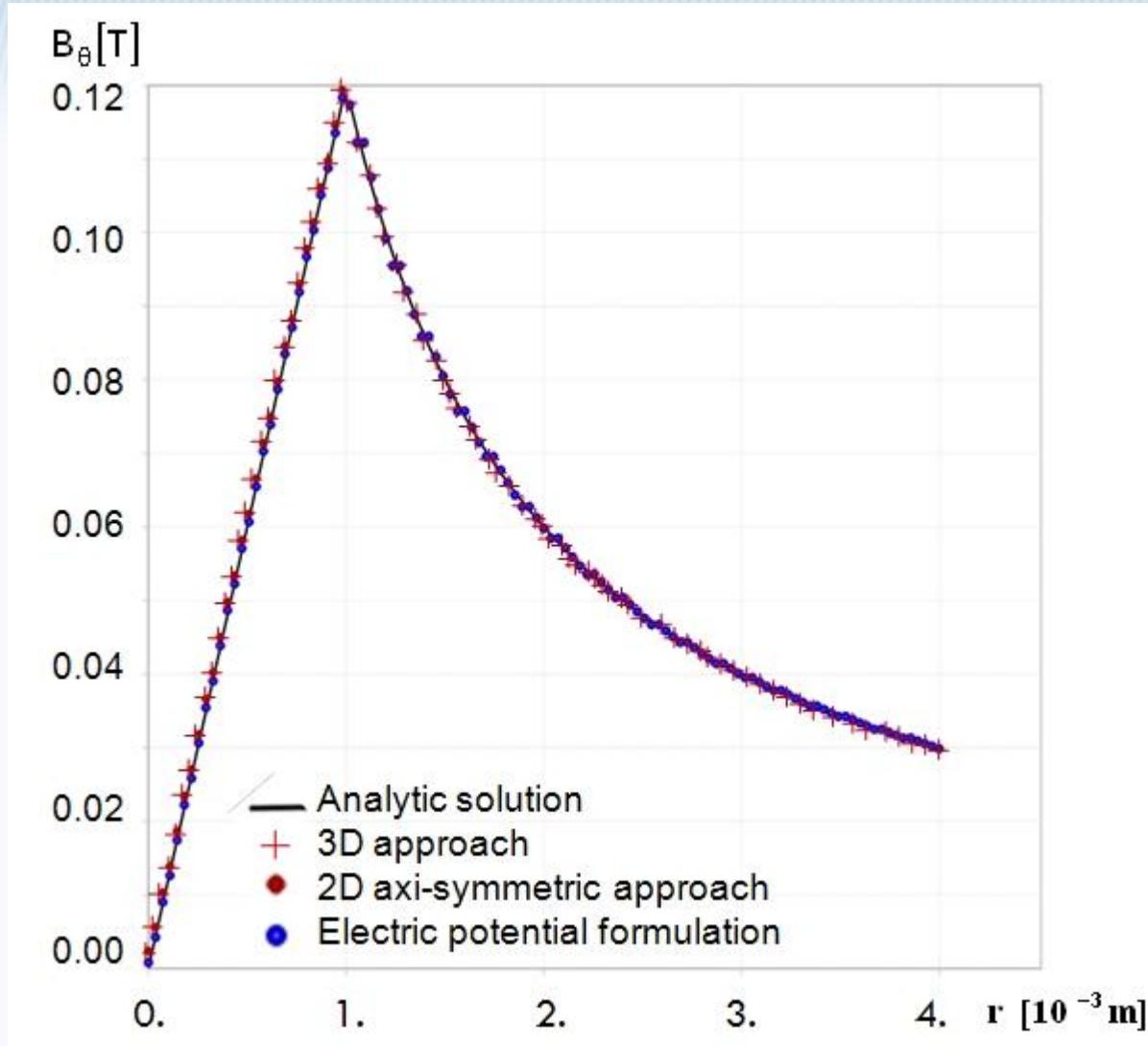
Analytic solution:

$$B_\theta(r) = \frac{\mu_0 J_{\text{axial}} r}{2} \quad \text{if } r < r_o ,$$

$$B_\theta(r) = \frac{\mu_0 J_{\text{axial}} r_o^2}{2 r} \quad \text{if } r \geq r_o$$

$\sigma = 2700 \text{ A}/(\text{V} \cdot \text{m})$

$\sigma = 10^{-5} \text{ A}/(\text{V} \cdot \text{m})$

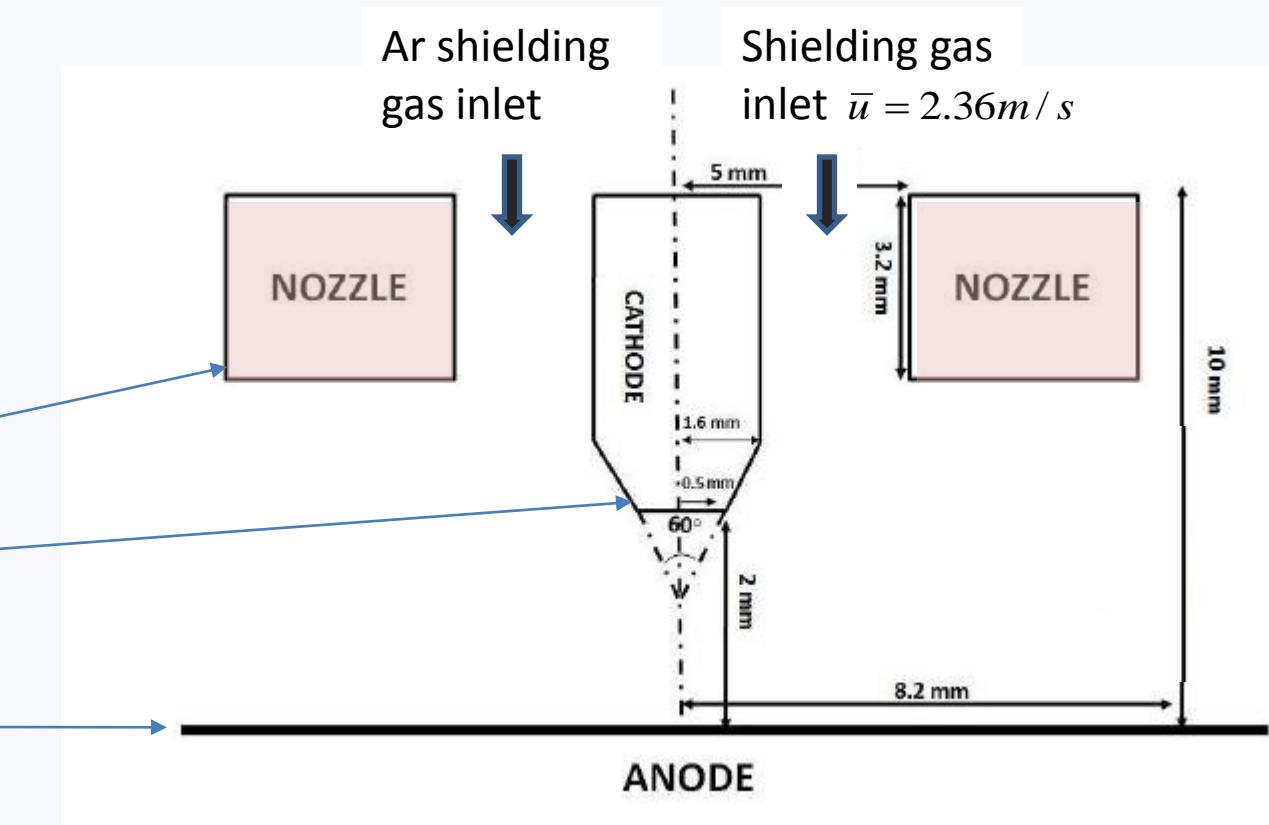


Azimuthal component of the magnetic field along the radial direction ($r_0 = 10^{-3}$ m)

Test case: Tungsten Inert Gas welding



Applied current: $I=200\text{A}$

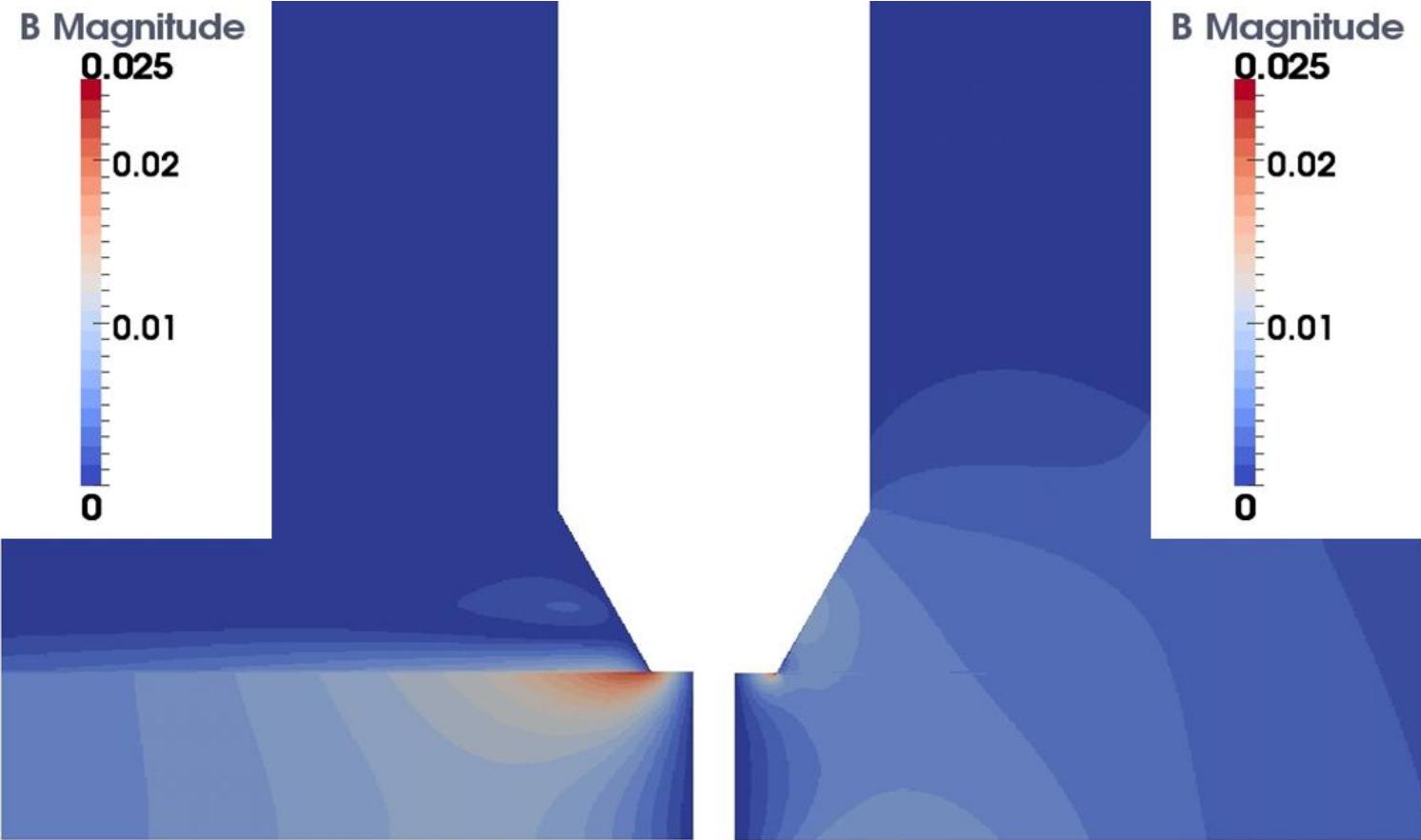


Picture of a TIG torch

Sketch of the cross section of a TIG torch

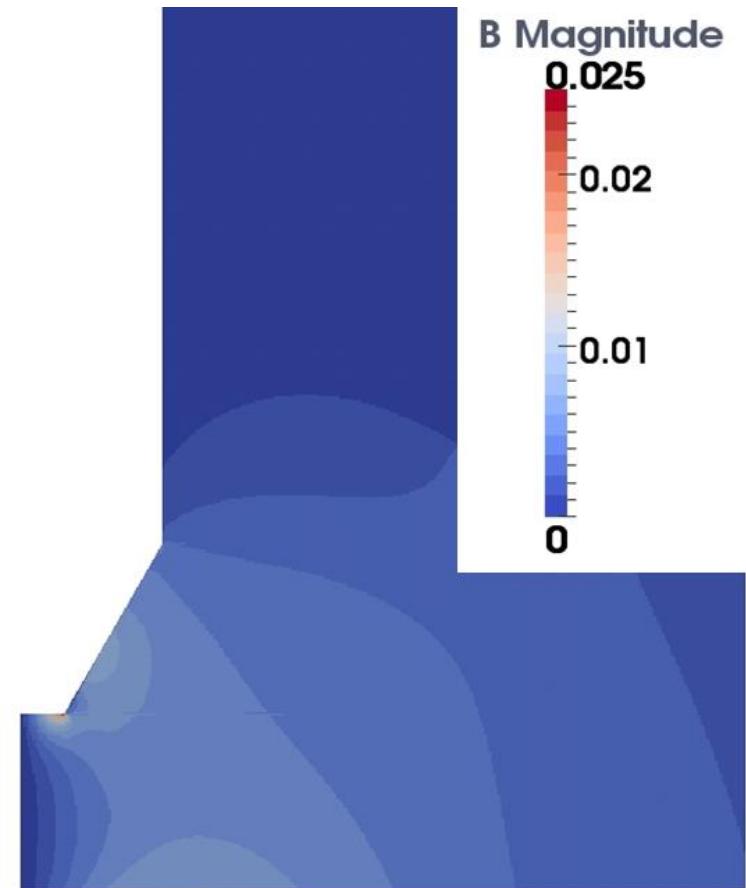
$$B_\theta(r) = \frac{\mu_0}{r} \int_0^r J_{axial}(l) l dl$$

$$B_\theta = (\nabla \times \vec{A})_\theta$$



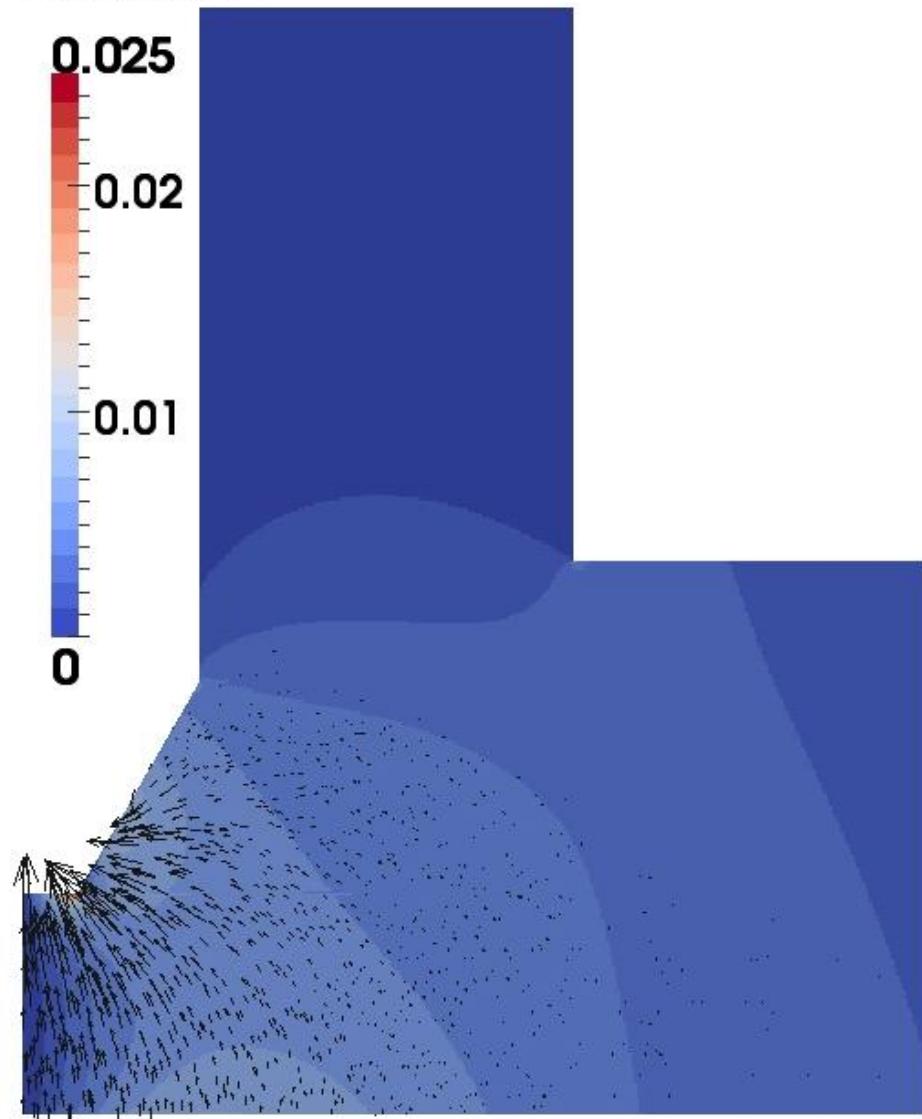
Magnetic field magnitude calculated with the electric potential formulation (left) and the axi-symmetric
one (right).

$$B_\theta = (\nabla \times \vec{A})_\theta$$



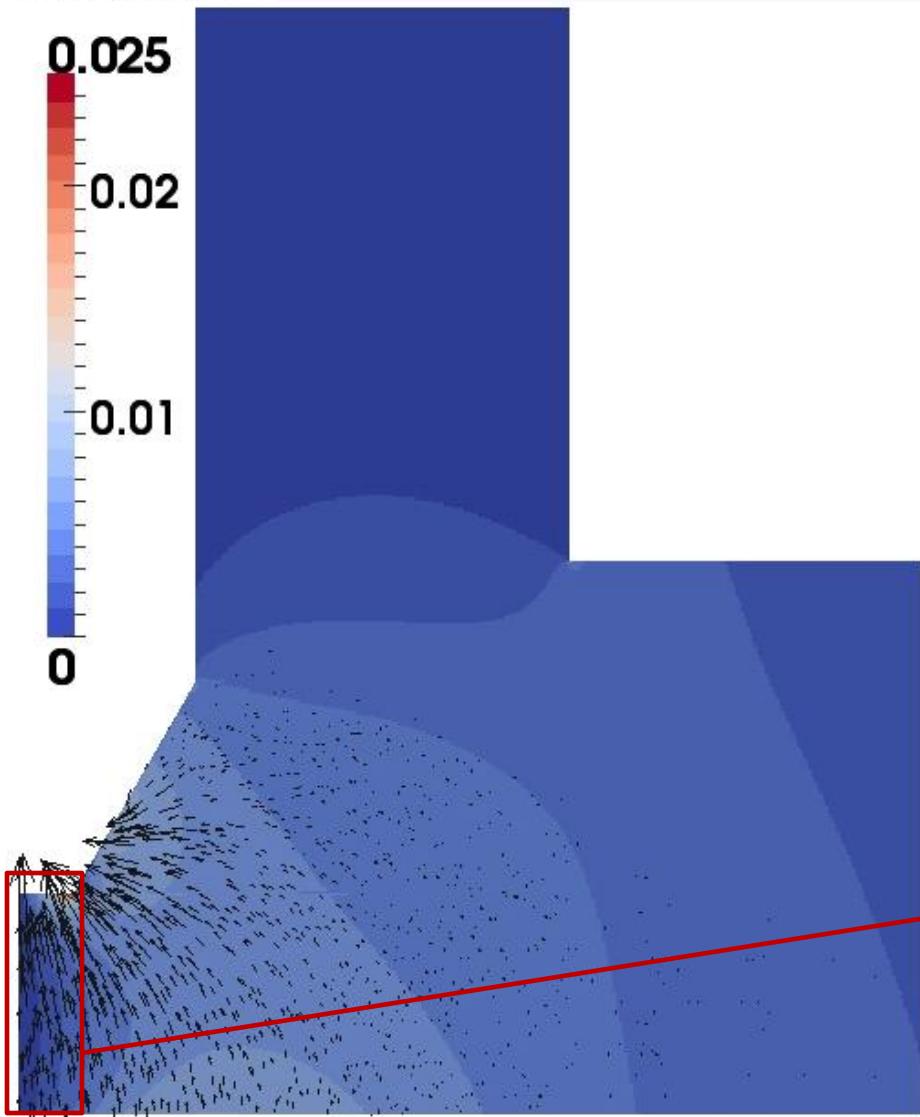
Magnetic field magnitude
calculated with the axi-

B Magnitude



Current density \vec{J}

B Magnitude

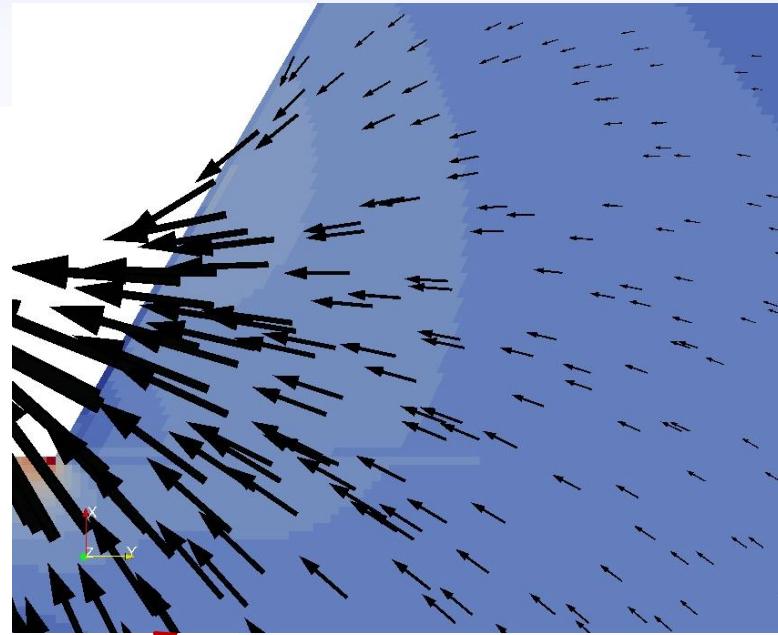
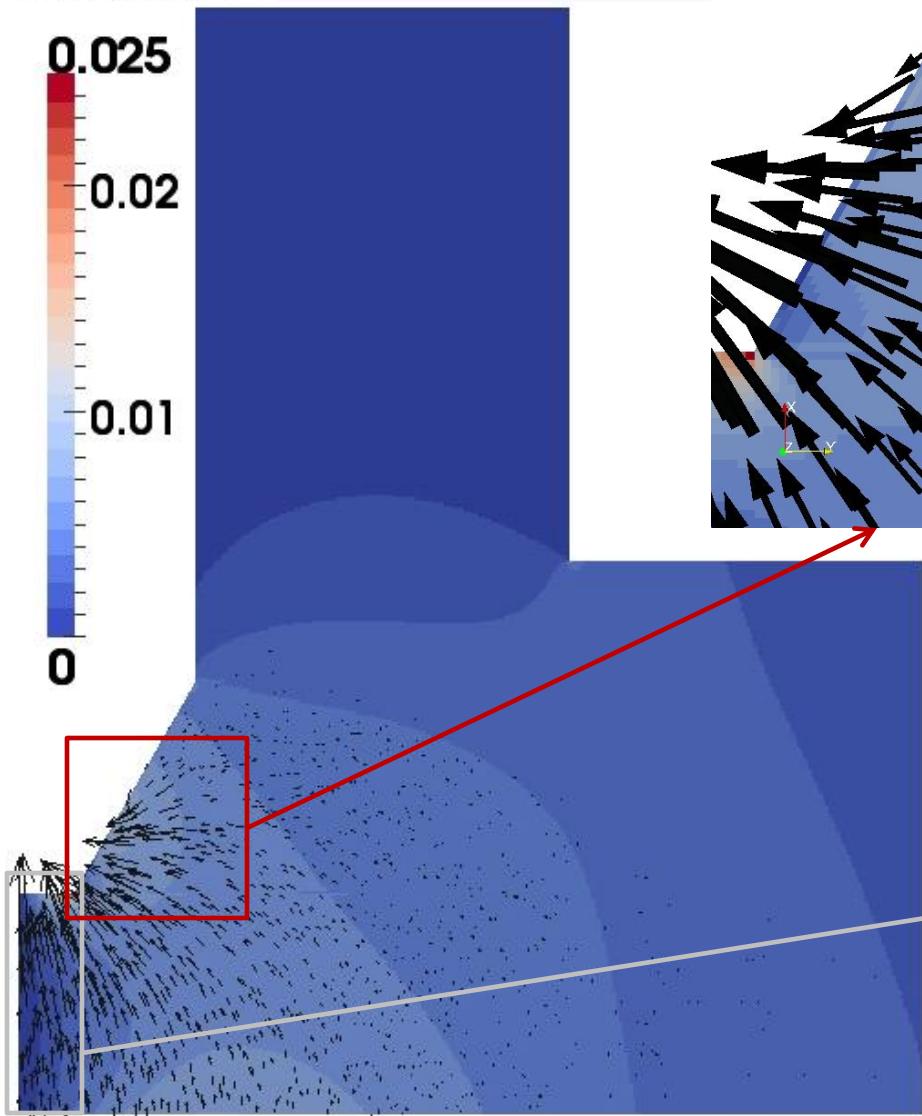


Current density \vec{J}



$$J_z \gg J_r$$

B Magnitude



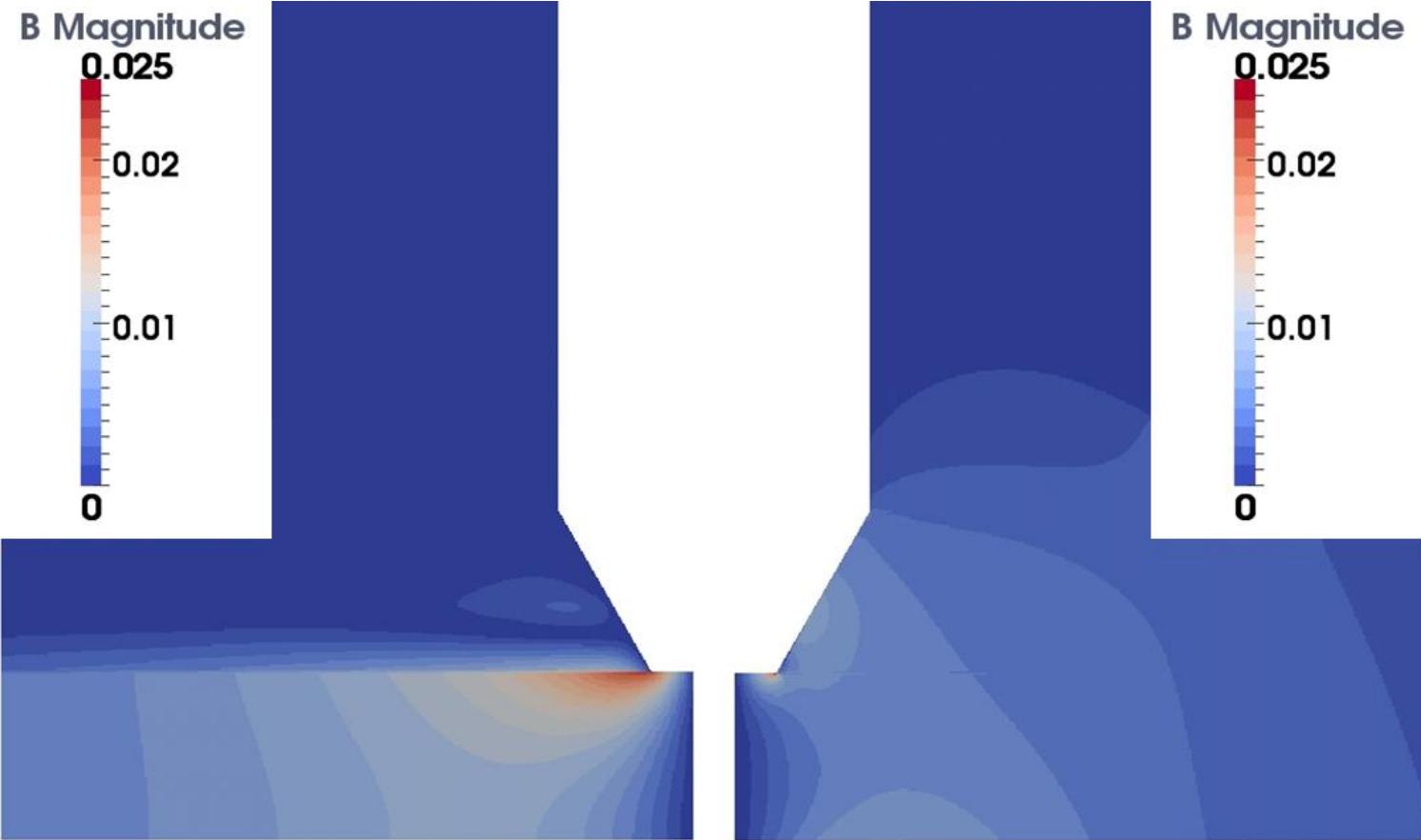
Current density \vec{J}



$J_z \gg J_r$

$$B_\theta(r) = \frac{\mu_0}{r} \int_0^r J_{axial}(l) l dl$$

$$B_\theta = (\nabla \times \vec{A})_\theta$$



Magnetic field magnitude calculated with the electric potential formulation (left) and the axi-symmetric
1 (right)

electromagnetic model / conclusion

- 3D model with $V, \vec{A} \rightarrow \vec{E}, \vec{J}, \vec{B}$
- 2D axi-symmetric models:

✓ Electric potential formulation $V \rightarrow \vec{E}, \vec{J} \rightarrow B_\theta$

✓ Magnetic field formulation $B_\theta \rightarrow \vec{E}, \vec{J}$

Conclusions

- 3D model with $V, \vec{A} \rightarrow \vec{E}, \vec{J}, \vec{B}$
- 2D axi-symmetric models:

✓

✓

✓ Electric potential formulation if

✓ Magnetic field formulation has an "additional degree of freedom"

Conclusions

- 3D model with $V, \vec{A} \rightarrow \vec{E}, \vec{J}, \vec{B}$

- 2D axi-symmetric models:

$$\checkmark V, A_r, A_z \rightarrow \vec{E}, \vec{J}, B_\theta$$

✓

✓ Electric potential if

✓ Magnetic field formulation has an "additional degree of freedom"

Conclusions

- 3D model with $V, \vec{A} \rightarrow \vec{E}, \vec{J}, \vec{B}$
 - 2D axi-symmetric models:
 - ✓ $V, A_r, A_z \rightarrow \vec{E}, \vec{J}, B_\theta$
 - ✓ $V, B_\theta \rightarrow \vec{E}, \vec{J}$
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- ✓ Magnetic field formulation has an "additional degree of freedom"

Conclusions

- 3D model with $V, \vec{A} \rightarrow \vec{E}, \vec{J}, \vec{B}$
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Conclusions

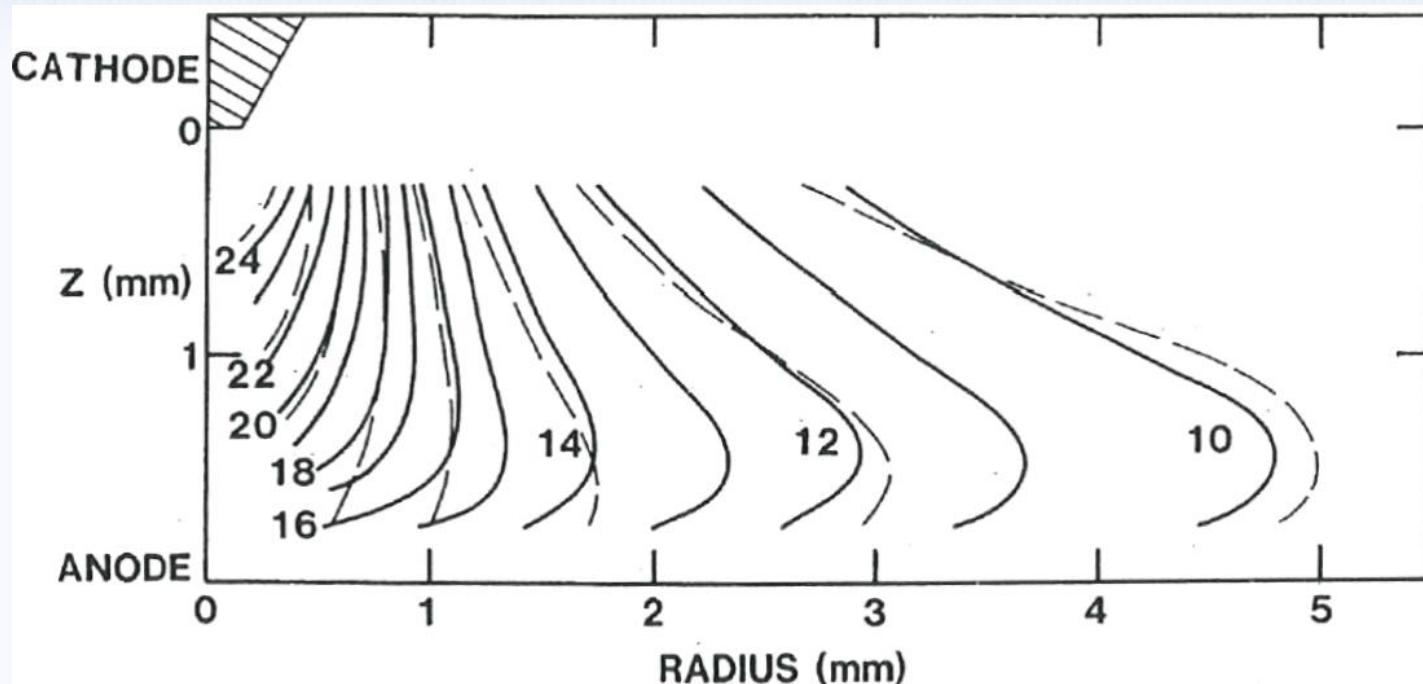
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- Acknowledgements

To Profs. Jacques Aubreton and Marie-Françoise Elchinger
for the data tables of thermodynamic and transport
properties.

To KK-foundation,
ESAB, and
the Sustainable Production Initiative at Chalmers
for their support.

Thank you for your attention !



Measured temperature profile for
a current intensity 200 A and 2 mm long

Figure from: *G.N. Haddad and A.J.D. Farmer (1985). Temperature measurements in gas tungsten arcs, Welding J., 64, pp. 339-342.*

Boundary conditions:

M.C. Tsai, and Sindo Kou (1990). Heat transfer and fluid flow in welding arcs produced by sharpened and flat electrodes, Int. J. Heat Mass Transfer, 33, pp. 2089-2098