Background	sdfibm solver	sdfIbmESI solver	Bibliography
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Implementing Immersed Boundary Method for particle representation in OpenFOAM-v2112

Chit Yan Toe

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Fluid-particle interaction problems -

- powder technology
- sediment transport
- granular mechanics
- plastic waste transport

 Background
 edf1bm solver
 edf1bmESI solver
 The End
 Bibliography

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 Different types of Computational mesh





- Time-dependent mesh
- Imposes no-slip BC on the particle surface
- Requires re-meshing for dynamic meshes

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- Time-dependent mesh
- Imposes no-slip BC on the particle surface
- Requires re-meshing for dynamic meshes

- Time-independent mesh
- A single mesh during the simulation
- No mesh for particles
- So, how can particles be recognized by the flow?

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Navier-Stokes Equations for incompressible flow

$$\frac{\partial \boldsymbol{u}}{\partial t} + \boldsymbol{u} \cdot \nabla \boldsymbol{u} = -\frac{\nabla \boldsymbol{p}}{\rho} + \nu \Delta \boldsymbol{u}$$

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Navier-Stokes Equations for incompressible flow

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Added a forcing term

$$\frac{\partial \boldsymbol{u}}{\partial t} + \boldsymbol{u} \cdot \nabla \boldsymbol{u} = -\frac{\nabla \boldsymbol{p}}{\rho} + \nu \Delta \boldsymbol{u} + \boldsymbol{f}$$

where f is the interaction force between the particle and the flow.

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Navier-Stokes Equations for incompressible flow

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This is the so-called Immersed Boundary Method (IBM).

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Navier-Stokes Equations for incompressible flow

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where f is the interaction force between the particle and the flow.

This is the so-called Immersed Boundary Method (IBM). How to impose f?

Background	sdfibm solver	sdfIbmESI solver	Bibliography
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Two groups	of IBM		

• Continuous Forcing Approach — f is added *before* numerical discretization

Background	sdfibm solver	sdfIbmESI solver	Bibliography
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- ullet Continuous Forcing Approach f is added before numerical discretization
- Discrete Forcing Approach f is added *after* numerical discretization

Background	sdfibm solver	sdfIbmESI solver	Bibliography
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Two groups	of IBM		

- Continuous Forcing Approach f is added *before* numerical discretization
- Discrete Forcing Approach f is added *after* numerical discretization
 - Indirect imposition technique Use of distribution function
 - Direct imposition technique directly impose boundary condition on the IB

Background	sdfibm solver	sdfIbmESI solver	Bibliography
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IBM in Oper	nFOAM		

• <code>OpenFOAM-v2006</code> \rightarrow <code>porousPimpleIbFoam</code> solver developed by Vergassola [1] — Continuous forcing

Background	sdfibm solver	sdfIbmESI solver	Bibliography
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- <code>OpenFOAM-v2006</code> \rightarrow <code>porousPimpleIbFoam</code> solver developed by Vergassola [1] Continuous forcing
- foam-extend-5.0 \rightarrow pimpleDyMIbFoam solver by Jasak [2] Direct forcing

Background	sdfibm solver	sdfIbmESI solver	Bibliography
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IBM in	n OpenFOAM		

- <code>OpenFOAM-v2006</code> \rightarrow <code>porousPimpleIbFoam</code> solver developed by Vergassola [1] Continuous forcing
- foam-extend-5.0 \rightarrow pimpleDyMIbFoam solver by Jasak [2] Direct forcing
- <code>OpenFOAM v9</code> \rightarrow sdfibm solver by Zhang [3] Direct forcing

Background	sdfibm solver	sdfIbmESI solver	Bibliography
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IBM in Op	enFOAM		

- <code>OpenFOAM-v2006</code> \rightarrow <code>porousPimpleIbFoam</code> solver developed by Vergassola [1] Continuous forcing
- foam-extend-5.0 \rightarrow pimpleDyMIbFoam solver by Jasak [2] Direct forcing
- <code>OpenFOAM v9</code> \rightarrow sdfibm solver by Zhang [3] Direct forcing
- This project \rightarrow sdfIbmESI solver Direct forcing + OpenFOAM-v2112

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Background	sdfibm solver	sdfIbmESI solver	Bibliography
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Direct for	ing technique		

$$\frac{\partial \boldsymbol{u}}{\partial t} + \boldsymbol{u} \cdot \nabla \boldsymbol{u} = -\frac{\nabla \boldsymbol{p}}{\rho} + \nu \Delta \boldsymbol{u} + \boldsymbol{f}$$

Background	sdfibm solver	sdfIbmESI solver	Bibliography
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Direct for	cing technique		

$$\frac{\partial \boldsymbol{u}}{\partial t} + \boldsymbol{u} \cdot \nabla \boldsymbol{u} = -\frac{\nabla \boldsymbol{p}}{\rho} + \nu \Delta \boldsymbol{u} + \boldsymbol{f}$$

Using general time discretization

$$\frac{\boldsymbol{u}^{n+1}-\boldsymbol{u}^n}{\Delta t} = \operatorname{RHS}^{n+1/2} + \boldsymbol{f}^{n+1/2}$$

Background	sdfibm solver	sdfIbmESI solver	Bibliography
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Direct for	cing technique		

$$\frac{\partial \boldsymbol{u}}{\partial t} + \boldsymbol{u} \cdot \nabla \boldsymbol{u} = -\frac{\nabla \boldsymbol{p}}{\rho} + \nu \Delta \boldsymbol{u} + \boldsymbol{f}$$

Using general time discretization

$$\frac{\boldsymbol{u}^{n+1}-\boldsymbol{u}^n}{\Delta t} = \operatorname{RHS}^{n+1/2} + \boldsymbol{f}^{n+1/2}$$

To obtain $\boldsymbol{u}^{n+1} = \boldsymbol{V}^{n+1}$,

$$\boldsymbol{f}^{n+1/2} = -\mathrm{RHS}^{n+1/2} + \frac{\boldsymbol{V}^{n+1} - \boldsymbol{u}^n}{\Delta t}$$

for some grid nodes.

Background	sdfibm solver	sdfIbmESI solver		Bibliography
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Volume-ave	erage discrete	e forcing metho	d — sdfit	om solver

Reconsider

$$abla \cdot \boldsymbol{u}_{\mathrm{f}} = 0$$
 (1)

 and

$$rac{\partial oldsymbol{u}_{\mathrm{f}}}{\partial t} + oldsymbol{u}_{\mathrm{f}} \cdot
abla oldsymbol{u}_{\mathrm{f}} = -rac{1}{
ho_{\mathrm{f}}}
abla oldsymbol{p} +
u_{\mathrm{f}}
abla^2 oldsymbol{u}_{\mathrm{f}}$$

(2)

Reconsider

$$abla \cdot \boldsymbol{u}_{\mathrm{f}} = 0$$
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$$rac{\partial oldsymbol{u}_{\mathrm{f}}}{\partial t} + oldsymbol{u}_{\mathrm{f}} \cdot
abla oldsymbol{u}_{\mathrm{f}} = -rac{1}{
ho_{\mathrm{f}}}
abla oldsymbol{p} +
u_{\mathrm{f}}
abla^2 oldsymbol{u}_{\mathrm{f}}$$

Define the volume-weighted average of velocity as

$$\boldsymbol{u} = (1 - \alpha)\boldsymbol{u}_{\mathrm{f}} + \alpha \boldsymbol{u}_{\mathrm{p}}$$

where

$$\boldsymbol{u}_{\mathrm{p}} = \boldsymbol{v}_{\mathrm{p}} + \boldsymbol{\omega}_{\mathrm{p}} \times \boldsymbol{r}.$$

(2)

Background	sdfibm solver	sdfIbmESI solver		Bibliography
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$$\boldsymbol{u} = (1 - \alpha)\boldsymbol{u}_{\mathrm{f}} + \alpha \boldsymbol{u}_{\mathrm{p}}$$

where

$$oldsymbol{u}_{\mathrm{p}} = oldsymbol{v}_{\mathrm{p}} + oldsymbol{\omega}_{\mathrm{p}} imes oldsymbol{r}.$$

We also have

$$\nabla \cdot \boldsymbol{u} = 0 \tag{3}$$

and

$$\frac{\partial \boldsymbol{u}}{\partial t} = \boldsymbol{H} - \nabla \boldsymbol{P} + \boldsymbol{f}_{\mathrm{p}}$$
⁽⁴⁾

where

$$\boldsymbol{H} \equiv -\boldsymbol{u}\cdot\nabla\boldsymbol{u} + \nu_{\mathrm{f}}\nabla^{2}\boldsymbol{u}$$

and $P \equiv p/\rho_{\rm f}$ and $\boldsymbol{f}_{\rm p}$ is the interaction force.

Chit Yan Toe

(2)



Contd.

$$\frac{\partial \boldsymbol{u}}{\partial t} = \boldsymbol{H} - \nabla \boldsymbol{P} + \boldsymbol{f}_{\mathrm{p}}$$

where

$$\boldsymbol{H} \equiv -\boldsymbol{u} \cdot \nabla \boldsymbol{u} + \nu_{\rm f} \nabla^2 \boldsymbol{u}$$

In other words, $f_{\rm p}$ is the force required to adjust the single-phase fluid velocity $u_{\rm f}$ to the averaged velocity u.

Contd.

$$\frac{\partial \boldsymbol{u}}{\partial t} = \boldsymbol{H} - \nabla \boldsymbol{P} + \boldsymbol{f}_{\mathrm{p}}$$

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In other words, $f_{\rm p}$ is the force required to adjust the single-phase fluid velocity $u_{\rm f}$ to the averaged velocity u.

Using general time discretization

$$\boldsymbol{u}^{n+1} = \boldsymbol{u}^n + \Delta t \left(\boldsymbol{H} - \nabla \boldsymbol{P} + \boldsymbol{f}_{\mathrm{p}} \right)$$

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Contd.

$$\frac{\partial \boldsymbol{u}}{\partial t} = \boldsymbol{H} - \nabla \boldsymbol{P} + \boldsymbol{f}_{\mathrm{p}}$$

where

$$\boldsymbol{H} \equiv -\boldsymbol{u} \cdot \nabla \boldsymbol{u} + \nu_{\rm f} \nabla^2 \boldsymbol{u}$$

In other words, $f_{\rm p}$ is the force required to adjust the single-phase fluid velocity $u_{\rm f}$ to the averaged velocity u.

Using general time discretization

$$\boldsymbol{u}^{n+1} = \boldsymbol{u}^n + \Delta t \left(\boldsymbol{H} - \nabla \boldsymbol{P} + \boldsymbol{f}_{\mathrm{p}} \right)$$

Without interaction force,

$$\hat{\boldsymbol{u}} = \boldsymbol{u}^n + \Delta t \left(\boldsymbol{H} - \nabla P \right)$$

Contd.

$$\frac{\partial \boldsymbol{u}}{\partial t} = \boldsymbol{H} - \nabla \boldsymbol{P} + \boldsymbol{f}_{\mathrm{p}}$$

where

$$\boldsymbol{H} \equiv -\boldsymbol{u} \cdot \nabla \boldsymbol{u} + \nu_{\rm f} \nabla^2 \boldsymbol{u}$$

In other words, $f_{\rm p}$ is the force required to adjust the single-phase fluid velocity $u_{\rm f}$ to the averaged velocity u.

Using general time discretization

$$\boldsymbol{u}^{n+1} = \boldsymbol{u}^n + \Delta t \left(\boldsymbol{H} - \nabla \boldsymbol{P} + \boldsymbol{f}_{\mathrm{p}} \right)$$

Without interaction force,

$$\hat{\boldsymbol{u}} = \boldsymbol{u}^n + \Delta t \left(\boldsymbol{H} - \nabla \boldsymbol{P} \right)$$

Therefore, $\boldsymbol{u}^{n+1} - \boldsymbol{\hat{u}} = \Delta t \boldsymbol{f}_{\mathrm{p}}$



Contd. We know that $\boldsymbol{u}^{n+1} - \boldsymbol{\hat{u}} = \Delta t \boldsymbol{f}_{\mathrm{p}}.$



Contd. We know that $\boldsymbol{u}^{n+1} - \hat{\boldsymbol{u}} = \Delta t \boldsymbol{f}_{\mathrm{p}}.$

• For the solid cell, we require $\boldsymbol{u}^{n+1} = \boldsymbol{u}_p$, therefore we get

$$m{f}_{\mathrm{p}} = rac{m{u}_{\mathrm{p}} - m{\hat{m{u}}}}{\Delta t}$$



Contd. We know that $\boldsymbol{u}^{n+1} - \boldsymbol{\hat{u}} = \Delta t \boldsymbol{f}_{\mathrm{p}}.$

• For the solid cell, we require $\boldsymbol{u}^{n+1} = \boldsymbol{u}_p$, therefore we get

$$m{f}_{
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m p} - m{\hat{m{u}}}}{\Delta t}$$

 $\bullet\,$ For the fluid cell, we require no interaction force, therefore ${\pmb f}_{\rm p}={\pmb 0}$



Contd. We know that $\boldsymbol{u}^{n+1} - \boldsymbol{\hat{u}} = \Delta t \boldsymbol{f}_{\mathrm{p}}.$

• For the solid cell, we require $\boldsymbol{u}^{n+1} = \boldsymbol{u}_p$, therefore we get

$$m{f}_{\mathrm{p}} = rac{m{u}_{\mathrm{p}} - m{\hat{m{u}}}}{\Delta t}$$

- For the fluid cell, we require no interaction force, therefore $m{f}_{
 m p}=m{0}$
- For the interface cell, we get

$$\boldsymbol{f}_{\mathrm{p}} = \alpha \frac{\boldsymbol{u}_{\mathrm{p}} - \hat{\boldsymbol{u}}}{\Delta t}$$

where α needs to determined by geometrical functions.

Background	sdfibm solver	sdfIbmESI solver	Bibliography
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How to cald	culate α ?		



Fraction of AB lying within the surface S is simply the ratio: $-\varphi_A/(\varphi_B - \varphi_A)$

Background sdfibm solver sdfibmESI solver The End Bibliography o

Implementation of sdfibm solver

Directory of sdfibm solver

- 1 |-- CMakeLists.txt
- 2 |-- LICENSE.txt
- 3 |-- README.md
- 4 |-- examples
- 5 |-- figs
- 6 |-- src
- 7 '-- tool_vof

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Listing 1: Creation of solidcloud object in main.cpp of sdfibm solver

```
1 #include "solidcloud.h"
2
3 int main(int argc, char *argv[])
4 {
      // #include "--.H"
5
      std::string dictfile;
6
      if(runTime.time().value() > 0)
7
      ł
8
          if(!Foam::Pstream::parRun())
9
               dictfile = mesh.time().timeName() + "/solidDict";
10
          else
11
               dictfile = "processor0/" + mesh.time().timeName() + "/solidDict";
12
      }
13
      else
14
      Ł
15
          dictfile = "solidDict":
16
      3
17
      sdfibm::SolidCloud solidcloud(args.path() + "/" + dictfile, U, runTime.value
18
       ()):
      solidcloud.saveState(); // write the initial condition
19
```

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Listing 2: Solving momentum equations in main.cpp of sdfibm solver

```
while (runTime.loop())
20
      ł
          Foam::Info << "Time = " << runTime.timeName() << Foam::endl;</pre>
23
          #include "CourantNo.H"
          Foam::dimensionedScalar dt = runTime.deltaT();
24
          if(solidcloud.isOnFluid())
25
           ſ
26
               Foam::fvVectorMatrix UEqn(
27
                   fvm::ddt(U)
28
                 + 1.5*fvc::div(phi, U) - 0.5*fvc::div(phi.oldTime(), U.oldTime())
29
                 ==0.5*fvm::laplacian(nu, U) + 0.5*fvc::laplacian(nu, U));
30
               UEan.solve():
31
32
               phi = linearInterpolate(U) & mesh.Sf();
33
               Foam::fvScalarMatrix pEqn(fvm::laplacian(p) == fvc::div(phi)/dt -
34
       fvc::div(Fs)):
               pEqn.solve();
35
```

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Listing 3: Solving momentum equations in main.cpp of sdfibm solver

```
Ħ
                           - dt*fvc::grad(p);
                    = U
37
               phi = phi - dt*fvc::snGrad(p)*mesh.magSf();
38
39
               Foam::fvScalarMatrix TEqn(
40
                    fvm::ddt(T)
41
                  + fvm::div(phi, T)
42
                  ==fvm::laplacian(alpha, T));
43
               TEqn.solve();
44
           }
45
```

Listing 4: Fluid-particle interaction main.cpp of sdfibm solver

```
solidcloud.interact(runTime.value(), dt.value());
46
           if(solidcloud.isOnFluid())
47
           £
48
               U = U - Fs*dt:
49
               phi = phi - dt*(linearInterpolate(Fs) & mesh.Sf());
50
               U.correctBoundaryConditions();
51
               adjustPhi(phi, U, p);
52
               T = (1.0 - As) * T + Ts:
               T.correctBoundaryConditions();
54
               #include "continuityErrs.H"
55
           3
56
           solidcloud.evolve(runTime.value(), dt.value());
57
           solidcloud.saveState();
58
           if(solidcloud.isOnFluid())
59
           ł
60
               solidcloud.fixInternal(dt.value());
           }
62
```

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Listing 5: Saving output file main.cpp of sdfibm solver

```
if(runTime.outputTime())
63
           Ł
                runTime.write():
65
66
                if(Foam::Pstream::master())
67
                ſ
68
                    std::string file_name;
                    if(Foam::Pstream::parRun())
70
                         file_name = "./processor0/" + runTime.timeName() + "/
71
       solidDict";
                    else
72
                         file_name = "./" + runTime.timeName() + "/solidDict";
73
                    solidcloud.saveRestart(file_name);
74
                }
75
           }
76
77
      Foam::Info << "DONE\n" << endl;</pre>
78
      return 0;
79
80 | }
```





Figure: Computational domain.

Figure: Result of pimpleDyMIbFoam solver.

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Figure: Computational domain.



Figure: Result of pimpleDyMIbFoam solver.



Background	sdfibm solver	sdfIbmESI solver	Bibliography
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Re-impleme	ntation — sdf]	bmESI solver	

- Main difference is in compilation procedure
 - CMake in OpenFOAM v9
 - wmake in OpenFOAM-v2112 \rightarrow Make folder is required.

Background	sdfibm solver	sdfIbmESI solver	Bibliography
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Re-implement	ntation — sdf]	bmESI solver	

- Main difference is in compilation procedure
 - CMake in OpenFOAM v9
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- Some minor differences e.g.
 - type conversion vector() function, readScalar function
 - #include "IFstream.H" in solidcloud.C file

Background	sdfibm solver	sdfIbmESI solver	Bibliography
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- Main difference is in compilation procedure
 - CMake in OpenFOAM v9
 - wmake in OpenFOAM-v2112 \rightarrow Make folder is required.
- Some minor differences e.g.
 - type conversion vector() function, readScalar function
 - #include "IFstream.H" in solidcloud.C file
- no main.cpp file in OpenFOAM-v2112, but sdfIbmESI.C file

Directory of sdfibmESI solver

1	sdfIbmESI/
2	Make
3	I UEqn.H
4	I correctPhi.H
5	I createFields.H
6	I pEqn.H
7	sdflbmESI.C
8	' setRDeltaT.H
- 1	

Background	sdfibm solver	sdfIbmESI solver	Bibliography
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Re-implement	ntation — sdf1	bmESI solver	

Start with library files — libcollision, libshape, libmaterial, libmotion

```
collision.h of sdfibm solvercollision.H of sdfibmESI solver1#ifndef COLLISION_HPP12#define COLLISION_HPP2334#include "../types.h"45#include "../utils.h"56#include "../solid.h"6
```



Start with library files — libcollision, libshape, libmaterial, libmotion



options file in Make folder of libcollision library







Background	sdfibm solver	sdfIbmESI solver	Bibliography
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- \bullet Download the files from GitHub repository sdfIbmESI solver
 - \$ git clone https://github.com/ChitYanToe/sdfIbmESI.git
- Run the script for compiling and running the simulation.
 - \$./Allrun
- Or, for manual compilation instead of using Allrun file, one needs to run \$ source exportFile.sh

Background	sdfibm solver	sdfIbmESI solver	The End	Bibliography
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Thank you for your time.

Q & A.

Background	sdfibm solver	sdfIbmESI solver	Bibliography
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