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#### CFD WITH OPENSOURCE SOFTWARE

A COURSE AT CHALMERS UNIVERSITY OF TECHNOLOGY TAUGHT BY HÅKAN NILSSON

## Implementation of library for acoustic sound pressure and spanwise correction

Developed for OpenFOAM-3.0.x Requires: AcousticAnalogy library

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# Learning outcomes

The reader will learn:

#### How to use it:

• How to use the acousticAnalogy library

#### The theory of it:

• The theory of the Curle's acoustic analogy and the spanwise correction

#### How it is implemented:

• The implementation of the AcousticAnalogyCorr library

#### How to modify it:

• How to modify the AcousticAnalogy library for the spanwise correction

# Prerequisites

The reader is expected to know the following in order to get maximum benefit out of this report:

- $\bullet\,$  Fundementals of acoustics
- It is recommended to have a look at paper [1] for understanding the method for spanwise correction

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# **Preface**

In this tutorial, the AcousticAnalogy library is introduced to calculate the sound pressure generated from a bluff body based on the acoustic wave equation. This library is developed by M. Heinrich and uploaded on the course website [2]. The library predicts the acoustic sound using Curle's analogy method.

When long-span bodies such as cylinder or airfoil are studied for their noise emission, it can be computationally expensive to simulate the large spatial domain which covers the whole section of the body. This tutorial extends the AcousticAnalogy library so that the sound pressure generated from the entire body surface can be obtained using the pressure field data of the computed domain based on the spanwise correction method.

## Chapter 1

# Theory

This chapter explains briefly the Curle's acoustic analogy, which the AcousticAnalogy library is based on and the method to correct sound pressure for the long-span body. The following section shows the expression of sound pressure p', which is obtained from the pressure and velocity fields. These flow field data are computed by the CFD solver. Since no interaction between the flow field and the sound field is assumed here, the calculation of sound is independent on the solution of the CFD simulations and thus is post-processing.

#### 1.1 Curle's acoustic analogy

Here the fluid is assumed homogenous at rest. In order to study acoustics, we will express the pressure or the density as  $p(\mathbf{x},t) = p_0 + p'(\mathbf{x},t)$ ,  $\rho(\mathbf{x},t) = \rho_0 + \rho'(\mathbf{x},t)$ , which are the summation of disturbance p',  $\rho'$  from the equilibrium state and constant values  $p_0$ ,  $\rho_0$  at rest. The wave equation for p' is derived from the equations for conservation of mass and momentum. It is expressed as

$$\frac{1}{c_0} \frac{\partial^2 p'}{\partial t^2} - \nabla^2 p' = 0 \tag{1.1}$$

where  $c_0$  is the sound speed at rest. The propagation of the acoustic sound p' can be described by the solution for the wave equation, which can be generally obtained by applying the Gauss theorem.

The acoustic analogies, which are derived based on the wave equation, are used to predict noise in engineering applications. These analogies take different formations depending on the assumptions for derivation. The Curle's equation is one of the acoustic analogies and takes into consideration the influence of static solid boundaries upon the sound field, i.e., the Curle's analogy can be applied for the cases where a static object is placed in a fluid. It represents the disturbance of the density  $\rho'(x,t)$  with integrals of the total volume V external to the solid boundaries and the surface S of the boundaries as

$$\rho'(\boldsymbol{x},t) = \frac{1}{4\pi c_0^2} \frac{\partial^2}{\partial x_i \partial x_j} \int_V \frac{T_{ij}}{r} dV(\boldsymbol{y}) - \frac{1}{4\pi c_0^2} \frac{\partial}{\partial x_i} \int_S \frac{n_j}{r} (p\delta_{ij} - \tau_{ij}) dS(\boldsymbol{y})$$
(1.2)

where  $r = |\mathbf{x} - \mathbf{y}|$  is the distance between the observer  $\mathbf{x}$  and the sound source  $\mathbf{y}$ ,  $n_j$  is the ourward surface normal from the fluid,  $T_{ij}$  is the Lighthill's stress tensor, which is  $\rho v_i v_j + p_{ij} - c_0^2 \rho \delta_{ij}$ , and  $\tau_{ij}$  is  $\rho v_i v_j$ . The detailed derivation is described in the reference [3].

Larsson *et al.* [4] rewrites Equation (1.2) based on the formations by Brentner and Farassat [5]. The spatial derivative is converted to a temporal one and the  $\frac{\partial r}{\partial x_i}$  term becomes

$$\frac{\partial r}{\partial x_i} = \frac{\partial \sqrt{(x_j - y_j)^2}}{\partial x_i} = \frac{x_i - y_i}{r} = l_i \tag{1.3}$$

where  $l_i$  is a unit vector pointing from the source location to the observer. Equation (1.2) is modified on a form where the derivatives are taken inside the integral, and the sound pressure  $p'(\boldsymbol{x},t)$  is expressed as

$$p'(\boldsymbol{x},t) = \frac{1}{4\pi} \int_{V} \left( \frac{l_{i}l_{j}}{c_{0}^{2}r} \ddot{T}_{ij} + \frac{3l_{i}l_{j} - \delta_{ij}}{c_{0}r^{2}} \dot{T}_{ij} + \frac{3l_{i}l_{j} - \delta_{ij}}{r^{3}} T_{ij} \right) dV(\boldsymbol{y}) + \frac{1}{4\pi} \int_{S} l_{i}n_{j} \left( \frac{\dot{p}\delta_{ij} - \dot{\tau}_{ij}}{c_{0}r} + \frac{p\delta_{ij} - \tau_{ij}}{r^{2}} \right) dS(\boldsymbol{y}). \quad (1.4)$$

Equation (1.4) takes the same formation as written in the code.

#### 1.2 Spanwise correction

There are some methods which predict the total sound pressure of long-span bodies, e.g. cylinder, airfoil, plate, so on, based on the pressure radiated from a part of the span section. Their approach can be applied to extrapolate the sound pressure outside the computational domain. Here, an approach by Kato et al. [1] is introduced, which models the frequency characteristics of pressure to consider the phase shift in the spanwise direction. The procedure for correction is shown in Figure 1.1. The total span length of the body is L, and the length of which part intersects in the computational domain is  $L_s$ .

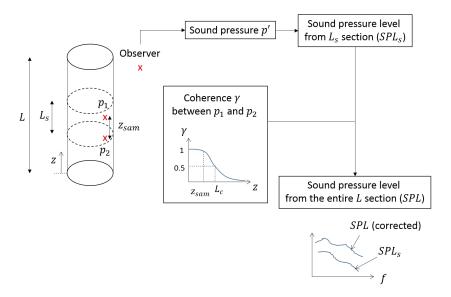


Figure 1.1: Calculation procedure for spanwise correction

The sound pressure level (SPL) is a logarithmic scale of the sound pressure expressed by  $20 \log_{10}(p'/p_{ref})$  dB (decibel).  $p_{ref}$  is a reference pressure that is typically the threshold of human hearing,  $2 \times 10^{-5}$  Pa. The SPL in the frequency domain corrected by the Kato's method,  $20 \log_{10}(p'_{corr}/p_{ref})$ , is described as follows

$$SPL(f) \equiv \begin{cases} SPL_s(f) + 20\log(L/L_s) & (L \le L_c(f)) & (1.5a) \\ SPL_s(f) + 20\log\{L_c(f)/L_s\} + 10\log\{L/L_c(f)\} & (L_s \le L_c(f) \le L) & (1.5b) \\ SPL_s(f) + 10\log(L/L_s) & (L_c(f) \le L_s) & (1.5c) \end{cases}$$

where  $SPL_s$  is the value directly calculated from the source in the computed region as shown in the figure. The coherence function  $\gamma(f,z)$  can be defined from coherence between surface pressure at

two points apart by distance z in the spanwise direction, which are  $p_1$  and  $p_2$  depicted in the figure. The spanwise coherence length  $L_c(f)$  is the distance z when  $\gamma(f,z)$  is 0.5.

The above equations are rewritten so that the sound pressure  $p'_{corr}$  can be simply expressed using a correction coefficient  $r_{corr}$  as  $p'_{corr} = r_{corr}p'$  where

$$\left(\begin{array}{ccc}
L/L_s & (L \le L_c(f)) & (1.6a) \\
\hline
\sqrt{L_s} & (L \le L_c(f)) & (1.6a)
\end{array}\right)$$

$$r_{corr}(f) \equiv \begin{cases} L/L_s & (L \le L_c(f)) \\ \sqrt{LL_c}/L_s & (L_s \le L_c(f) \le L) \\ \sqrt{L/L_s} & (L_c(f) \le L_s) \end{cases}$$
(1.6a) (1.6b)

The coherence function  $\gamma(f,z)$  needs to be calculated in order to find  $L_c$  at each frequency. Given signals at two locations z = x, y, the coherence function is generally represented as the ratio of the

cross power spectral density,  $W_{xy}(f)$ , to the power spectral densities,  $W_{xx}(f)$  and  $W_{yy}(f)$ .

$$\gamma(f) = \frac{|W_{xy}(f)|^2}{W_{xx}(f) \cdot W_{yy}(f)}$$
(1.7)

The two signals correspond to  $p_1$  and  $p_2$  in our case. Since  $\gamma(f,z)$  is also the function of z, it is theoretically necessary to have the surface pressure at all points along the z direction in order to determine  $\gamma(f,z)$  for each z. However, instead of sampling pressure at all points,  $\gamma(f,z)$  is approximated in the code according to the idea by Siddon [6] for simplification. He noted that the correlation of the surface pressure can be modeled by the Gaussian function.

$$\gamma(f,z) = \exp\left(-\frac{z^2}{2l(f)^2}\right) \tag{1.8}$$

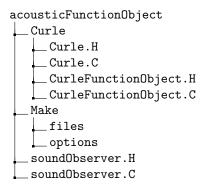
l is a constant but is dependent on frequency. For a certain frequency f, the value of  $\gamma(f, z_{samp})$  can be obtained from the sampled surface pressure  $p_1$  and  $p_2$  which are apart by distance  $z_{samp}$ . Then l is determined, and  $\gamma(f,z)$  is found as a function z.  $L_c(f)$  is the value of z=z' which satisfies  $\gamma(f,z')=0.5$ . By doing so, the code samples the surface pressure  $p_1$  and  $p_2$  at only two points.

## Chapter 2

# AcousticAnalogy library

This chapter describes how the function object, the AcousticAnalogy library, which was developed by M. Heinrich [2], calculates the sound pressure based on the Curle's acoustic analogy. This library is implemented as functionObject for OpenFOAM 3.0.x, and it is intended for solving incompressible flow. A user gives the patch names of the surface, the density at rest, the sound speed, and the observer positions as inputs. Time histories of the sound pressure received at each observer are written to a file created under postProcessing directory.

The top-level directory acousticFunctionObject consists of the following files.



The Curle.C file is the main source file, which describes the definition of the Curle class to mainly calculate the sound pressure p'. The soundObserver.C file defines the SoundObserver class, which is called inside the Curle class and stores both the positions of the observers and the received sound pressure.

#### 2.1 Curle class

Some important member functions in the Curle class will be explained in this section. One of the member data observers\_ in the Curle class is declared as

#### List<SoundObserver> observers\_;

which is a list of the SoundObserver class type. As explained in the next section, the SoundObserver class stores data for the position of the observer and the sound pressure. Each element in the list holds the information for each observer.

The read member function reads the input entries, such as the sound speed, the density of fluid, information of the observers, and so on, that a user specifies in the case directory. This function also stores the observer's names and positions in observers.

The calculate member function calculates the sound pressure p' received at each observer, which consists of the volume and the surface integrals as expressed in Equation (1.4). The calculate function calculates the term for the volume integral as follows.

```
SoundObserver& obs = observers_[obsI];
        scalar pPrime = 0.0;
429
430
        // Volume integral
431
        if (cellZoneID_ != -1)
433
            // List of cells in cellZoneID
            const labelList& cells = mesh.cellZones()[cellZoneID_];
436
            // Cell volume and cell center
437
            const scalarField& V = mesh.V();
            const vectorField& C = mesh.C();
            // Loop over all cells
441
            forAll(cells, i)
442
            {
                label cellI = cells[i];
444
                // Distance to observer
                scalar r = mag(obs.position() - C[cellI]);
                vector l = (obs.position() - C[cellI]) / r;
448
                // Calculate pressure fluctuation
                pPrime += coeff * V[cellI] *
452
                             ((1*1) && d2Tijdt2[cellI]) / (cRef_ * cRef_ * r)
453
                           + ((3.0 * 1*1 - I) && dTijdt[cellI]) / (cRef_ * r * r)
                           + ((3.0 * 1*1 - I) && Tij[cellI]) / (r * r * r)
                         );
456
            }
457
            reduce(pPrime, sumOp<scalar>());
458
        }
459
```

The positions of observers are read from the list observers\_ in line 428. pPrime corresponds to the sound pressure p'. coeff is a constant,  $1/4\pi$ . If the equation for pPrime is compared with Equation (1.4), 1 is the vector  $l_{i,j}$ , cRef\_ is the sound speed  $c_0$ , r is the distance r. Tij, dTijdt, and d2Tijdt2 are other member functions of the Curle class which return the Lighthill tensor  $T_{ij}$  and its first and second time derivatives,  $\dot{T}_{ij}$  and  $\ddot{T}_{ij}$  respectively. Tij is simply calculated by  $\rho_0 UU^T$ , and the function for Tij is defined as follows.

```
Foam::tmp<Foam::volTensorField> Foam::Curle::Tij() const

foam::tmp<foam::volTensorField> foam::tmp<foam::volTensorField> foam::tmp<foam::volTensorField> foam::volTensorField> foam::tmp<foam::volTensorField> foam::volTensorField> foam::vol
```

dTijdt and d2Tijdt2 are obtained based on the second-order backward differencing time derivative

and the first-order Euler second time derivative methods, respectively. Thus the functions for dTijdt and d2Tijdt2 load the velocity fields of the current and last two time steps.

The term of the surface integral is written as follows.

```
// Surface integral - loop over all patches
       forAllConstIter(labelHashSet, patches_, iter)
462
463
            // Get patch ID
            label patchI = iter.key();
466
            // Surface area vector and face center at patch
            vectorField Sf = mesh.Sf().boundaryField()[patchI];
468
            vectorField Cf = mesh.Cf().boundaryField()[patchI];
470
            // Normal vector pointing towards fluid
            vectorField n = -Sf/mag(Sf);
472
            // Pressure field and time derivative at patch
474
            scalarField pp = p.boundaryField()[patchI];
            scalarField dpdtp = dpdt.boundaryField()[patchI];
            // Lighthill tensor on patch
478
            tensorField Tijp = Tij.boundaryField()[patchI];
479
            tensorField dTijdtp = dTijdt.boundaryField()[patchI];
            // Distance surface-observer
482
            scalarField r = mag(obs.position() - Cf);
483
            vectorField l = (obs.position() - Cf) / r;
485
            // Calculate pressure fluctuations
            pPrime += coeff * gSum
487
            (
                (
489
                     (1*n)
                  &&
491
                         (dpdtp*I - dTijdtp) / (cRef_*r)
493
                        (pp*I - Tijp) / sqr(r)
                )
496
              * mag(Sf)
497
            );
       }
499
        obs.pPrime(pPrime);
500
```

n is the surface normal  $n_j$  and mag(Sf) is the surface area. p and dpdtp are the member functions which return the pressure and its time derivative. The functions for p and dpdtp are defined as follows.

The fvc::ddt class returns information about the time scheme, thus dpdt is derived based on the time scheme specified in fvSchemes of the case directory. After both the volume and surface integrals are obtained, the total sound pressure pPrime is stored in the obj object in line 500.

The writeCurle member function writes the sound pressure each time step to both the log file and a file placed in the postProcessing directory as follows.

#### 2.2 SoundObserver class

As shown above, the main Curle class calculates the sound pressure received at each observer. Each sound pressure is stored in each element of the list of the SoundObserver class type. The SoundObserver class does nothing for calculations but is needed to store data for the position of the observer and the sound pressure.

The member data in the SoundObserver class are as follows.

```
//- Name of the sound observer
       word name_;
56
       //- Position of the sound observer
58
       vector position_;
60
       //- Pressure fluctuation [Pa]
61
       scalar pPrime_;
62
   The member functions are as follows.
       //- Return name
       const word& name() const
85
       {
            return name_;
87
       }
89
       //- Return position of observer
       const vector& position() const
91
       {
92
            return position_;
93
```

}

94

```
//- Return fluctuation pressure
const scalar& pPrime() const
{
    return pPrime_;
}

//- Set fluctuating pressure
void pPrime(scalar pPrime);
```

A user has to give the names and positions for each observer, which are stored in  $name_{-}$  and  $positions_{-}$ , respectively. The sound pressure, which is p' in Equation (1.4), is stored in  $pPrime_{-}$ .

## Chapter 3

mkdir CurleCorr

# Implementation of sound pressure correction

The procedure to implement the spanwise correction for sound pressure is explained here. The original acousticAnalogy library calculates and writes out the sound pressure of each time step. We will modify the code so that it also calculates both the spectrum of the sound pressure  $(SPL_s)$  and the corrected spectrum (SPL) during run time. To obtain the corrected spectrum, the coherence function  $\gamma(f,z)$  first needs to be found using the pressure sampled on the body surface. Then the correction coefficient  $r_{corr}(f)$  is determined from  $\gamma(f,z)$ . The corrected spectrum SPL is calculated by multiplying  $r_{corr}(f)$  to the original spectrum  $SPL_s$ .

Assummed that the acousticFunctionObject directory, which is uploaded on website [2], is placed under \$WM\_PROJECT\_USER\_DIR/src, we first go to \$WM\_PROJECT\_USER\_DIR/src and prepare a new directory CurleCorr for modification by copying and renaming files.

```
cp -r acousticFunctionObject/* CurleCorr/
    cd CurleCorr
    mv Curle/Curle.H Curle/CurleCorr.H
    mv Curle/Curle.C Curle/CurleCorr.C
    mv Curle/CurleFunctionObject.H Curle/CurleCorrFunctionObject.H
    mv Curle/CurleFunctionObject.C Curle/CurleCorrFunctionObject.C
The word Curle is replaced by CurleCorr in all files.
    sed -i s/Curle/CurleCorr/g Curle/*
We rename the library as AcousticAnalogyCorr, so it should be written in Make/files as
    Curle/CurleCorr.C
    Curle/CurleCorrFunctionObject.C
    soundObserver.C
    LIB = $(FOAM_USER_LIBBIN)/libAcousticAnalogyCorr
and in Make/options as
    EXE_INC = \
        -I$(LIB_SRC)/finiteVolume/lnInclude \
        -I$(LIB_SRC)/meshTools/lnInclude \
        -I$(LIB_SRC)/fileFormats/lnInclude \
```

```
-I$(LIB_SRC)/sampling/lnInclude \
-I$(LIB_SRC)/randomProcesses/lnInclude

LIB_LIBS = \
-lspecie \
-lfiniteVolume \
-lmeshTools \
-lfileFormats \
-lsampling \
-lrandomProcesses
```

After all modifications in the following sections are completed, the code can be compiled using the command wmake. The new library named libAcousticAnalogyCorr.so will be created under \$FOAM\_USER\_LIBBIN. The reader can also refer to the supplied final codes when implementing this library.

#### 3.1 Modifications in CurleCorr.H

Two header files should be included.

```
#include "probes.H"
#include "complexFields.H"
```

The probes class is needed to sample the surface pressure which is then used to calculate the coherence function  $\gamma(f,z)$ . The complexFields.H file needs to be included to use the complex numbers for the Fourier analysis. To inherit the probes class, the top of the CurleCorr class declaration should be as follows.

```
class CurleCorr
:
   public functionObjectFile,
   public probes
```

The protected member data from the probes class which are used in this library should be added.

```
const fvMesh& mesh_;
bool loadFromFiles_;
wordReList fieldSelection_;
bool fixedLocations_;
word interpolationScheme_;
```

And the additional member data should be added as well.

```
scalar L_;
scalar Ls_;
label freqSample_;
label Nstart_;
label Naverage_;
label countStep_;
label countFFT_;
List<List<scalar>> pList_;
scalar distance_;
word fileDir_;
scalarField Coh_;
List<List<scalar>> CofftObs_;
```

L\_ and Ls\_ are L and  $L_s$  in Equation (1.5), respectively. For example, if freqSample\_ = 1024 and Nstart\_ = 3, the first  $1024 \cdot 2^{3-1}$  steps are discarded. The spectra are calculated when the number of stored data reaches  $1024 \cdot 2^{i+3}$  ( $i=0,1,\ldots$ ). Every time the spectra are calculated, they are written out in a new file. Naverage\_ is the number for averaging the power spectra, and then the averaged power spectra are used to obtain the coherence function  $\gamma(f,z)$ . distance\_ is the distance between the locations of sampled pressure,  $z_{samp}$ . Coh\_ is the value of  $\gamma(f,z_{samp})$ . CofftObs\_ is the corrected sound pressure,  $p_{corr}$ .

The additional public member functions are declared as

```
virtual void storeSampledPressure();
virtual void calculateSpectrum();
virtual void calculateCoherence();
virtual void calculateCorrection();
virtual complexField calcFFT(const scalarList&);
```

The storeSampledPressure function stores the surface pressure  $p_1$  and  $p_2$  sampled by the probes class. The calculateSpectrum function calculates the spectrum of the sound pressure p' and write it to the file. The calculateCoherence function finds  $Coh_{-}$ , i.e., the value of  $\gamma(f, z_{samp})$  for each frequency f using the  $p_1$  and  $p_2$  data. The calculateCorrection function determines the coherence function  $\gamma(f,z)$  and  $r_{corr}$  to calculate the spectrum of the corrected sound pressure  $p'_{corr}$ , which is also written to the file. The calcFFT function performs the Fourier transform. The detail of each function will be explained in the next section.

#### 3.2 Modifications in CurleCorr.C

The following line should be included in the top.

```
#include "fft.H"
```

This header file is needed for the FFT analysis used in the calcFFT function.

The following lines should be added before the last line initialised\_ = true; in the initialise function.

The above lines give an error message if a user doesn't give a proper value of Nstart\_ or Naverage\_. distance\_ is calculated here and printed out in the log file. pList\_ and CofftObs\_ are initialized to match their size to two and the number of the observers, respectively.

In the constructor, some lines are necessary for initialization

```
probes(name, obr, dict, loadFromFiles),
    mesh_(refCast<const fvMesh>(obr)),
    loadFromFiles_(loadFromFiles),
    fieldSelection_(),
    fixedLocations_(true),
    interpolationScheme_("cell"),
    L_{-}(0),
    Ls_{-}(0),
    freqSample_(1),
    Nstart_(0),
    Naverage_(0),
    countStep_(1),
    countFFT_(0),
    pList_(0),
    distance_(0),
    fileDir_(word::null),
    Coh_{(0)}
    CofftObs_(0)
and one line after read(dict); in the if (readFields) statement as well.
    probes::read(dict);
As for the CurleCorr::read function, the word "patches" in the if (active_) statement should
be replaced by "patchName". And the following lines should be added also in the if (active_)
statement.
    L_ = readScalar(dict.lookup("L"));
    Ls_ = readScalar(dict.lookup("Ls"));
    freqSample_ = readLabel(dict.lookup("freqSample"));
    Nstart_ = readLabel(dict.lookup("Nstart"));
    Naverage_ = readLabel(dict.lookup("Naverage"));
At the end of the CurleCorr::read function, the following lines are needed.
    fileName fileSubDir = name_;
    if (mesh_.name() != polyMesh::defaultRegion)
        fileSubDir = fileSubDir/mesh_.name();
    fileSubDir = "postProcessing"/fileSubDir/mesh_.time().timeName();
    if (Pstream::parRun())
    {
        fileDir_ = mesh_.time().path()/".."/fileSubDir;
    }
    else
    {
        fileDir_ = mesh_.time().path()/fileSubDir;
    }
```

At the end of the definition of the CurleCorr::calculate function, one line should be inserted in the forAll(observers\_, obsI) statement.

```
obs.storepPrime(pPrime);
```

In the CurleCorr::write function, the following lines should be added after the line calculate();.

```
probes::write();
storeSampledPressure();
if ( countStep_ == freqSample_*(pow(2,countFFT_)+pow(2,Nstart_-1)) ) {
    calculateSpectrum();
    calculateCoherence();
    calculateCorrection();
    countFFT_ += 1;
}
```

The first line, probes::write();, is not necessary if the sampled pressure does not need to be written out. The storeSampledPressure() function is executed all time steps. The functions, calculateSpectrum(), calculateCoherence(), and calculateCorrection(), are executed every time it solves the specified number of time steps, more specifically, freqSample\_ $\cdot 2^{i+\text{Nstart}}$  ( $i=0,1,\ldots$ ).

The definition of the CurleCorr::storeSampledPressure function should be as below.

```
void Foam::CurleCorr::storeSampledPressure()
{
    const volScalarField& p = obr_.lookupObject<volScalarField>(pName_);
    const scalarField p_sample = probes::sample( p );

    forAll(p_sample,i)
    {
        pList_[i].append(p_sample[i]);
    }
}
```

This function stores the surface pressure at two locations  $p_1$  and  $p_2$  that a user specifies using the function object probes.

The definition of the CurleCorr::calculateSpectrum function should be as below.

```
void Foam::CurleCorr::calculateSpectrum()
{
    Info <<"Calculating spectrum" << endl;

    mkDir(fileDir_/mesh_.time().timeName());
    OFstream* fPtr1 = new OFstream(fileDir_/mesh_.time().timeName()/"pPrimeFFT");
    OFstream& fout1 = *fPtr1;

fout1 << "# Frequency ";
    forAll( observers_, i)
    {
        fout1 << "pPrimeFFT_at_"<< observers_[i].name() << " ";
    }
}</pre>
```

```
fout1 << endl;</pre>
    scalar deltaT = mesh_.time().deltaT().value();
    scalar N = countStep_ -freqSample_*pow(2,(Nstart_-1));
    scalarField freq(N);
    forAll( freq, i )
        freq[i] = i/(deltaT*N);
    }
    forAll( observers_, i)
        SubList<scalar> subpPrimeList( observers_[i].pPrimeAll(), N,
                                          freqSample_*pow(2,(Nstart_-1)));
        scalarField Cofft_obs_i = mag(calcFFT( subpPrimeList ));
        CofftObs_[i] = Cofft_obs_i;
    }
    forAll( freq, freqi)
        fout1 << freq[freqi] << " ";</pre>
        forAll( observers_, i)
        {
            fout1 << CofftObs_[i][freqi] << " ";</pre>
        fout1 << endl;
  }
}
```

The original Curle class calculates the sound pressure in the calculate() function. Then this function applies the FFT to obtain the spectrum, stores both frequency and its magnitude in CofftObs\_, and write it in a new file.

The definition of the CurleCorr::calculateCoherence function should be as below.

{

```
scalar hanningi = 0.5*(1 -cos(constant::mathematical::twoPi*freqi/N2));
                pListWin[freqi] = subpList[freqi] *hanningi;
            pListFFTtemp.append(calcFFT( pListWin ));
        }
        complexField Wxyi(N2);
        complexField Wxxi(N2);
        complexField Wyyi(N2);
        forAll( pListFFTtemp[0], freqi )
            Wxyi[freqi] = pListFFTtemp[0][freqi].conjugate() *pListFFTtemp[1][freqi];
            Wxxi[freqi] = pListFFTtemp[0][freqi].conjugate() *pListFFTtemp[0][freqi];
            Wyyi[freqi] = pListFFTtemp[1][freqi].conjugate() *pListFFTtemp[1][freqi];
        }
        Wxy[i] = Wxyi;
        Wxx[i] = Wxxi;
        Wyy[i] = Wyyi;
    }
    Coh_.resize(N2);
    forAll( Wxy[0], freqi )
        complex WWxy;
        complex WWxx;
        complex WWyy;
        forAll( Wxy, i )
            WWxy += Wxy[i][freqi]/Naverage_;
            WWxx += Wxx[i][freqi]/Naverage_;
            WWyy += Wyy[i][freqi]/Naverage_;
        }
        Coh_[freqi] = magSqr(WWxy)/( mag(WWxx)*mag(WWyy) );
    }
}
```

This function first applies the FFT to each Naverage\_ segment of the sampled pressure with the Hann window. Then after averaging the power spectra of all segments, the coherence  $\gamma(f, z_{samp})$  in Equation (1.7) is obtained and stored in Coh\_.

The definition of the CurleCorr::calculateCorrection function should be as below.

```
void Foam::CurleCorr::calculateCorrection()
{
    Info << "Calculating correction " << endl;

    scalar deltaT = mesh_.time().deltaT().value();
    scalar N2 = ( countStep_ -freqSample_*pow(2,(Nstart_-1)) )/Naverage_;</pre>
```

```
scalarField freq(N2);
forAll( freq, i )
    freq[i] = i/(deltaT*N2);
}
scalar 12;
scalar Lc;
scalarField rCorr(N2);
forAll( freq, freqi )
    if (Coh_[freqi] < 0.5)
    {
        rCorr[freqi] = sqrt(L_/Ls_);
    else if ( 0.5 \le Coh_{freqi} \& Coh_{freqi} \le 0.999999 )
        12 = -0.5*sqr(distance_)/log(Coh_[freqi]);
        Lc = sqrt( -2 *12 *log(0.5) );
        rCorr[freqi] = sqrt(L_*Lc)/Ls_;
        if ( Lc > L_ )
        {
            rCorr[freqi] = L_/Ls_;
        }
    }
    else
        rCorr[freqi] = L_/Ls_;
    }
}
List<List<scalar>> CofftObsCorr(observers_.size());
forAll( observers_, i)
{
    CofftObsCorr[i].resize(N2);
    forAll( freq, freqi )
        scalar fft0 = Cofft0bs_[i][freqi*Naverage_];
        CofftObsCorr[i][freqi] = fftO*rCorr[freqi];
    }
}
mkDir(fileDir_/mesh_.time().timeName());
OFstream* fPtr2 = new OFstream(fileDir_/mesh_.time().timeName()/"pPrimeFFT_corr");
OFstream& fout2 = *fPtr2;
fout2 << "# Frequency ";</pre>
forAll( observers_, i)
    fout2 << "pPrimeFFTcorrected_at_" << observers_[i].name() << " ";</pre>
```

```
fout2 << endl;

forAll( freq, freqi)
{
    fout2 << freq[freqi] << " ";
    forAll( observers_, i)
    {
        fout2 << CofftObsCorr[i][freqi] << " ";
    }
    fout2 << endl;
}</pre>
```

This function calculates the correction coefficient  $r_{corr}$ , which is then used to determine the corrected spectrum of the sound pressure. The correction coefficient represented as **rCorr** in the code is found for each frequency as explained in Equation (1.6) based on the coherence. The corrected spectrum is obtained by multiplying **rCorr** to CofftObs\_ and it is printed out in the new file.

The definition of the CurleCorr::calcFFT function should be as below.

This function uses the fft class, which needs an input of the complex field. ReComplexField creates a list of the complex values. The calcFFT function returns the result scaled by the size of input data.

#### 3.3 Modifications in soundObserver.H

One private member data should be added

```
List<scalar> pPrimeAll_;
and two public member functions as well.

const List<scalar>& pPrimeAll() const
{
    return pPrimeAll_;
}

void storepPrime(scalar pPrime);
```

#### 3.4 Modifications in soundObserver.C

In the constructor, the following line should be added after pPrime\_(0.0),.

```
pPrimeAll_(0)
```

The definition of the SoundObserver::storepPrime function should be as below.

```
void Foam::SoundObserver::storepPrime(scalar pPrime)
{
     pPrimeAll_.append(pPrime);
}
```

## Chapter 4

### Test case

This section represents an example case where the AcousticAnalogyCorr library is applied. In this test case, a circular cylinder is placed in the flow field and the sound is observed at some distance away from the cylinder. The cylinder has longer span length than the height of the computational domain. The library will calculate the spectrum of the sound pressure, p, which is generated from the span section of the computational domain. The spectrum of the corrected sound pressure,  $p_{corr}$ , generated from the entire cylinder will also be obtained.

#### 4.1 Case description

Figure 4.1 shows the setup where the span length in the computational domain is  $L_s$  (= 0.05 m) and the total span length of the cylinder is L (= 0.5 m). The pressure is sampled at two locations on the cylinder surface,  $p_1$  and  $p_2$ . The inlet velocity is 70.2 m/s and the cylinder diameter is 19.0 mm.

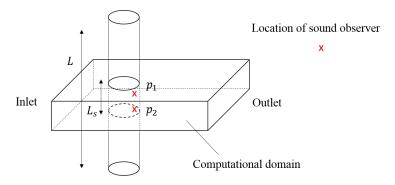


Figure 4.1: Setup of test case

The input entries in functions in the controlDict file should includes as follows.

```
CurleCorr
{
    functionObjectLibs
                         ( "libAcousticAnalogyCorr.so" );
                         CurleCorr;
    outputControl
                         timeStep;
    outputInterval
                         1;
    fields
                         (p);
                         ( cylinder );
    patchName
    fixedLocations
                         true;
    probeLocations
```

```
(
    (0.0095057 \ 0 \ -0.02)
    (0.0095057 \ 0 \ 0.02)
);
log
                     true;
rhoRef
                     1.204;
cRef
                     343;
observers
{
    micro1 { position (0 -2.4335 0); }
    micro2 { position (-2.4335 0 0); }
    micro3 { position (-2.4335 -2.4335 0); }
}
L
                     0.5;
Ls
                     0.05;
freqSample
                     1024;
Nstart
                     3;
                     4;
Naverage
```

Two locations where the surface pressure is sampled should be specified in probeLocations. cRef is the sound speed and rhoRef is the density of the medium. The name and the location for sound observers should be given in observers. L and L<sub>s</sub> are L and L<sub>s</sub>, respectively. freqSample, Nstart, and Naverage correspond the variables mentioned early in Section 3.1. freqSample and Naverage must be a number of powers of two.

Note that the code in this library assume a constant time step, which means that adjustableRunTime in controlDict should be switched off. To make it simple, the surface pressure at only two points are chosen to sample for calculation of the coherence function. The distance between their two points should not be too close for accurate correction.

#### 4.2 Results

}

Figure 4.2 shows the sound pressure spectra observed at 2.4 m away from the center of the cylinder. The red line represents the spectrum of  $p_{corr}$  obtained based on the correction coefficient  $r_{corr}$  expressed in Equation (1.6). It can be seen that the magnitude of  $p_{corr}$  are larger than that of p by correction.

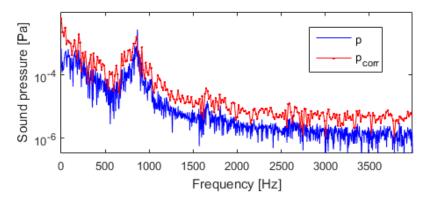


Figure 4.2: Sound pressure spectrum

# **Bibliography**

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# Study questions

- 1. Why does the AcousticAnalogy library have the SoundObserver class besides the main Curle class?
- 2. What is the purpose of implementing the AcousticAnalogyCorr library?
- 3. What is the purpose of inheriting the probes class in the AcousticAnalogyCorr library?
- 4. If  $L/L_s$  is for example 20, what is the maximum and minimum differences of the SPL in decibel between p and  $p_{corr}$  according to the correction method implemented in the library?
- 5. The AcousticAnalogyCorr library creates files for the spectrum of p and  $p_{corr}$  including each of the frequency table. How many times is the difference of the frequency resolution between them?