



# MooDy: a dynamic mooring library used for station-keeping simulations in OpenFOAM

**Johannes Palm, Claes Eskilsson and Lars Bergdahl**

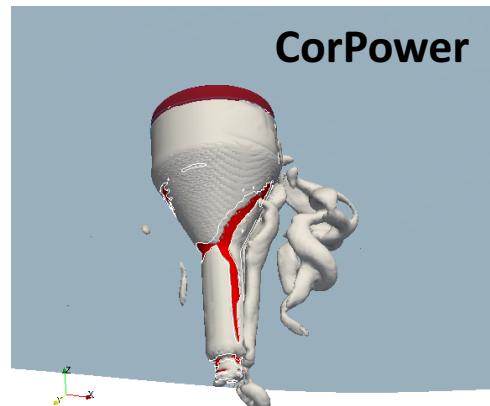
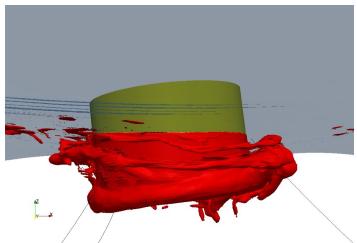
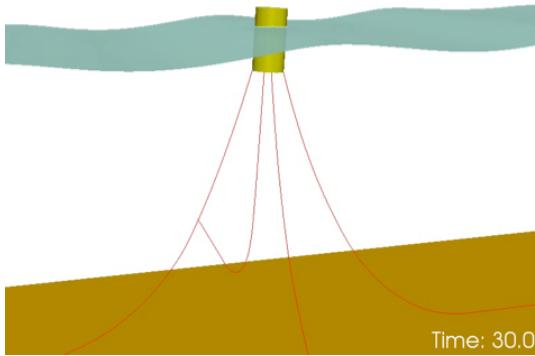
Associate Professor  
Dep of Civil Engineering  
Aalborg University, Denmark  
[cge@civil.aau.dk](mailto:cge@civil.aau.dk)

Senior Researcher  
Safety and Transport  
RISE Research Institutes of Sweden  
[claes.eskilsson@ri.se](mailto:claes.eskilsson@ri.se)

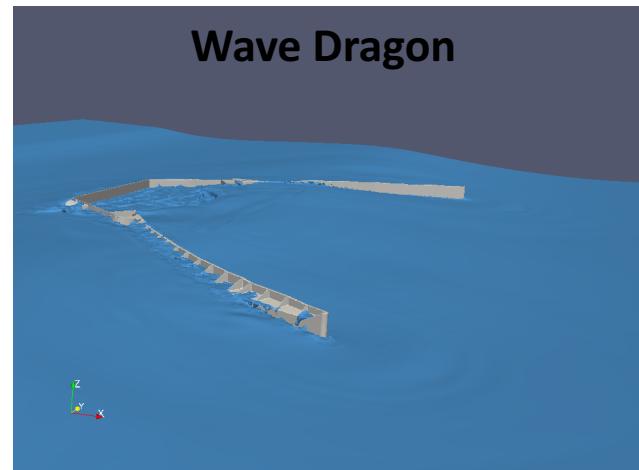


# Floating wave energy converters...

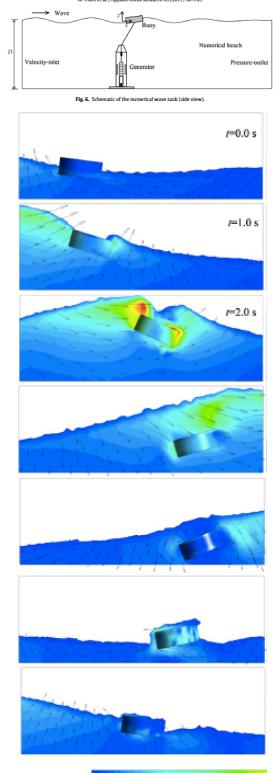
Simple forms



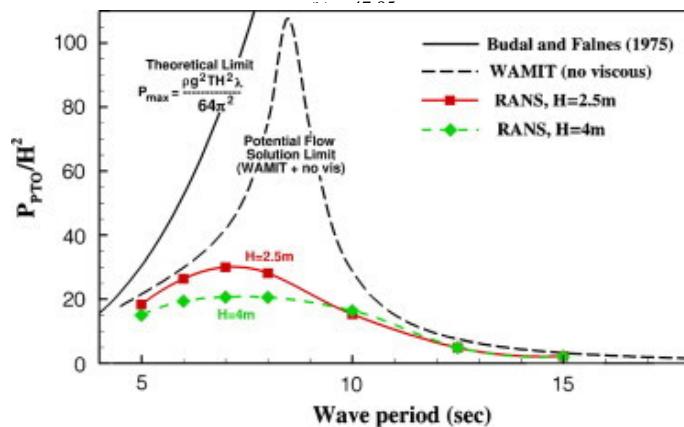
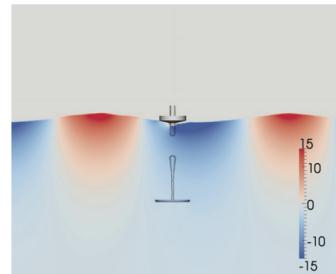
Wave Dragon



## Survival



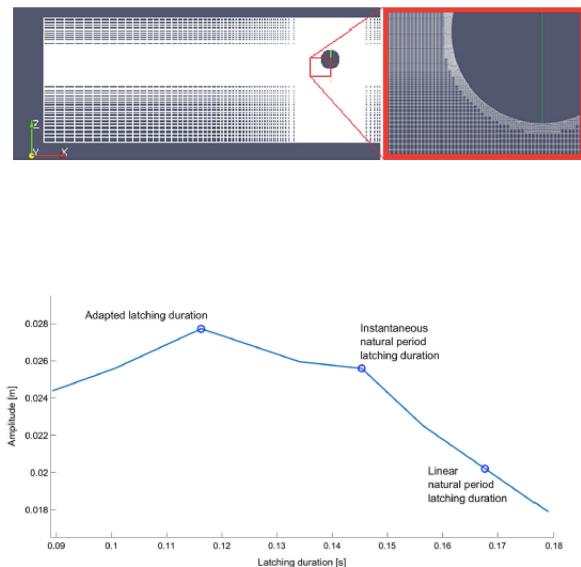
## Resonance



Chen et al 2016

Yu and Li 2013

## Control

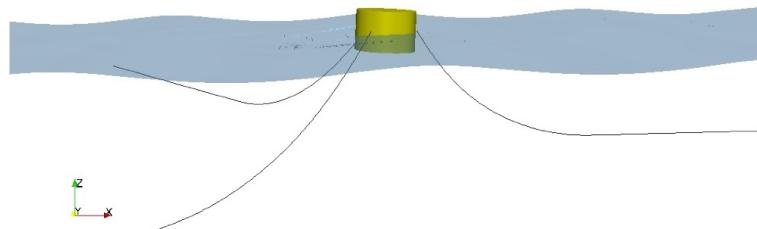


Girogi Ringwood 2016

# MooDy is a solver for mooring cable dynamics

- Designed to handle snap loads
  - Equations for re-written in conservative form
  - High-order discontinuous Galerkin method
  - $hp$ -adaptive solution
  - Explicit time-steppers
- Cables with negligible bending stiffness
- Written in C++ with no dependencies (except std lib)
- Coupled to OpenFOAM and WEC-SIM/FAST
- Released as pre-compiled lib

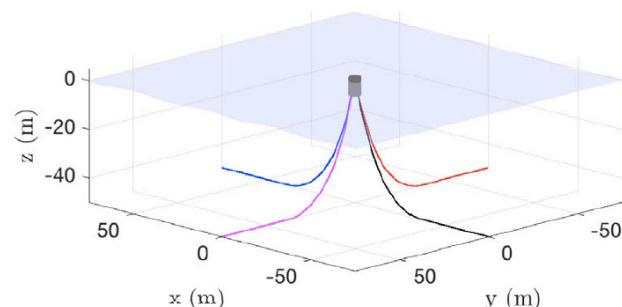
OpenFOAM



11/

WEC-SIM (and FAST)

— c<sub>1</sub> — c<sub>2</sub> — c<sub>3</sub> — c<sub>4</sub>



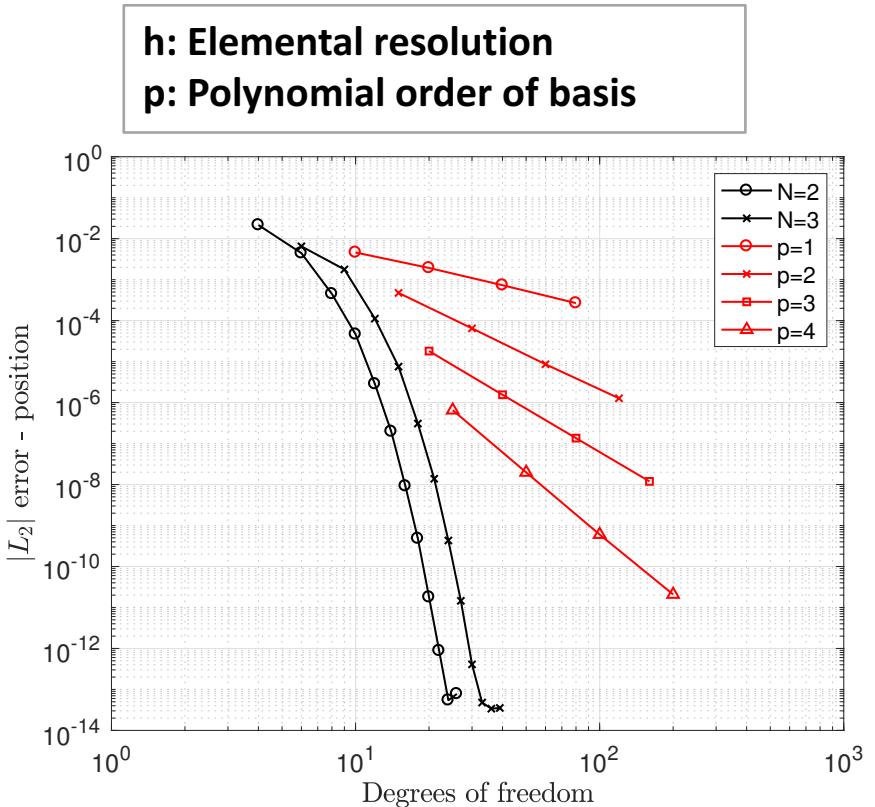
- Smooth solutions

- Verified on linearised standing wave
- Exponential convergence:  $h^{p+1/2}$

**Use high-order elements!**

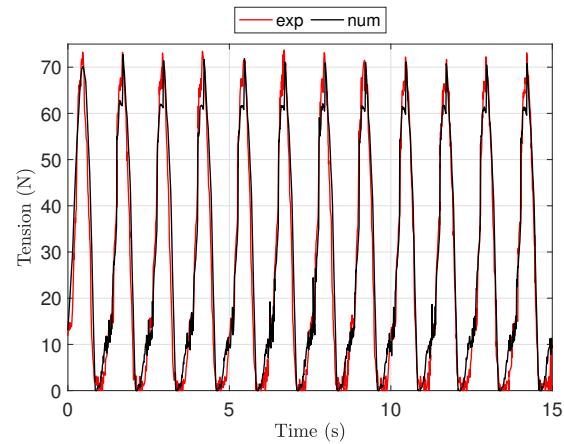
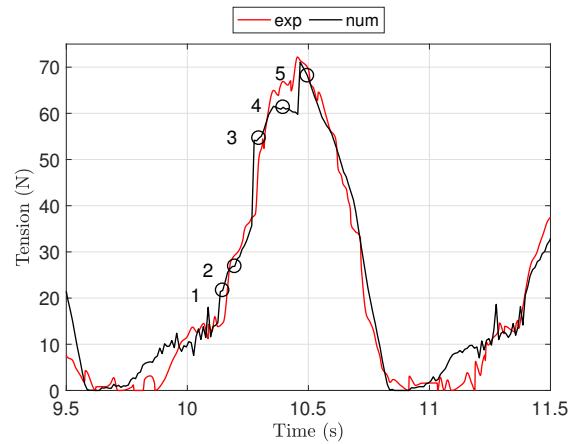
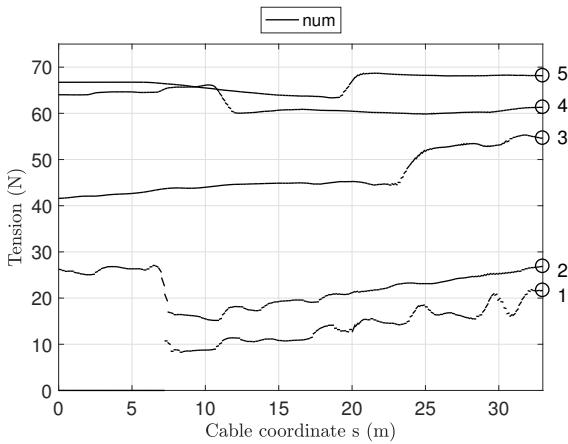
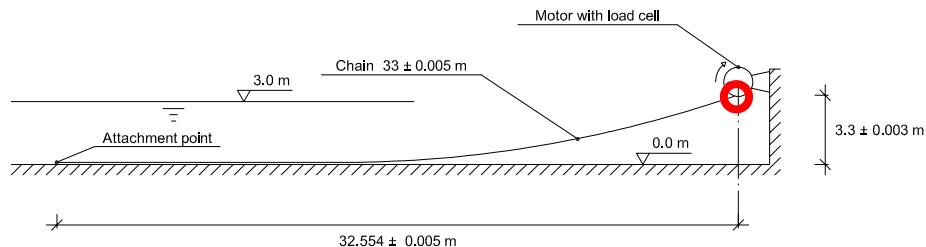
Table 1: Convergence rates for the linear standing wave for position.  $\alpha$  is the convergence rate based on  $\varepsilon = Ch^\alpha$ .

$p$	$\varepsilon_{N10}$	$\varepsilon_{N20}$	$\varepsilon_{N40}$	$\alpha_{20/10}$	$\alpha_{40/20}$
1	$2.13 \times 10^{-3}$	$7.65 \times 10^{-4}$	$2.73 \times 10^{-4}$	1.48	1.48
2	$1.03 \times 10^{-4}$	$1.30 \times 10^{-5}$	$1.63 \times 10^{-6}$	3.00	2.99
3	$1.57 \times 10^{-6}$	$1.36 \times 10^{-7}$	$1.20 \times 10^{-8}$	3.52	3.51
4	$3.75 \times 10^{-8}$	$1.08 \times 10^{-9}$	$3.05 \times 10^{-11}$	5.12	5.14



- **Validation case**

- *Excellent match with experimental data*
- *Snap load from cable slack*



## Station-keeping approaches used

- Heave only → `sixDoFRigidBodyMotionConstraints::line/axis`
- Linear spring → `sixDoFRigidBodyMotionRestraints::linearSpring`
- Quasi-static approach → `sixDoFRigidBodyMotionRestraints::mooringLine` (`waves2Foam`)
- **Dynamic approach → `sixDoFRigidBodyMotionRestraints::moodyR`**

```

/*-----*
     Class moodyR Declaration
-----*/
class moodyR
{
    public sixDoFRigidBodyMotionRestraint
    {
        // Private data

        // Reference points of attachment to the solid body //
        List<point> attachPts_;

        // Word containing the filename of the input file for the
        mooring system //
        string mooringSystemFilename_;

        // The number of attachment points //
        int noOfAttachments_;

        // The ramp time of the mooring force (not invoked in moody,
        but before force is returned to motion_) //
        scalar mooringRampTime_;

        // Last call time of function //
        scalar startTime_;

        // If moored or not
        bool moored_;

        // Switch to ensure that moody is only initialised once
        bool moodyStarted_;

    public:

        // Runtime type information
        TypeName("moodyR");

```

```

// Constructors

// Construct from components
moodyR
(
    const word& name,
    const dictionary& sDoFRBMRDict
);

// Construct and return a clone
virtual autoPtr<sixDoFRigidBodyMotionRestraint> clone()
const
{
    return autoPtr<sixDoFRigidBodyMotionRestraint>
    (
        new moodyR(*this)
    );
}

// Destructor
virtual ~moodyR();

// Member Functions

// Calculate the restraint position, force and moment.
// Global reference frame vectors.
void restrain
(
    const sixDoFRigidBodyMotion& motion,
    vector& restraintPosition,
    vector& restraintForce,
    vector& restraintMoment
);

// Update properties from given dictionary
bool read(const dictionary& sDoFRBMRCoeff);

// Write
void write(Ostream&) const;
};


```

```

void Foam::sixDoFRigidBodyMotionRestraints::moodyR::restrain
(
    const sixDoFRigidBodyMotion& motion,
    vector& restraintPosition,
    vector& restraintForce,
    vector& restraintMoment
)
{
    ...
    if ( moored_ )
    {
        // Compute values at present motion state
        double attachInfo[3*noOfAttachments_]; // Always 3D
        List<point> currentPositions(attachPts_);

        for ( int ii = 0; ii<noOfAttachments_; ++ii)
        {
            // Transform the starting points to present
            motion state
            currentPositions[ii] =
            motion.transform(attachPts_[ii]);

            // Fill attachInfo with transformed values
            attachInfo[ii*3] = currentPositions[ii].x();
            attachInfo[ii*3+1] = currentPositions[ii].y();
            attachInfo[ii*3+2] = currentPositions[ii].z();
        }

        // Send info to moody
        double allForces[3*noOfAttachments_];

        moodySolve( attachInfo , allForces ,
        motion.state0().time() , motion.state().time());
    }
}

```

```

// Compute moment and total force
vector tmpVector(vector::zero);

for ( int ii = 0; ii<noOfAttachments_; ++ii)
{
    tmpVector[0] = -allForces[ii*3];
    tmpVector[1] = -allForces[ii*3+1];
    tmpVector[2] = -allForces[ii*3+2];

    restraintForce += tmpVector;

    restraintMoment += (currentPositions[ii] -
    motion.centreOfRotation())^tmpVector;

    Info<< " Mooring force at point " << ii << ", "
position: " << currentPositions[ii] << " is : " << tmpVector
           << " Total force: " << restraintForce
           << " Total moment: " << restraintMoment
           << endl;
}

// End mooring loop with assigning rP as
centreOrRotation. No added moment should be computed //
restraintPosition = motion.centreOfRotation();
}

} // end of restrain member

```

```
restraints
{
    mooring
    {
        sixDoFRigidBodyMotionRestraint      moodyR;

        attachmentPoints      (
            (0.6 0.6 0.3)
            (0.6 0.4 0.3)
            (0.4 0.4 0.3)
            (0.4 0.6 0.3)
        );

        mooringSystemFilename      "moodyInput.txt";
    }
}
```

```

%----- Time settings -----
startTime = 0; % [s] Start time
endTime = 1; % [s] End time of simulation
timeStep = 5e-5; % [s] Time step size
saveInterval = 0.1; % save results every xx time interval
timeStepScheme='RK3'; %'RK3'
lagTimeFraction = 0.5;
courantNo = 0.9; % compute time step size from Courant no. (CFL condition)

%----- General settings -----
gravity = 1; % [-] Gravity is 1=on, 0=off
waterLevel = 0.52; % [m] z-coordinate of mean water level
waterDensity = 1e3; % [kg/m??] Density of water
airDensity = 0; % [kg/m??] Density of air
dimensionNumber = 3; % [-] 1D, 2D or 3D : 1, 2 or 3

%----- Ground model input -----
% ground.type = 'springDampGround';
% ground.level = -50;
% ground.dampingCoeff = 1;
% ground.frictionCoeff = 1;
% ground.vc = 0.1;
% ground.stiffness = 1e6;

%----- Type definition -----
cableType1.diameter = 0.01;
cableType1.gamma0 = 1;
cableType1.CDn = 1.5;
cableType1.CDt = 0.1;
cableType1.CMn = 1.0;
cableType1.materialModel.type = 'bilinearCable';
cableType1.materialModel.EA = 100; % specific input to material model.

%----- Geometry -----
vertexLocations = {
    1 [2.5 2.5 0];
    2 [0.0 0.0 0.0];
    3 [2.5 -1.5 0];
    4 [0.0 0.0 0.0];
    5 [-1.5 -1.5 0];
    6 [0.0 0.0 0.0];
    7 [-1.5 2.5 0];
    8 [0.0 0.0 0.0];
};


```

```

%----- Object definitions -----
cableObject1.name = 'cable1';
cableObject1.typeNumber = 1;
cableObject1.startVertex = 1; %
cableObject1.endVertex = 2; %
cableObject1.length = 1.0; %
cableObject1.IC.type = 'Prestrain';
cableObject1.IC.esp0 = 0.1;
cableObject1.mesh.N = 5;
cableObject1.mesh.P = 4;

cableObject2.name = 'cable2';
cableObject2.typeNumber = 1;
cableObject2.startVertex = 3; %
cableObject2.endVertex = 4; %
cableObject2.length = 1.0; %
cableObject2.IC.type = 'Prestrain';
cableObject2.IC.esp0 = 0.1;
cableObject2.mesh.N = 5;
cableObject2.mesh.P = 4;

cableObject3.name = 'cable3';
cableObject3.typeNumber = 1;
cableObject3.startVertex = 5; %
cableObject3.endVertex = 6; %
cableObject3.length = 1.0; %
cableObject3.IC.type = 'Prestrain';
cableObject3.IC.esp0 = 0.1;
cableObject3.mesh.N = 5;
cableObject3.mesh.P = 4;

cableObject4.name = 'cable4';
cableObject4.typeNumber = 1;
cableObject4.startVertex = 7; %
cableObject4.endVertex = 8; %
cableObject4.length = 1.0; %
cableObject4.IC.type = 'Prestrain';
cableObject4.IC.esp0 = 0.1;
cableObject4.mesh.N = 5;
cableObject4.mesh.P = 4;

%----- Boundary conditions -----
bc1.vertexNumber = 1;
bc1.type = 'dirichlet'; % 'dirichlet', 'neumann' or mixed.
bc1.mode = 'fixed';

bc2.vertexNumber = 2;
bc2.type = 'dirichlet';
bc2.mode = 'externalPoint'; % 'laggingQuadraticInterp';

bc3.vertexNumber = 3;
bc3.type = 'dirichlet'; % 'dirichlet', 'neumann' or mixed.
bc3.mode = 'fixed';

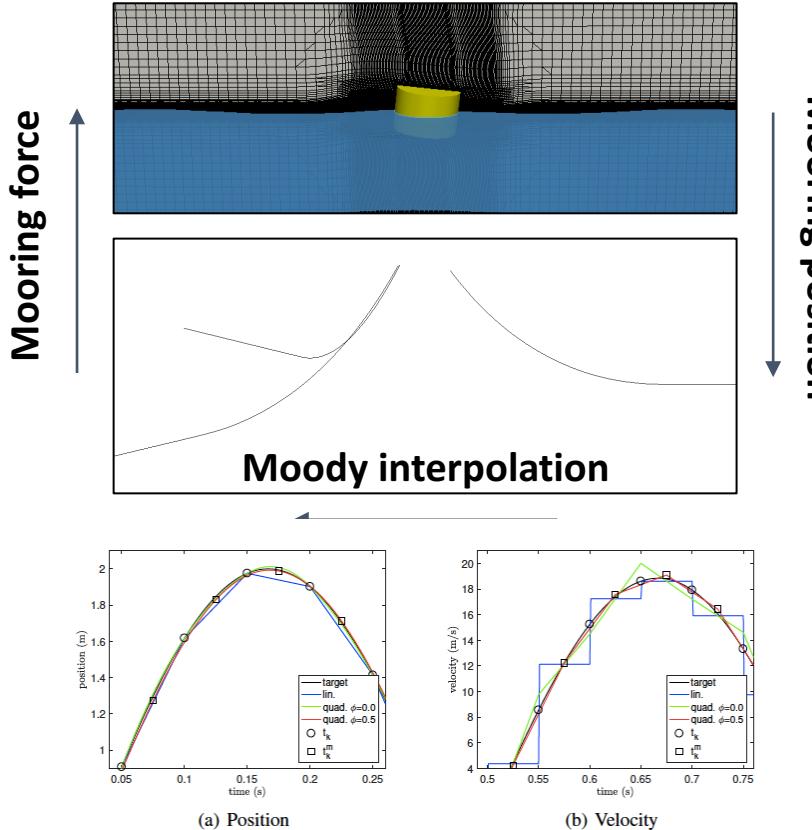
bc4.vertexNumber = 4;
bc4.type = 'dirichlet';
bc4.mode = 'externalPoint'; % 'laggingQuadraticInterp';

bc5.vertexNumber = 5;
bc5.type = 'dirichlet'; % 'dirichlet', 'neumann' or mixed.
bc5.mode = 'fixed';

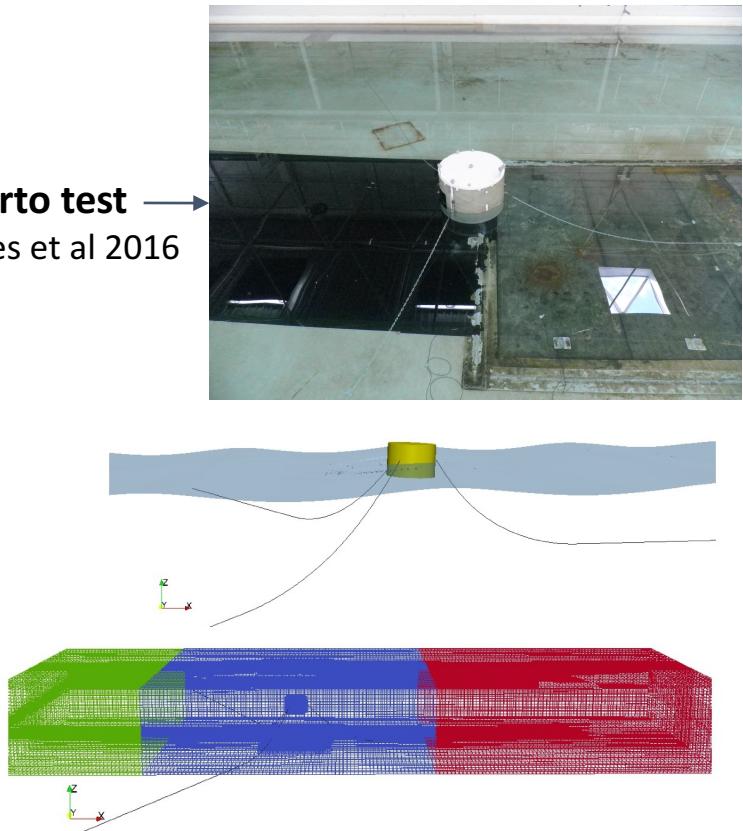
bc6.vertexNumber = 6;
bc6.type = 'dirichlet';
bc6.mode = 'fixed';

```

Two timescales. Boundary condition interpolation required

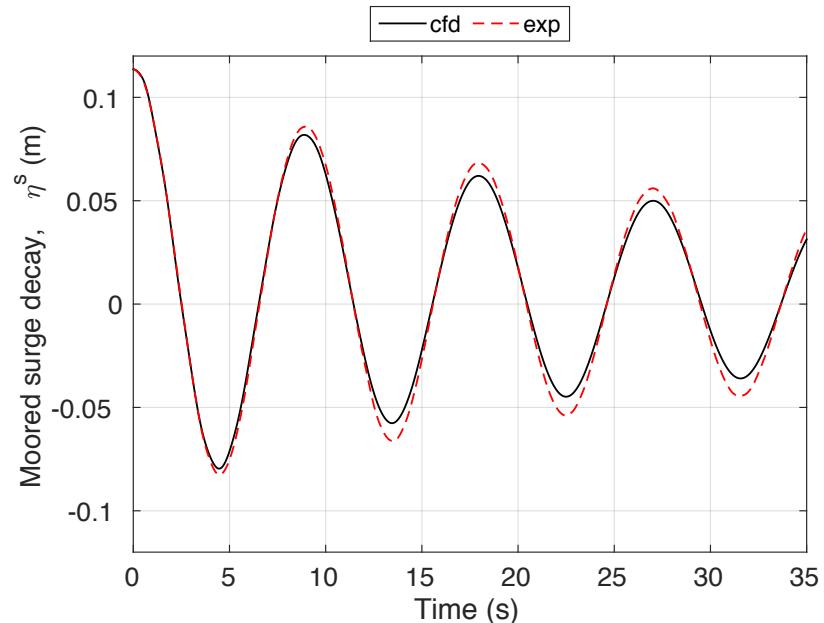


Porto test →  
Paredes et al 2016



- **Surge (horizontal)**

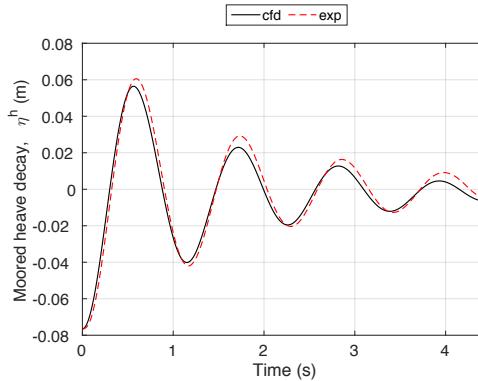
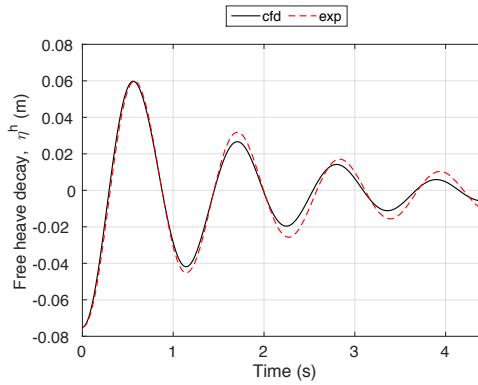
- *Very good agreement*
- *All stiffness comes from the moorings*
- *Coupled mooring validated!*



- **Heave (vertical)**



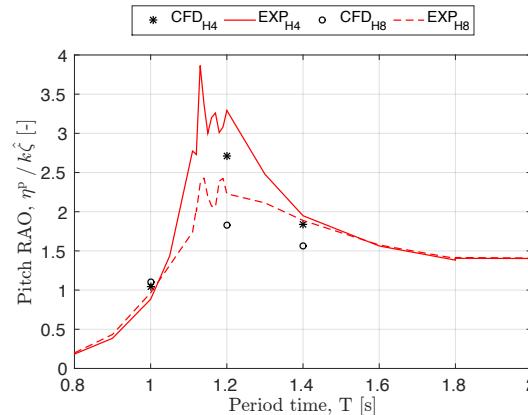
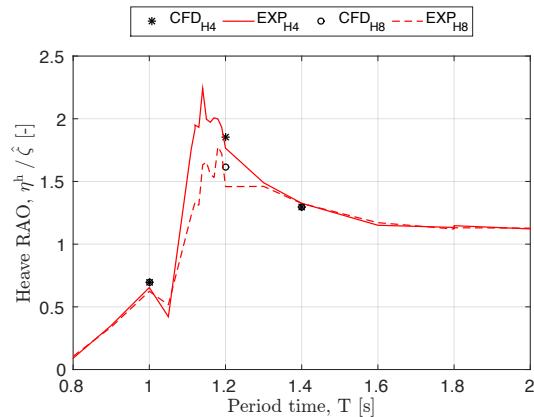
- *Very good agreement both with and without moorings*
- *Slightly more damping in cfd*



- Motion response

- Three wave periods, two wave heights*
- Good agreement in heave and mooring force*
- RAO is strongly nonlinear*
- Pitch is underpredicted, but influence of nonlinearity is correct*

**RAO: Response Amplitude Operator**  
***Motion amplitude / wave amplitude.***  
***Constant for each frequency in linear theory***

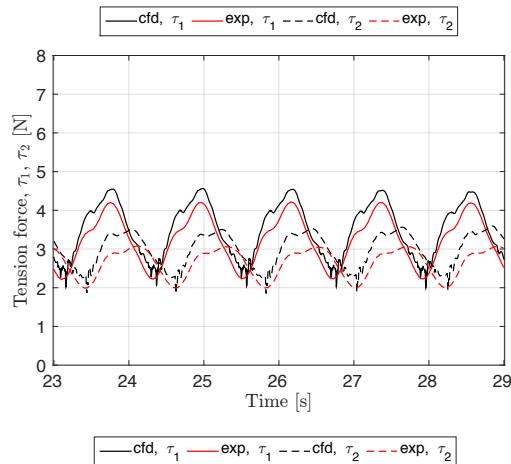


- Mooring forces**

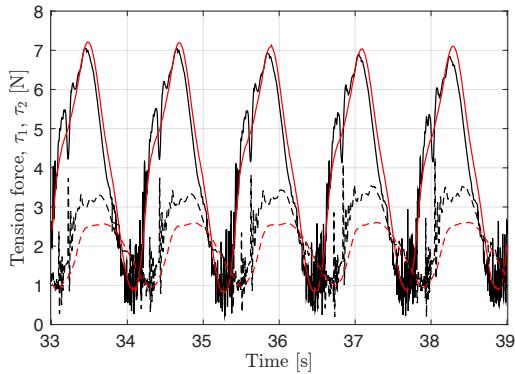
- Good agreement in mooring forces*
- Overall dynamic behaviour captured*
- Some discrepancies in amplitude*



$T=1.2 \text{ s}, H=4 \text{ cm}$



$T=1.2 \text{ s}, H=8 \text{ cm}$



# Detailed info can be found in the following publications (open-access)

V International Conference on Computational Methods in Marine Engineering  
MARINE 2013  
B. Brinkmann and P. Wriggers (Eds)

## SIMULATION OF MOORING CABLE DYNAMICS USING A DISCONTINUOUS GALERKIN METHOD

JOHANNES PALM<sup>a</sup>, GUILHERME MOURA PAREDES<sup>b†</sup>, CLAES ESKILSSON<sup>a</sup>, FRANCISCO TAVEIRA PINTO<sup>b</sup> AND LARS BERGDAHL<sup>a\*</sup>

\* Department of Shipping and Marine Technology  
Chalmers University of Technology  
SE-412 96 Gothenburg, Sweden  
Email: johannes.palm@chalmers.se Web page: www.chalmers.se

<sup>†</sup> Departamento de Engenharia Civil  
Faculdade de Engenharia, Universidade do Porto  
4200-465 Porto, Portugal  
Email: moura.paredes@fe.up.pt Web page: www.fe.up.pt

[http://publications.lib.chalmers.se/records/fulltext/185127/local\\_18](http://publications.lib.chalmers.se/records/fulltext/185127/local_18)

Key words: Mooring cables, Discontinuous Galerkin method, High-order finite elements  
<http://publications.lib.chalmers.se/records/fulltext/185127.pdf>  
Abstract: A new numerical model for simulating the dynamics of mooring cables is presented. The model uses the *hp* formulation of the discontinuous Galerkin method. Verification against analytical solutions for a static and a dynamic case is carried out and the model is shown to exhibit exponential convergence with increasing polynomial

Ocean Engineering 144 (2017) 266–276

Contents lists available at ScienceDirect

Ocean Engineering

journal homepage: [www.elsevier.com/locate/oceaneng](http://www.elsevier.com/locate/oceaneng)

International Journal of Marine Energy 16 (2016) 83–99

Contents lists available at ScienceDirect

International Journal of Marine Energy

journal homepage: [www.elsevier.com/locate/ijome](http://www.elsevier.com/locate/ijome)

Coupled mooring analysis for floating wave energy converters using CFD: Formulation and validation

CrossMark

Johannes Palm <sup>a,\*</sup>, Claes Eskilsson <sup>a</sup>, Guilherme Moura Paredes <sup>b</sup>, Lars Bergdahl <sup>a</sup>

<sup>a</sup>Department of Shipping and Marine Technology, Chalmers University of Technology, SE-412 96 Gothenburg, Sweden

<sup>b</sup>Department of Civil Engineering, Faculty of Engineering, University of Porto, 4200-465 Porto, Portugal

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journal homepage: [www.elsevier.com/locate/oceaneng](http://www.elsevier.com/locate/oceaneng)

ARTICLE INFO

015  
2016  
May 2016

ABSTRACT

Floating wave energy converters (WECs) affected by non-linearities arising from motion and the mooring restraints. To a method which readily accounts for the coupled mooring analysis using a two-dimensional finite element model of mooring cables. The model is validated against experimental measurements of a cylinder in a wave tank. There is a comparison between the computational results with respect to the coupled numerical model and the experimental amplitude of the moored cylinder. © 2016 The Authors. Published by Elsevier

<http://www.sciencedirect.com/science/article/pii/S2211869116000077>

MOODY

JOHANNES PALM  
CLAES ESKILSSON

[www.sciencedirect.com/science/article/pii/S2211869116000077](http://www.sciencedirect.com/science/article/pii/S2211869116000077)

ARTICLE INFO

Keywords:  
Mooring cable  
Snap load  
Discontinuous Galerkin method  
High-order  
Shock-capturing

ABSTRACT

This paper focuses on modelling snap loads in mooring cables. Snap loads are a known problem for the established oil and gas industry, and they pose a major challenge to robust mooring design for the growing industry of wave energy conversion. We present a discontinuous Galerkin formulation using a local Lax-Friedrich Riemann solver to capture snap loads of mooring cables. A high-order hp-adaptive discontinuous Galerkin method is used to automatically change the order of the numerical solution. A shock indicator and a shock-capturing to capture shocks with slope-limited linear elements while using high-order Legendre polynomials. The shock indicator is based on the condition number of the stiffness matrix, and the shock indicator is  $p = 1/2$  for smooth solutions. Efficient and accurate computations of idealised shock waves in both linear and non-linear materials were achieved using *hp*-adaptivity. Comparison with experimental data gives excellent results.

THESIS FOR THE DEGREE OF DOCTOR OF PHILOSOPHY

Mooring Dynamics for Wave Energy Applications

A high-order discontinuous Galerkin method for cables, coupled to Reynolds averaged Navier-Stokes simulations.

JOHANNES PALM

[publications.lib.chalmers.se/records/fulltext/248879/248879.pdf](http://publications.lib.chalmers.se/records/fulltext/248879/248879.pdf)



Department of Shipping and Marine Technology  
CHALMERS UNIVERSITY OF TECHNOLOGY  
Gothenburg, Sweden  
2017

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**sixDOFRigidBodyRestraint::moodyR** and **libmoodyWrap.so**  
can be downloaded from:

**<https://github.com/johannep/moodyAPI>**